

Aluminum Structural Plate

Aluminum Box Culvert


## Table of Contents

## Steel and Aluminum Structural Plate design manual.

This design manual is provided to assist designers with most applications and design aspects of Contech Engineered Solutions' MULTI-PLATE, Aluminum Structural Plate, Aluminum Box Culverts, SUPER-SPAN/SUPER-PLATE and BridgeCor. In addition to this written guideline, standard CAD details which can be used by any designer to aid with plan preparation are available. Hydraulic nomographs or FHWA HY-8 support is available from your local Contech representative.

## Typical Design Steps

Selection of Structure Shape ...................................... 5
Designing for Service Life .......................................... 7
Structural Design of Corrugated Metal Structures ..... 13
Minimum Cover over Plate Structures ....................... 22
Structure End Treatments ......................................... 23
Material Design and Installation Specs ..................... 29
MULTI-PLATE
Product Details ....................................................... 30
Round .................................................................... 32
Vertical Ellipse......................................................... 34
Pipe Arch................................................................ 36
Single Radius Arch ................................................... 39
Horizontal Ellipse .................................................... 42
Underpass............................................................. 44
Specifications......................................................... 46

## Aluminum Structural Plate <br> Product Details........................................................ 49

Round .................................................................... 51
Pipe Arch................................................................. 52
Single Radius Arch .................................................. 54
Underpass.............................................................. 56
Ellipse ..................................................................... 58
Handling Weights .................................................. 59
Reinforcing Rib Design ............................................ 60
Specification ........................................................... 61
Aluminum Box Culvert
Design Details for H20/H25 Live Loads ..... 64
H-20/HS-20 ..... 66
H-25/HS-25 ..... 67
HL-93 ..... 68
Prefabricated Aluminum Headwalls ..... 71
Prefabricated Aluminum Full Invert ..... 74
Prefabricated Aluminum Footing Pads ..... 77
Specification ..... 80
SUPER-SPAN/SUPER-PLATE
General Design Overview ..... 81
Steel Design Details ..... 86
Steel Specifications. ..... 93
Aluminum Design Details ..... 95
Aluminum Specifications. ..... 98
BridgeCor
Product Details ..... 101
Specifications ..... 103
Box Culvert Design Details. ..... 107
Round Design Details ..... 112
Single Radius Arch Design Details ..... 114
2-Radius Arch Design Details ..... 116

## Outline of Typical Design Steps

The following steps describe a basic, typical procedure for designing a structural plate bridge or culvert but are not intended to represent all possible considerations that a prudent designer should investigate. Although not all of these steps will be covered in this document, additional design aids are available. Should the designer have questions regarding an aspect of structure designs, the designer should contact the local Contech representative or call 800-338-1 122 for the telephone number of the local Contech representative.

## Design Sequence and References

1. General Structure Selection

- Guidelines for selection of Hydraulic, Traffic/ Pedestrian passage, or grade separation structure

2. Additional Selection Considerations

- Refining Structure Selection

3. Check Service Life and Protection of Structure from Environment

- Environmental Effects
- Design Life
- Material Selection - Galvanized Steel or Aluminum
- Protection from aggressive environments
- De-icing Salts

4. Check Structure Hydraulics (not covered herein)

- Performing Hydraulic Checks
- Hydraulics of corrugated metal structures
- Tools for hydraulic analysis*
- Scour Analysis

5. Check Structural Design

- Performing Structural Checks
- Design Methods outline
- American Association of State Highway and Transportation Officials (AASHTO covered herein) ${ }^{* *}$
- American Iron and Steel Institute
- Example calculations
- Material Properties
- Load Rating Structural Plate (not covered herein) ***
* Hydraulic nomographs and FHWA HY-8 program assistance is available from your local Contech representative.
** An NCSPA Corrugated Steel Pipe Design Manual is available from your local Contech representative.
*** NCSPA Design Data Sheet 19 is available from your local Contech representative.

6. Specify Bedding, Backfill and Check Foundation

- Soil envelope under and around structure
- Bedding
- Foundation Requirements
- Backfill envelope - Backfill recommendations

7. Structure End Treatment

- Bevels, Skews
- Headwalls
- Toe-walls and cutoff walls

8. Specify Structure Installation Procedure

- AASHTO Section 26
- ASTM A807 for steel structures, ASTM B879 for Aluminum Structural Plate

9. Material, Design, and Installation Specifications

- AASHTO MULTI-PLATE, SUPER-SPAN, Aluminum Structural Plate, Box Culvert and BridgeCor Material Design and Installation
- Typical Specifications

10. CAD Drawings

- Structure Shape and detail drawings are available to the designer upon request.

These are the typical steps involved in designing a structural plate bridge. This brochure contains specific information about MULTI-PLATE, Aluminum Structural Plate, SUPER-SPAN/ SUPER-PLATE, Aluminum Box Culverts and BridgeCor.
More specific information on each step or topic is available from Contech Engineered Solutions.

| STRUCTURE SHAPE GEOMETRY |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Shapes |  | Sizes=Span $\times$ Rise | Common Uses | Steel | Aluminum | Trade Name |
| Round |  | $5^{\prime}$ to $50^{\prime}-6^{\prime \prime}$ | Culverts, storm sewers, aggregate tunnels, vehicular and pedestrian tunnels and stream enclosures. Functions well in all applications, but especially in those with high cover | x |  | MULTI-PLATE BridgeCor |
|  |  |  |  |  | $\times$ | Aluminum Structure Plate |
| Vertical Ellipse |  | $\begin{aligned} & 4^{\prime}-8^{\prime \prime} \times 5^{\prime}-2^{\prime \prime} \\ & 5^{\prime}+0 \times 27^{\prime}-8^{\prime \prime} \end{aligned}$ | Culverts, storm sewers, service tunnels, recovery tunnels and stream enclosures. Works well in higher cover applications. | x |  | MULTI-PLATE |
|  |  |  |  |  | x | Aluminum Structure Plate |
| Underpass |  | $\begin{gathered} 12^{\prime}-2^{\prime \prime} \times 11^{\prime}-0^{\prime \prime} \\ \text { to } \\ 20^{\prime}-4^{\prime \prime} \times 17^{\prime}-9^{\prime \prime} \end{gathered}$ | Offers efficient shape for passage of pedestrians or livestock, vehicular traffic and bicycles with minimal buried invert. | $\times$ |  | MULTI-PLATE |
|  |  |  |  |  | x | Aluminum Structure Plate |
| Plpe-Arch |  | $\begin{gathered} 6^{\prime}-1 " \times 4^{\prime}-7^{\prime \prime \prime} \\ \text { to } \\ 20^{\prime}-77^{\prime \prime} \times 13^{\prime}-2^{\prime \prime} \end{gathered}$ | Limited headroom. Has hydraulic advantages at low flow levels. Culverts, storm sewer, underpass and stream enclosures. | $\times$ |  | MULTI-PLATE |
|  |  |  |  |  | x | Aluminum Structure Plate |
| Horizontal Ellipse |  | $\begin{gathered} 7^{\prime}-4^{\prime \prime} \times 5^{\prime}-6^{\prime \prime} \\ \text { to } \\ 14^{\prime}-11^{\prime \prime} \times 11^{\prime}-2^{\prime \prime} \end{gathered}$ | Culverts, bridges, low cover applications, wide centered flow, good choice when poor foundations are encountered. | $\times$ |  | MULTI-PLATE |
|  |  |  |  |  | x | Aluminum Structure Plate |
| Arch (single radius) |  | $\begin{gathered} 6^{\prime} \times 1^{\prime}-10^{\prime \prime} \\ \text { to } \\ 54^{\prime}-4^{\prime \prime} \times 27^{\prime}-22^{\prime \prime} \end{gathered}$ | Low clearance, large waterway opening. Aesthetic shapes and open natural bottoms for environmentally-friendly crossings. | $\begin{aligned} & x \\ & x \end{aligned}$ |  | MULTI-PLATE BridgeCor |
|  |  |  |  |  | x | Aluminum Structure Plate |
| Arch (2-radius) |  | $\begin{gathered} 18^{\prime}-5^{\prime \prime} \times 8^{\prime}-4^{\prime \prime} \\ 5^{\prime}-7^{\prime \prime} \times 19^{\prime}-11^{\prime \prime} \end{gathered}$ | Low clearance, large waterway opening. Aesthetic shapes and open natural bottoms for environmentally-friendly crossings. | $\times$ |  | BridgeCor |
| Low-Profile Arch* |  | $\begin{gathered} 20^{\prime}-1^{\prime \prime} \times 7^{\prime}-6^{\prime \prime} \\ \text { +o } \\ 45^{\prime}-0^{\prime \prime} \times 18^{\prime}-8^{\prime \prime} \end{gathered}$ | Culvert, storm sewers, low headroom and large opening. Bridge structures, stream enclosures. Aesthetic shapes and open natural bottoms for environmentally friendly crossings. | $\times$ |  | MULTI-PLATE |
|  |  |  |  |  | x | Aluminum Structure Plate |
| High-Profile * |  | $\begin{gathered} 20^{\prime}-1^{\prime \prime} \times 9^{\prime}-1^{\prime \prime} \\ \text { to } \\ 35^{\prime}-4^{\prime \prime} \times 20^{\prime}-0^{\prime \prime} \end{gathered}$ | Culverts, storm sewers, bridges, Higher rise, large area opening. Open natural bottoms for environmentally friendly crossings. | $\times$ |  | SUPER-SPAN |
|  |  |  |  |  | x | SUPER-PLATE |
| Pear- Arch |  | $\begin{gathered} 23^{\prime}-11^{\prime \prime} \times 23^{\prime}-4^{\prime \prime} \\ \text { to } \\ 30^{\prime}-4^{\prime \prime} \times 25^{\prime}-10^{\prime} \end{gathered}$ | Railroad underpasses or large clearance areas. | $\times$ |  | SUPER-SPAN |
|  |  |  |  |  |  |  |
| Pear |  | $\begin{gathered} 23^{\prime}-8^{\prime \prime} \times 25^{\prime}-5^{\prime \prime} \\ \text { to } \\ 29^{\prime \prime}-11^{\prime \prime} \times 31^{\prime}-33^{\prime} \end{gathered}$ | Railroad underpasses or large clearance areas. | x |  | SUPER-SPAN |
|  |  |  |  |  |  |  |
| Horizontal Ellipse |  | $\begin{gathered} 19^{\prime}-4^{\prime \prime} \times 12^{\prime}-9^{\prime \prime} \\ \text { to } \\ 37^{\prime}-2^{\prime \prime} \times 22^{\prime}-2^{\prime \prime} \end{gathered}$ | Larger culverts and bridges. Low headroom, wide-centered flow, good choice when poor foundations are encountered. | x |  | SUPER-SPAN |
|  |  |  |  |  | x | SUPER-PLATE |
| Box Culvert |  | $\begin{gathered} 8^{\prime}-9^{\prime \prime} \times 2^{\prime}-6^{\prime \prime} \\ \text { to } \\ 35^{\prime}-3^{\prime \prime} \times 13^{\prime}-7^{\prime \prime} \end{gathered}$ | Very low, wide bridges, culverts and stream enclosures, with limited headroom. Functions well as a fast small-span bridge replacement. | $\times$ |  | BridgeCor |
|  |  |  |  |  | $\times$ | Aluminum Box Culvert |
| Elliptical/Circular Arch ** |  | $12^{\prime}$ to $102{ }^{\prime}$ | Culverts, bridges, tunnels, wetlands crossings, overpass/ underpass, underground containment, wine/cheese cellars and shelters. |  |  | $\begin{gathered} \text { CON/SPAN® } \\ \text { BEBO® } \\ \text { (concrete) } \end{gathered}$ |
| $\begin{aligned} & \text { H } 20 \text { Bridge ** } \\ & \text { Pedestrian ** } \end{aligned}$ |  | spans up to $300^{\prime}$ spans up to $300^{\prime}$ | County, city, parks, industrial complexes. Recreational, overpasses, industrial conveyor, pipe support. | $\times$ |  | U.S. Bridge ${ }^{\circledR}$ Vehicular Truss Continental ${ }^{\text {® }}$ Pedestrian Truss |

[^0]
## Selection of Structure Shape

Contech manufactures and supplies structural plate in a wide variety of structure shapes and sizes in both galvanized steel and aluminum alloy. The large selection of structure types ensures that a designer will be able to select the optimum structure for virtually any application from low cover situations to extreme cover heights and from pedestrian underpasses to grade separations for airport runways or railroad passages.

The structures listed on the prior page are generally configured for use in specific drainage or traffic passage applications. They are prioritized from top to bottom. This will ensure the most efficient usage and best economy. For example, a designer should first check to see if a round structure will fit. If there is inadequate headroom for a round structure, proceed to a pipe-arch, horizontal ellipse, or arch and on to Aluminum Box Culverts. If a round structure is not large enough, consider a SUPER-SPAN type structure. More detailed structure dimensions and information can be found in later sections of this document.

Following are some tips on structure shape and size selection:
$\checkmark$ It is usually best to select a shape that most closely matches the shape of the drainage channel. For example, a deep narrow channel will accept a round structure. Horizontal ellipses, low profile arches and Aluminum Box Culvert shapes are best suited to relatively wide, shallow channels.
$\checkmark$ Look first at the end area requirement in square feet for the structure and divide the number by the vertical distance from the streambed to the surface elevation less approximately $1.5^{\prime}$ to $3.0^{\prime}$ for fill cover over the structure. This will somewhat underestimate the approximate minimum span required depending upon the structure shape.
$\checkmark$ Look for the most efficient structure in terms of reducing design loads. For Aluminum Box Culverts, choose a structure that meets the hydraulic requirements and provides for cover of $3^{\prime}-4^{\prime}$. A taller structure which minimizes cover may be less cost-effective than one of similar span with slightly higher cover.
$\checkmark$ For other plate structures:

- Where fill over the structure is high, try to utilize the tallest structure feasible to minimize cover. As cover increases, so does gage as well as footing sizes.
- Where fill over the structures is low, choose a structure that maintains the minimum allowable cover.


## Additional Considerations

In addition to simple geometric and hydraulic concerns, the designer should consider other parameters that may influence structure type, shape and material including:

## - Very High Fill

Fills over 30' should warrant the consideration of Keyhole Slot MULTI-PLATE ${ }^{\circledR}$ discussed on page 16.

## - Pipe Structure versus Arch on Footings

In general, a pipe with a full invert or pipe with a buried invert is preferable in terms of cost over an arch because of the elimination of concrete footings. However, many regulations prefer natural, undisturbed stream bottoms. In this case, an arch on footings is typically less expensive than a traditional bridge.

## - Bearing Capacity

See sections on individual structure types for recommendations on minimum bearing capacity and footings designs. Pipe arch design should include considerations of applied corner bearing pressure.

## - Flow Characteristics

If flow is to be particularly abrasive, the designer should consider a natural invert (arch or buried invert), heavier invert plates, an aluminum structure, or preferably, a paved invert.

## - Corrosive Soils

Analyze structure life projections based upon the CALTRANS/ A.I.S.I. method. If design life is not met using galvanized steel, consider asphalt coating the steel, adding a concrete field paved invert or using aluminum instead. See page 12 for recommendations for protection from de-icing salts.

## - Corrosive Effluents

Analyze structure invert life projections based upon the CALTRANS/A.I.S.I. method. If design life is not met using galvanized steel, consider either heavier gage invert plates, aluminum, paved invert, or natural invert. In particularly corrosive situations an arch on elevated footing walls (pedestal walls) may be necessary.

## Scour

If scour is a concern, a pipe structure or pipe structure with a buried invert may be more desirable than an arch. The invert eliminates footings subject to scour. Also, arches with partially buried structure legs (and footings) may satisfy scour depth. Often, when an arch on footings must be used, protecting the footings with rip-rap, sheet piling, permanent erosion control, hard armor interlocking blocks, etc., is more cost effective than deep footings or footings on piles. Scour analysis is outside the scope of this brochure.

FHWA Hydraulics Engineering Circular HEC 18 outlines the design for scour. FHWA Hydraulics Engineering Circular 23 outlines the design procedures for scour counter measures.


Protect footings from scour

## Selection of Structure Based Upon Clearance Requirements

The following describes the process of selecting a structure with sufficient clearance for the passage of vehicular or pedestrian traffic.

It should be noted that the shape of finished corrugated metal structures may differ from the nominal dimensions described in literature. For instance, taller single radius arches may "peak" slightly during backfilling, thus slightly decreasing the effective span.

If clearance tolerance is critical, it is recommended that a slightly larger structure be selected or that the structure shape be monitored during erection and backfilling. Proper control of compaction and the use of high quality granular backfill material will minimize structure movement during backfilling. Contact your Contech representative for assistance or recommendations regarding monitoring and the use of particular shapes.

MULTI-PLATE ${ }^{\circledR}$, Aluminum Structure Plate vertical ellipses and underpass shapes are configured specifically for vehicular and pedestrian traffic. The structure invert is often "paved" to provide a smooth surface.
While arch structures often appear to be the best choice for many applications, the same shape in a round or elliptical shape may be more economical due to the elimination of footings. For example, a round structure or horizontal ellipse with the invert buried and paved are often used in lieu of an arch for grade separation structures.


Horizontal ellipse SUPER-SPAN at Lowes Motor Speedway

## Designing For Service Life

After a structure shape and size is selected based upon hydraulic or clearance requirements and the structure gage is determined, the designer should normally proceed to an analysis of the possible effects of the environment on structure performance. This may lead the designer to specific selections of material, structure type, coating, or invert protection.

Structure life can be affected by the corrosive action of the backfill in contact with the outside of a structure or more commonly by the corrosive and abrasive action of the flow in the invert of the structure. The design life analysis of the structure should include a check for both water side and soil side environments to determine which is most critical or which governs structure life.


The choice of material or structure type can be extremely important to service life. For example, if it is determined that water flowing through a structure is projected to limit the life of the invert through abrasive or corrosive action, an arch may be used with a natural invert or the invert may be paved. Other possible remedies may exist depending upon other structure requirements.

## Prediction of Structure Life Limited by Corrosion

Galvanized steel structure plate has been used in the United States since 1931. Aluminum Structure Plate has been in use since the early 1960's. Tens of thousands of structures are in use in a wide variety of applications and environments. This wealth of experience provides unsurpassed "in-the-ground" performance knowledge. Several rational methods exist for determination of the effects of corrosion upon galvanized steel and aluminum drainage structures. Numerous federal agencies, including the Federal Highway Administration and U.S. Army Corp of Engineers as well as a large number of state departments of transportation, have published guidelines on the subject. All have valuable information pertinent to possible corrosive effects on both steel and aluminum materials.

## Galvanized Steel MULTI-PLATE ${ }^{\circledR}$

With regard to galvanized steel MULTI-PLATE, this brochure will follow the guidelines set forth by the A.I.S.I. The A.I.S.I. design method grew out of a California Department of Transportation (CALTRANS) study which preformed an inspection of over 7,000 galvanized steel drainage structures in the state of California for the purposes of developing a reliable method for the prediction of the life of corrugated galvanized steel structures. The data collected reflected the combined effects of corrosion and a wide range of abrasive levels. CALTRANS defined the end of the structure life to be coincident with the first perforation of approximately $12 \%$ metal loss in the invert.

Many state DOT's found the CALTRANS method to be overly conservative in that it underestimated the average observed service life of galvanized steel structures in service in their states. This was primarily due to the fact that a gravity flow drainage structure of any kind functions properly well beyond the occurrence of the first perforation.

In addition, many of the structures surveyed in California were in mountainous areas and, therefore, were affected by above average abrasion. R.F. Stratful, based upon research by the U.S. Dept. of Weights and Measures upon corrosion rates, refined the method developed by CALTRANS and produced a reliable means of predicting the average effective invert service life of a galvanized steel drainage structure - the end of average effective service life being determined by approximately $25 \%$ metal loss in the invert. The basis for this being that if the in-service time that it takes for a $12 \%$ metal loss produces the first perforation, then the structure should function properly for at least twice that period. Also, a $25 \%$ metal loss still provides for remediation such as invert paving.

An important factor when choosing a design method, either CALTRANS or A.I.S.I., is knowledge of the structure backfill type. A structure backfilled with very fine material may be affected by the loss of this material through perforations. Thus, the CALTRANS method may be valid. If the backfill is more granular, which is usually the case with plate structures, then first perforation is probably inconsequential and, therefore, the A.I.S.I. method would be more appropriate. Recent inspections of 30 -year-old SUPER-SPANs have revealed little, if any metal loss. Even the A.I.S.I. method would predict some metal loss. Because of this, the remainder of this discussion will focus upon the A.I.S.I. design method.

The A.I.S.I. chart for estimating average invert life is shown on the following page.

Minimum Resistivity ( $R$ ) ohm cm


To further validate the use of the A.I.S.I. design method, galvanized steel plate structures feature a 3 oz . per square foot galvanized coating versus the 2 oz . coating found on the structures inspected in the original CALTRANS study. In addition, larger plate structures usually experience lower velocity flows and, hence, less potential for abrasion than the smaller culvert structures from the CALTRANS study.

The designer should note that other factors will affect the rate of metal loss. The primary factor is the presence of dissolved salts such as CaCO 3 and MgCO 3 . Total hardness is a measure of the level of dissolved salts and defined water runoff as hard or soft water.

Hardness levels greater than $300 \mathrm{mg} / \mathrm{L}$ indicate dissolved salts (hard water) of a level that will cause the formation of a mineral "scale" on the galvanized surface that will provide excellent protection and increased service life in the absence of abrasion. Inspections have shown 50-year-old structures with mineral scale and pristine metal conditions beneath.

Hardness levels below $300 \mathrm{mg} / \mathrm{L}$ warrant further consideration by the designer and the possible use of coatings, invert protection/paving or aluminum.

In general, the recommended environmental range for use of galvanized steel Structural Plate that will provide a minimum service life of 50 years is:

$$
\begin{array}{ccc}
\text { water side } & \& & \text { soil side } \\
6 \leq \mathrm{pH} \leq 10 & & 6 \leq \mathrm{pH} \leq 10
\end{array}
$$

$$
2000 \text { ohm- } \mathrm{cm} \leq R \leq 8000 \text { ohm- }-\mathrm{cm}^{*}
$$

* Values greater than 8000 ohm-cm for water side resistivity may indicate low level of dissolved salts (soft water). Water hardness should be tested. Invert protection may be required to meet the designated service life.



## Aluminum Structural Plate

Studies similar to those conducted by CALTRANS have been performed upon a large number of Aluminum Structural Plate installations for the same purpose although none have produced a mathematical model like that for galvanized steel. Aluminum loss rates have been so low as to preclude a reliable model.

Aluminum alloy reacts much differently than galvanized steel when in contact with air, soil, and water. Instead of zinc/steel system of galvanic protection, aluminum resists corrosion by a passive formation of a very tenacious aluminum-oxide layer on its surface. This oxide layer has been shown in field and laboratory observation to be stable in an environment of pH between 4 and 9 and resistivity greater than 500 ohm-cm. Within this range, corrosion rates are minimal and prediction of service life is a matter of assigning a pit rate based upon laboratory testing. Conservatively, a pit rate based on 0.001 " $/ \mathrm{yr}$ may be used.
In this case:
$0.100^{\prime \prime}$ thick plate $0.001^{\prime \prime} / \mathrm{yr}=100 \mathrm{yrs}$ design life .
Actual field observations of aluminum alloy pipe (ALCLAD) and Aluminum Structural Plate support this prediction.

In tidal brackish and saltwater environments, Aluminum Structural Plate will perform well if backfilled with freedraining material. The pH and resistivity requirements outlined previously must also be met. Sea water normally exhibits a $\mathrm{pH}=7.5-8.0$ and resistivity $<100 /$ ohm-cm, but given the neutral pH and a free draining backfill, Aluminum Structural Plate still performs well.

Note: For more detailed information on the subject of corrosion or copies of the referenced documents or guidelines, contact your Contech representative.

## Abrasion

The potential for metal loss in the invert of a drainage structure due to abrasive flows is often overlooked by designers and its effects are often mistaken for corrosion. Environments conducive to abrasive flows are well defined but due to the periodic nature of this event, it is easy to miss.

Three factors must combine to cause invert abrasion:

- Abrasive bedload
- Sufficient velocity to carry the bedload
- Flow duration and frequency

Examples of abrasive materials include but are not limited to sands, gravels, and stone. The designer should not underestimate the abrasive action of sand transported in sustained flows. When flow velocities reach approximately 5-6 feet-per-second, sand and gravels can become mobile or suspended.

Most commonly, abrasive bedloads remove protective mineral scale and produce oxidation on galvanized steel which will accelerate corrosion. Upstream stilling basins that allow abrasive particles to settle or drop out prior to entering the structure can be very effective in extending the service life.

Guidelines for abrasion levels are excerpted from the FHWA Memorandum on Design Guidance and Specification Changes for Drainage Pipe Alternative Selection and are shown on the next page.

Both of these factors, velocity and abrasiveness, may be present at a particular site. However, if the flow necessary to carry the bedload occurs only a few times during the life of the structure, abrasion may not be a concern. The designer should refer to the 2- or 5-year event velocity and then use this to decide if abrasion is a valid concern.

Should abrasion be determined to be a limiting factor in structure life, several solutions are available to the designer. These solutions include:

- Use of a structure with a buried invert
- Use of an arch structure
- Concrete invert pavement (see page 12)
- Heavier gage invert plates
- Stilling basins near the invert

Note: Aluminum performs better than galvanized steel when subjected to abrasion. In some cases, the formation of the oxidized steel layer (in hard water) is removed by abrasion, exposing the galvanized coating beneath. After years of abrasion have taken place, the protective galvanized coating is abraded away and corrosion of the bare steel begins. This corrosion/abrasion cycle continues for the life of the structure.

Aluminum may lose its oxide layer when abraded away but it quickly reforms at low flows, therefore limiting corrosion. Aluminum does not have a protective coating to lose after years of abrasive flow.

This is not meant to suggest that Aluminum Structural Plate should be used in heavily abrasive environments. However, its performance can be expected to be superior to galvanized steel.

## Addifional Service Life Considerations

## Dissimilar metals

Metals with a substantial difference in electrical potential should be insulated from each other. Electrical potential may be established by referring to the electromotive scale. The only significant concern with regard to structural plate is the use of "black" steel in conjunction with aluminum. Black steel should not be in contact with aluminum. Hot Dipped Galvanized steel is compatible with Aluminum Structural Plate.

## Concrete or grout in contact with aluminum

During the relatively short period while concrete cures, minor etching ( $<0.001^{\prime \prime}$ ) of the surface of the plate will occur. If the designer is concerned with cosmetic etching of the aluminum, the surface may be coated with asphalt or primer paint.

## De-icing salts

The potential for use of de-icing salts on roadway surfaces above structural plate must be addressed during the design phase. Calcium chloride and magnesium chloride as well as other de-icing materials can cause corrosion of galvanized steel and aluminum.

It is recommended that the designer consider the use of either an asphalt coating on the exterior of the structure, a layer of impermeable clay over the structure or a polymeric membrane over the structure. Details for each of these solutions are presented on the following pages.

## FHWA Memorandum on

## Design Guidance and Specification Changes for Drainage Pipe Alternative Selection

The durability and service life of a drainage pipe after installation is directly related to the environmental conditions encountered at the site and the type of materials and coatings from which the culvert was fabricated. Two principal causes of early failure in drainage pipe materials are corrosion and abrasion. The environmental damage caused by corrosion and abrasion can be delayed by the type of materials, coatings and invert protection.

It is Federal Lands Highway (FLH) policy to specify alternative drainage pipe materials on projects where feasible and to comply with the provisions of the Federal-
Aid Policy Guide Section 611.411 (d). All permanent drainage pipe installations shall be designed for a minimum of 50 years with a maintenance-free service life. A shorter service life may be used for temporary installations, and a longer service life may be considered in unusual situations.
All suitable pipe materials, including reinforced concrete, steel, aluminum and plastic pipe shall be considered as alternatives on FLH projects. The portion of this pipe selection criteria covering metal pipe complies with the guidance contained in Federal Highway Administration (FHWA) Technical Advisory T 5040.12 dated October 22, 1979, and incorporates information contained in FHWA-FLP-91-006, Durability of Special Coatings for Corrugated Steel Pipe.
Abrasion: An estimate of the potential for abrasion is required at each pipe location in order to determine the need for invert protection. Four levels of abrasion are referred to in this guidance and the following guidelines are established for each level:

- Level 1 nonabrasive conditions exist in areas of no bed load and very low velocities. This is the condition assumed for the soil side of drainage pipes.
- Level 2 low abrasive conditions exist in areas of minor bed loads of sand and velocities of 1.5 meters per second ( 5 feet per second) or less.
- Level 3 moderate abrasive conditions exist in areas of moderate bed loads of sand and gravel and velocities between $1.5 \mathrm{~m} / \mathrm{s}$ and $4.5 \mathrm{~m} / \mathrm{s}$ ( 5 and 15 fps ).
- Level 4 severe abrasive conditions exist in areas of heavy bed loads of sand, gravel, and rock and velocities exceeding $4.5 \mathrm{~m} / \mathrm{s}$ ( 15 fps ).

These definitions of abrasion levels are intended as guidance to help the designer consider the impacts of
bedload wear on the invert of pipe materials. Sampling of the streambed materials is not required, but visual examination and documentation of the size of the materials in the streambed and the average slope of the channel will give the designer guidance on the expected level of abrasion. Where existing culverts are in place in the same drainage area, the conditions of inverts should also be used as guidance. The expected stream velocity should be based upon a typical flow and not a 10- or 50-year design flood.

Corrosion: Alkalinity/Acidity ( pH ) and Resistivity-
Determinations of pH and resistivity are required at each pipe location in order to specify pipe materials capable of providing a maintenance free service life. The samples shall be taken in accordance with the procedures described in AASHTO T 288 and T 289. Samples should be taken from both the soil and water side environments to ensure that the most severe environmental conditions are selected for determining the service life of the drainage pipe. Soil samples should be representative of backfill material anticipated at the drainage site. Avoid taking water samples during flood flows or for two days following flood flows to insure more typical readings. In locations where streams are dry for much of the year, water samples may not be possible or necessary. In areas of known uniform pH and resistivity readings, a random sampling plan may be developed to obtain the needed information.

In corrosive soil conditions where water side corrosion is not a factor, consider specifying less corrosive backfill material to modify the soil side environment. The mitigating effect of the specified backfill should be taken into account in making alternative pipe materials selections in situations where soil side conditions control.

## Adjustments for Abrasion

Once the minimum structural gage is selected and service life requirement checked on "The AISI Chart for Estimating Average Invert Life" on page 8, adjustments should be made based on the abrasion potential of the site.

## Steel

At non-abrasive or low abrasive sites, no additional protection is needed. At sites that are moderately abrasive, increase the thickness of the material by one standard thickness or add invert protection like a concrete paved invert. At severely abrasive sites, increase the thickness of the material by one standard thickness and add a concrete paved invert.

## Aluminum

At non-abrasive, low abrasive or moderately abrasive sites, no additional protection is needed. At severely abrasive sites, increase the thickness of the material by one standard thickness and add a concrete paved invert.


## Structural Design of Corrugated Metal Structures

## Gage (Mefal Thickness) Defermination and Resulting Safety Factors

According to the American Association of State Highway and Transportation Officials (AASHTO) Standard Specifications for Highway Bridge, corrugated metal plate structures are "Soil - Corrugated Metal Structure Interaction Systems." The implication is that plate structures are composites comprised of the surrounding soil envelope which act in conjunction with the structures' inherent strength to support traffic and soil loads.

Design methods for corrugated metal plate structures are well established and provide the designer with uncomplicated, conservative procedures. Current AASHTO design procedures also address foundation, backfill and end treatment. (See page 29 for listing of all design specifications.)

The basic plate structure design process for the determination of the structure gage consists of:

1. Determine the backfill soil density by the soil structure.
2. Calculate the design pressure applied by the soil column and live load.
3. Compute the compression in the structure wall.
4. Determine the required thickness based upon checks for wall yielding and buckling (using the correct corrugated section properties).
5. Check for sufficient bolted longitudinal (plate to plate) seam strength.
6. Check for minimum stiffness required for proper handling, assembly, and installation.

## Quantifying Live and Dead Loads Applied to the Structure

Live loads consist of traffic loads applied to the surface or roadway above the structure. These loads also consider the effect of impact loads. Live loads reaching the structure diminish with increasing heights of cover. This manual typically considers $\mathrm{H} 2 \mathrm{O}, \mathrm{H} 25, \mathrm{HS} 20$, and HS 25 highway loads. Cooper railroad loads (E-80) are addressed in the Amercian Railroad Engineering and Maintenance of Way Association (AREMA) specification which is analogous to the procedure herein. Airport loading and off-highway loads such as mining equipment are special. Contech is available to assist the designer in the evaluation of these special loads on the structure.

Dead loads are those developed by the soil fill above the structure plus those of any stationary surcharge loads such as buildings. Dead loads are assumed to increase at a one-to-one ratio with depth.

Dead Load (DL) $=\mathrm{w} \times \mathrm{H}$
Where: $\mathrm{w}=$ unit weight of soil $\left(\mathrm{lb} / \mathrm{ft}^{3}\right)$

$$
\begin{aligned}
& \mathrm{H}=\text { Height of fill over structure }(\mathrm{ft}) \\
& \mathrm{DL}=\text { Dead load pressure }\left(\mathrm{lb} / \mathrm{ft}^{2}\right)
\end{aligned}
$$

Live loads reaching the structure are more complicated to determine. Using information provided by AASHTO, the National Corrugated Steel Pipe Association (NCSPA) has prepared a very comprehensive method for determination of the loads reaching the corrugated metal structure.

## NCSPA - Drainage Technology Bulletin November 1991

Section 3.3 of AASHTO specifications assume a rectangular tire contact pattern with an area ( $A$, square inches) equal to 1 percent of the wheel load ( P, pounds).
$P$ is $1 / 2$ of the axle load and should include any impact. The contact area is assumed to have a width (w) equal to 2.5 times its length (L) in the direction of traffic. Section 3.8.2.3 provides impact loads (I) for culverts with cover (H) less than 3 feet according to the following schedule:

$$
\begin{array}{ll}
H<1^{\prime}-0^{\prime \prime} & I=30 \% \\
1^{\prime}-1^{\prime \prime}<H<2^{\prime}-0^{\prime \prime} I=20 \% \\
2^{\prime}-1^{\prime \prime}<H<2^{\prime}-11^{\prime \prime} \quad I=10 \%
\end{array}
$$

Section 6.4 of AASHTO provides for the dissipation of the live load pressure depth assuming that the load is distributed over the base of a truncated prism with side slopes of 1 vertical to 0.875 horizontal (as seen on the next page).

|  | TABLE 1. <br> Height of Cover <br> (ft) |  |  | H20 Loading <br> (psf) | H25 Loading <br> (psf) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 2270 | 2580 |  |  |  |
| 2 | 850 | 1000 |  |  |  |
| 3 | 420 | 510 |  |  |  |
| 4 | 285 | 350 |  |  |  |
| 5 | 210 | 250 |  |  |  |
| 6 | 160 | 190 |  |  |  |
| 7 | 120 | 150 |  |  |  |
| 8 | 100 | 120 |  |  |  |
| 9 | -- | 100 |  |  |  |



AASHTO

- Tire contact area, A (sq. in.), is related to the wheel load, P (lbs, including impact), By

$$
A=0.01 P
$$

- Values of P are: $\quad(\mathrm{H}=$ Height of Cover)

$$
\begin{array}{ll}
H<1^{\prime}=0^{\prime \prime} & H 20=1.3 \times 16000=20,800 \\
& H 25=1.3 \times 20000=26,000 \\
1^{\prime}-1^{\prime \prime}<H<2^{\prime}-0^{\prime \prime} & H 20=1.2 \times 16000=19,200 \\
& H 25=1.2 \times 20000=24,000 \\
2^{\prime}-1^{\prime \prime}<H<2^{\prime}-11^{\prime \prime} & H 20=1.1 \times 16000=17,600 \\
& H 25=1.1 \times 20000=22,000 \\
H>2^{\prime}-11^{\prime \prime} & H 20=16,000 \\
& H 25=20,000
\end{array}
$$

- Length, L (inches) and Width, w (inches), of the contact area are related by

$$
\begin{aligned}
& A=L w \\
& w=2.5 L
\end{aligned}
$$

Therefore,

$$
w=\sqrt{0.025 P}
$$

- Depth, $\mathrm{h}^{\prime}$ (inches), to intersection of pressure zones under the two wheels is: $\mathrm{h}^{\prime}=\left(72^{\prime \prime}-\mathrm{w}\right) / 1.75$
- Pressure, $p$ (psf), at the top of pipe for a height of cover, $h$ (inches) is:

$$
\begin{aligned}
p= & 144 \mathrm{P} /((1.75 h+w)(1.75 h+L)) \\
& \text { When } h<h^{\prime}
\end{aligned}
$$

- For covers greater than $h^{\prime}$, the pressure zones overlap and the pressure is:

$$
p=288 P /((1.75 h+w+72)(1.75 h+L))
$$

$$
\text { When } h>h^{\prime}
$$

Table 1 summarizes these live load calculations for varying Heights of Cover. (See page 13.)

## AASHTO Section 12: Design Equations (Service Load Design)

- Design Pressure $P$

P = Live load + Dead Load (lb/sq ft)
Live load (table 1)
Dead load (height of cover $x$ unit weight of soil)

- Wall Thrust
$\mathrm{T}_{\mathrm{s}}=\mathrm{P} \times \mathrm{s} / 2$
$\mathrm{T}_{\mathrm{s}}=$ wall thrust (lb/ft)
$\mathrm{s}=$ dsiameter or span (ft)
- Wall area
$A=T_{s} / f_{a}$
$\mathrm{T}_{\mathrm{s}}=$ wall thrust ( $\mathrm{lb} / \mathrm{ft}$ )
$f_{a}=$ allowable stress (min. yield point f.s. $=2$ ) $\mathrm{lb} / \mathrm{sq}$ in)
- Buckling

If $f_{c r}$ is less than $f_{a}$, Area (A) must be recalculated using $f_{c r}$ in lieu of $f_{a}$.
Where:
$r=$ radius of gyration (inches)
If $s<\frac{r}{k} \sqrt{\frac{24 E_{M}}{f_{u}}}$
then $f_{c r}=f_{u}-\frac{f_{u}{ }^{2}}{48 E_{M}}(k s / r)^{2}$
If $s>\frac{r}{k} \sqrt{\frac{24 E_{M}}{f_{u}}}$
then $f_{c r}=\frac{12 E_{M}}{(\mathrm{ks} / \mathrm{r})^{2}}$
$f_{u}=$ min. tensile strength (psi)
$f_{c r}=$ critical buckling strength (psi)
$\mathrm{k}=$ soil stiffness factor $=0.22$
$s=$ pipe diameter or span (inches)
$\mathrm{E}_{M}=$ modulus of elasticity of metal (psi)

- Seam Strength
ss $=\mathrm{T}_{\mathrm{s}} \times$ S.F.
Safety factor $=3$
ss $=$ seam strength $=\mathrm{lb} / \mathrm{ft}$
- Flexibility Factor
$\mathrm{FF}=\mathrm{s}^{2} / \mathrm{E}_{\mathrm{M}} \mathrm{I}$
FF= Flexibility factor (in/lb)
$s=$ pipe diameter or max span (in)
$\mathrm{E}_{\mathrm{M}}=$ modulus of elasticity of metal (psi)
$\mathrm{I}=$ moment of inertia (in ${ }^{4} / \mathrm{in}$ )
Limiting Flexibility Factor Values
a) Steel 6" $\times 2$ " corrugations
round $=0.02$
pipe-arch $=0.03$
arch $=0.03$
b) Aluminum $9^{\prime \prime} \times 21 / 2^{\prime \prime}$ corrugations
round $=0.025$
pipe-arch $=0.036$
arch $=0.036$


## When Seam Strength Governs Structure Design

Should it be found through analysis that the seam strength of a structure is the limiting factor, which can occur when fill heights become great, the structure gage may be forced to undesirable levels to provide greater seam strength. In some cases, the seam strength provided by the standard four bolt per foot seam may not be sufficient to handle the load. In these cases, the designer may wish to consider the use of six or eight bolts per foot.

The following table provides seam strengths for four, six and eight bolts per foot.

| TABLE 2. <br> ULTIMATE SEAM STRENGTH OF BOLTED STEEL STRUCTURAL PLATE LONGITUDINAL SEAMS IN POUNDS PER FT OF SEAM |  |  |  |
| :---: | :---: | :---: | :---: |
| Specified Thickness in. | $6^{\prime \prime} \times 2^{\prime \prime}$ <br> Corrugation |  |  |
|  | 4 Bolts Per Ft. | 6 Bolts Per Ft. | 8 Bolts Per Ft. |
| 0.111 42,000 |  |  |  |
| 0.140 | 62,000 |  |  |
| 0.170 | 81,000 |  |  |
| 0.188 | 93,000 |  |  |
| 0.218 | 112,000 |  |  |
| 0.249 | 132,000 |  |  |
| 0.280 | 144,000 | 180,000 | 194,000 |
| 0.318 | 235,000 |  |  |
| 0.375 |  | 285,000 |  |
| Notes: |  |  |  |
| 1. Bolts used are $3 / 4^{\prime \prime}$ diameter - high strength bolts, meeting ASTM A 449 . |  |  |  |
| 2. Bolts and nuts also used for connecting arch plates to receiving angles and structural reinforcement to structural plates. <br> 3. $7 / 8^{\prime \prime}$ diameter bolts may be required with thicker plates. |  |  |  |


"The Chief" a 5,000,000 lb. drag line over steel SUPER-SPAN ${ }^{\text {™ }}$ at Peabody Coal in Zanesville, Ohio
$\left.\begin{array}{cc}\text { TABLE 3. } \\ \text { ULTIMATE SEAM STRENGTH } \\ \text { OF BOLTED ALUMINUM STRUCTURAL PLATE LONGITUDINAL SEAMS } \\ \text { IN POUNDS PER FT OF SEAM }\end{array}\right]$

## Notes:

1. Bolts are $3 / 4^{\prime \prime}$ diameter meeting ASTM A304


24'-0" diameter steel MULTI-PLATE ${ }^{\circledR}$ under 60 feet of fill owned by VDOT in Dryden, Virginia

## Keyhole Sloł MULTI-PLATE® Structures Under High Fill

Standard MULTI-PLATE can be designed to handle very high fill heights. The ability to deflect under load produces soil arching resulting in reduced design pressure. A modified version of MULTI-PLATE, Key-Hole Slot MULTI-PLATE, is specifically designed to handle high fill heights by use of a special bolted seam that yields or slips under load. (See diagram below).


Figure 2—Key-hole slot MULTI-PLATE ${ }^{\circledR}$ at work
This controlled yielding action in the structure seams decreases the structure circumference, promoting a high degree of soil arching over the structure. For these typically deeper installations, A-1 backfill per AASHTO M-145 is desired as backfill for any pipe or flexible structures and to gain the load carrying capacity for rigid structures.

While specific design criteria must be applied to any project, the use of Key-Hole Slot MULTI-PLATE versus standard MULTI-PLATE can decrease the gage (material thickness) by one to three gages. A CALTRANS deep burial study compared standard MULTI-PLATE to Key-Hole Slot MULTI-PLATE and found that the average thrust created at the springline level of the Key-Hole Slot structure was approximately $50 \%$ of standard structure.

This reduction in thrust in turn reduces the required seam strength, and therefore, the structure wall gage or thickness. The designer is urged to contact a Contech representative for additional information on Key-Hole Slot MULTI-PLATE.


High Covers made easy with Key-Hole Slot MULTI-PLATE ${ }^{\circledR}$

## Section Properties

| TABLE 4. STEEL CONDUITS |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| 6" $\times 2$ 2" Corrugations |  |  |  |  |
| Gage | Thickness (inches) | $\underset{(s q \cdot i n / f t)}{A_{s}}$ | (inches) | $\begin{gathered} 1 \times 10^{-3} \\ \text { (in. }{ }^{4} / \mathrm{in} . \text { ) } \end{gathered}$ |
| 12 | 0.111 | 1.556 | 0.682 | 60.411 |
| 10 | 0.140 | 2.003 | 0.684 | 78.175 |
| 8 | 0.170 | 2.449 | 0.686 | 96.163 |
| 7 | 0.188 | 2.739 | 0.688 | 108.000 |
| 5 | 0.218 | 3.199 | 0.690 | 126.922 |
| 3 | 0.249 | 3.650 | 0.692 | 146.172 |
| 1 | 0.280 | 4.119 | 0.695 | 165.836 |
| 5/16 | 0.318 | 4.671 | 0.698 | 190.000 |
| 3/8 | 0.375 | 5.613 | 0.704 | 232.000 |


| TABLE 5. <br> ALUMINUM CONDUITS |  |  |  |
| :---: | :---: | :---: | :---: |
|  | 9" $\times 2$ 1/2" Corrugations |  |  |
| Thickness (inches) | $\begin{gathered} A_{s} \\ (\mathrm{sq} . \mathrm{in} / \mathrm{ft}) \end{gathered}$ | $\begin{gathered} \stackrel{r}{4} \\ \text { (inches) } \end{gathered}$ | $\begin{gathered} 1 \times 10^{-3} \\ \text { (in. }{ }^{4} / \mathrm{in} . \text { ) } \end{gathered}$ |
| 0.100 | 1.404 | 0.8438 | 83.065 |
| 0.125 | 1.750 | 0.8444 | 103.991 |
| 0.150 | 2.100 | 0.8449 | 124.883 |
| 0.175 | 2.449 | 0.8454 | 145.895 |
| 0.200 | 2.799 | 0.8460 | 166.959 |
| 0.225 | 3.149 | 0.8468 | 188.179 |
| 0.250 | 3.501 | 0.8473 | 209.434 |

Steel Structural Plate Pipe, Pipe-Arch, and Arch
Material Requirements-AASHTO M 167

|  | TABLE 6. <br>  <br>  <br> $\mathrm{f}_{\mathrm{u}}$ | MECHANICAL PROPERTIES FOR DESIGN |
| :---: | :---: | :---: |
| Minimum <br> Tensile | Minimum <br> Strength <br> (psi) | Yield <br> Point <br> (psi) |
| 45,000 | $\mathrm{E}_{\mathrm{m}}$ <br> Mod. of <br> Elast. <br> (psi) |  |

Aluminum Structural Plate Pipe, Pipe-Arch, and Arch Material Requirements-AASHTO M 219, Alloy 5052 TABLE 7.
MECHANICAL PROPERTIES FOR DESIGN

|  | $f_{u}$ <br> Minimum <br> Tensile <br> Strength <br> (psi) | $\mathrm{f}_{\mathrm{y}}$ <br> Minimum <br> (inchess) | Yield <br> Point <br> (psi) |
| :---: | :---: | :---: | :---: |

## AASHTO Section 12

## (Service Load Design)

## Design Examples

## Example 1

Given: $\quad$ Pipe diameter $=22^{\prime}$ Round (Steel)
Height of cover $=10^{\prime}$
Live load, $\mathrm{LL}=\mathrm{H} 20$
Backfill $=$ Compacted 90\% AASHTO T-99
A-1, A-2, A-3

## Solution:

1. Design Pressure $P$ (refer to Table 1):

10' of cover, Live Load $=0$
Dead Load $=\mathrm{H}\left(10^{\prime}\right) \times$ soil unit weight ( 120 pcf )

$$
\text { Therefore } P=1200 \text { psf }
$$

2. Wall Thrust:

Ts $=P \times \frac{\text { Span }}{2}=1200 \mathrm{psf} \times \frac{22^{\prime}}{2}=13,200 \mathrm{lb} / \mathrm{ft}$.
3. Wall Area:
$A=T_{s} / f_{a}$
Where: ${ }^{\mathrm{f}_{a}} \quad \mathrm{~T}_{\mathrm{s}}=$ Wall Thrust
$\mathrm{f}_{\mathrm{a}}=$ allowable stress
(minimum yield point F.S. $=2$ )

Therefore:
$f_{a}=\frac{f_{y}}{2}=\frac{33,000}{2}=16,500 \mathrm{psi}$
$A=\frac{13,200 \mathrm{lb} / \mathrm{ft}}{16,500 \mathrm{psi}}=0.8 \mathrm{in}^{2} / \mathrm{ft}$ required
From Table 4, use 0.111 thickness
4. Buckling
(See page 14 for key to terms)
Wall area $\mathrm{A}=1.556 \mathrm{in}^{2} / \mathrm{ft}$ to be checked for possible buckling.

If allowable buckling stress, $\mathrm{f}_{\mathrm{cr}} / \mathrm{SF}<\mathrm{f}_{\mathrm{a}}$
then area must be rechecked using $\mathrm{f}_{\mathrm{cr}} / \mathrm{SF}$ in lieu of $\mathrm{f}_{\mathrm{a}}$.
$\mathrm{FS}=2.0$
If $s<\frac{r}{k} \sqrt{\frac{24 E_{m}}{f_{u}}}$ then $f_{c r}=f_{u}-\frac{f_{u}{ }^{2}}{48 E_{m}}(\mathrm{ks} / \mathrm{r})^{2}$

$$
\text { If } s>\frac{r}{k} \sqrt{\frac{24 E_{m}}{f_{u}}} \text { then } f_{c r}=\frac{12 E_{m}}{(k s / r)^{2}}
$$

In this example span is greater than $\frac{r}{k} \sqrt{\frac{24 E_{m}}{f_{u}}}$
Therefore $f_{c r}=\frac{12 \times 29 \times 10^{6}}{(.22 \times 264 / .682)^{2}}$
$f_{c r}=47,986$
$f_{c r}>f a 47,986>16,500$
therefore, $0.111^{\prime \prime}$ is OK.
5. Seam Strength (SS):

Required SS $=$ Ts (SF)
SS $=13,200 \times 3.0$
$S S=39,600$ required
actual seam strength
from Table $2=43,000 \mathrm{lbs} / \mathrm{ft}$
therefore $0.111^{\prime \prime}$ is OK
6. Handling and Installation Strength
(Flexibility factor, FF):
$F F=s^{2} / E_{m} \times I$ for round pipe 0.02 .
Therefore, I must equal $120.17 \times 10^{-3} \mathrm{in} .^{4} / \mathrm{in}$.
Where: s = Span in inches $\mathrm{E}_{\mathrm{m}} \quad=$ Modulus of elasticity
I $=$ Moment of inertia
Refer to Table 4 for I values
Therefore, use $0.218^{\prime \prime}$
Based upon this AASHTO Section 12 check, this
$22^{\prime}$ (264") diameter structure could be built using $0.218^{\prime \prime}$ thickness ( 5 gage) MULTI-PLATE ${ }^{\circledR}$ and exceed all safety factors.

## Example 2

Given: MULTI-PLATE ${ }^{\oplus}$ PIPE ARCH $20^{\prime}-5^{\prime \prime} \times 13^{\prime}-0^{\prime \prime}$
Corner radius 31"
Height of cover $=6^{\prime}$
Live Load $=\mathrm{H} 20$
Weight of soil $=120 \mathrm{pcf}$
By following the steps described in example \#1, the minimum gage would be $0.111^{\prime \prime}$ (12 gage)

For pipe-arches, flexibility factor must be less than 0.03
Actual Flexibility Factor $=0.034>0.03$ maximum
Therefore, next heavier gage of $0.140^{\prime \prime}$ (10 gage) must be used.

## Example 3

Given: MULTI-PLATE ${ }^{\circledR}$ Arch $23^{\prime}$ span $\times 11^{\prime} 6^{\prime \prime}$ rise Height of cover H = 19' Live load LL $=\mathrm{H} 20$ Weight of soil $\mathrm{W}=120 \mathrm{lb} / \mathrm{ft}^{3}$

By following the steps in examples 1 and 2, this structure can be built using 8 gage ( $0.170^{\prime \prime}$ )

Note: Design of Aluminum Structural Plate incorporating reinforcing ribs requires using combined properties of the ribs and corrugated shell. In addition, a plastic moment capacity check should be performed. Contech has supplied design height-ofcover tables that provide the optimum rib and shell thickness combination.

## SUPER-SPAN"' and SUPER-PLATE ${ }^{\circledR}$ Design

Design of SUPER-SPAN and SUPER-PLATE (Long Span) structures follow AASHTO Section 12.7.

SUPER-SPAN and SUPER-PLATE feature relatively large radius or flatter curvature in the top or sides (larger than standard structural plate designs). These shapes include:


The primary differences in long span design procedures and standard plate structures design procedures are:

- Design checks for buckling and flexibility are not applied because of special features not found in other Structural Plate structures and also because of the use of high quality backfill and shape monitoring during backfill.
- Special features such as longitudinal thrust beams are incorporated to assist in the ability of the structure to transfer load to the surrounding soil envelope. Thrust beams also work to isolate the top arc, diminishing the need for a buckling analysis.

- Gage of the top plates and minimum cover are determined by the top radius (see Table 8)
- Maximum central angle of top is 80 degrees
- Ratio of top radius to side radius is equal to or greater than 2.0 and less than or equal to 4.4 .


SUPER-SPAN
structure near
Hamilton, Ohio

The designer should consult with Contech Engineered Solutions LLC regarding these special features. Dimensions for longitudinal thrust beams are also available as are recommendations on the suitability of a particular backfill type.

Gage or thickness for SUPER-SPAN is a function of the structure's top radius and the live and dead loads. Table 8 shown provides the recommended gages for SUPER-SPAN. The designer should also note that Contech Engineered Solutions provides a "shape control monitor" as a condition of the sale of a SUPER-SPAN or SUPER-PLATE. The shape control monitor will be on-site during the entire backfilling process to ensure proper finished structure shape.

Aluminum SUPER-PLATE long spans are available in most of the same sizes and shapes as steel long spans.

Further information is available in the SUPER-SPAN and SUPER-PLATE section of this catalogue and technical guidelines contained in this brochure.

## TABLE 8.

MINIMUM THICKNESS - MINIMUM COVER TABLE, FT. H 20 LIVE LOAD

| Wall Thickness, Inches |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Top Radius <br> $\mathbf{R}_{\mathbf{T}}$ Ft. | $\mathbf{0 . 1 1 1 ^ { \prime \prime }}$ | $\mathbf{0 . 1 4 0 ^ { \prime \prime }}$ | $\mathbf{0 . 1 7 0 \prime \prime}$ <br> or $\mathbf{0 . 1 8 8 \prime \prime}^{\prime \prime}$ | $\mathbf{0 . 2 1 8 ^ { \prime \prime }}$ | $\mathbf{0 . 2 4 9 \prime \prime}$ | $\mathbf{0 . 2 8 0 \prime \prime}$ |
| $15^{\prime}$ | $2.5^{\prime}$ | $2 . .^{\prime} 5$ | $2.5^{\prime}$ | $2.0^{\prime}$ | $2.0^{\prime}$ | $2.0^{\prime}$ |
| $15^{\prime}-17^{\prime}$ |  | $3.0^{\prime}$ | $3.0^{\prime}$ | $2.5^{\prime}$ | $2.0^{\prime}$ | $2.0^{\prime}$ |
| $17^{\prime}-20^{\prime}$ |  |  | $3.0^{\prime}$ | $2.5^{\prime}$ | $2.5^{\prime}$ | $2.5^{\prime}$ |
| $20^{\prime}-23^{\prime}$ |  |  |  | $3.0^{\prime}$ | $3.0^{\prime}$ | $3.0^{\prime}$ |
| $23^{\prime}-25^{\prime}$ |  |  |  |  | $4.0^{\prime}$ | $4.0^{\prime}$ |

Contact a Contech representative for Pear and Pear-Arch shapes.

## Aluminum Box Culvert Design



The structural design of Aluminum Box Culvert does not follow the aforementioned processes. Due to the shape of the box culvert, the "ring compression" method used to quantify design pressures does not apply. The relatively flat radius crowns are subject to large moment forces. Therefore, a separate method is used to ensure that the Aluminum Box Culvert can support both the earth loads and the live loads applied to these structures under relatively shallow fills. Primarily, the design procedure quantifies the capacity of the corrugated aluminum shell and reinforcing ribs to resist bending moments.


Due to the indeterminate nature of the structural elements, finite element analysis was developed to evaluate the plastic moment capacity of the structure. The design requirements for Aluminum Box Culverts are contained in the AASHTO Highway Bridge Design Manual Section 12.8.

Contech Engineered Solutions has also generated height of cover tables that meet the requirements of AASHTO for both HS-20 and HS-25 live loads that supply the plate gages and reinforcing ribs necessary for a given height of cover. These tabled values are contained in the Aluminum Box Culvert section of this manual.

## Minimum Cover Over Plate Structures

Establishing minimum cover over plate structure is one of the most important factors in ensuring the successful installation of soil-corrugated metal interaction structures. Cover over the structure plays an important part in distributing the load that reaches the structure. Without minimum cover, loads applied by vehicles can result in unacceptable structure deformation.

Contech Engineered Solutions publishes suggested minimum cover heights as part of height of cover tables contained in each following section. Minimum cover heights have been established based primarily upon extensive experience. When HS-20 or 25 highway type loads are expected, minimum cover height over steel or aluminum structural plate (excluding SUPER-SPAN or Box Culvert structures) amounts to one eighth of the span or diameter of the structure with a minimum of $12^{\prime \prime}$ in all cases. E-80 railroad loadings require a minimum cover of about one sixth of the diameter or span. In some cases, a concrete load-relieving slab may be used when minimum cover is not achievable.

Being a more rigid structure, minimum cover over Aluminum Box Culverts is often much lower than those for standard plate structures. In all cases, the minimum cover over these structures is 1.4 feet given the proper reinforcing rib and plate gage combinations shown in the height of cover tables for Aluminum Box Culverts.

Minimum cover over SUPER-SPAN structures is dependent upon the top radius of the structure. Minimum cover may be determined from Table 8 on the previous page.
Minimum cover is measured from the top of the structure to the bottom of a flexible pavement and to the top of a rigid pavement. Particular attention should be given to the height of cover near roadway shoulders as they slope away from the road crown. Minimum cover heights must be maintained throughout the life of the structure. Gravel (unpaved) roads can be mistakenly graded below the minimum cover height resulting in unacceptable loading conditions. It is recommended that unpaved roads incorporate at least $6^{\prime \prime}$ more than the minimum allowable cover depth to allow for rutting.
It should be understood that often the greatest live load applied to the structure may be the load applied by construction equipment. The following information supplies guidance for necessary minimum cover. Other off-highway live loads such as mine haul trucks should be evaluated carefully. Contech can assist the designer with establishing minimum cover for this type of loading condition.

## BridgeCor ${ }^{\circledR}$ Design

The design procedure for BridgeCor is outlined in AASHTO LRFD Section 12.8.9 - Deep Corrugated Structural Plate Structures. These structures are designed as long-span culverts but must also meet provisions for flexure and general buckling. BridgeCor structures can be made in multiple shapes and sizes to meet site specific project requirements.

These shapes include:


Structures designed under this specification shall be analyzed by accepted finite element analysis. This analysis must consider the strength and stiffness properties of the structural plate and the soil. To properly analyze these properties using finite element analysis it is important to have a geotechnical report for each specific project. This information will allow the designer to optimize both the gage of the steel and the limits of the structural backfill adjacent to the BridgeCor structure.

This design procedure is more comprehensive than a typical ring compression design for MULTI-PLATE structures. Therefore, it will require additional time to properly evaluate a BridgeCor solution for any application. Proper planning is critical to a successful project.

## BridgeCor Monitoring

Due to the potential large sizes of BridgeCor structures and the information outlined in AASHTO Specification Section 26 - Metal Culverts, it is a requirement to monitor the shape of the structure during the backfill process. Depending on the size and complexity of a structure, guidelines have been established to determine what level of monitoring will be required on all projects. There are four levels of monitoring outlined for BridgeCor. These levels range from a preconstruction conference with a contractor to a full monitoring program similar to the process outlined for a SUPER SPAN structure. See your local Contech representative for additional information.


BridgeCor box culvert in Puerto Rico

## Guidelines

## General Guidelines for Minimum Cover Required for Heavy Off-Road Construction Equipment

For temporary construction vehicle loads, an extra amount of compacted cover may be required over the top of the pipe. The height of cover must meet the minimum requirements shown. The use of heavy construction equipment necessitates greater protection for the pipe than finished grade cover minimums for normal highway traffic.


Minimum Cover May Vary, Depending On Local Conditions. The Contractor Must Provide The Additional Cover Required To Avoid Damage To The Structure. Minimum Cover Is Measured From The Top Of The Structure To The Top Of The Maintained Construction Roadway Surface.

| TABLE 9. HEAVY WHEEL LOAD (STEEL) <br> MIN. COVER FOR OFF HIGHWAY VEHICLES UP TO 450T GVW |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DIAMETER | WALL THICKNESS, IN INCHES |  |  |  |  |  |  |
| (OR SPAN) IN FEET | $\begin{gathered} 0.111 " \\ \text { (12GA.) } \end{gathered}$ | $\begin{gathered} 0.140 " \\ (10 \mathrm{GA} .) \end{gathered}$ | $\begin{aligned} & 0.170 " \\ & \text { (8 GA.) } \end{aligned}$ | $\begin{aligned} & \hline 0.188^{\prime \prime} \\ & (7 \mathrm{GA} .) \end{aligned}$ | $\begin{aligned} & 0.218 " \\ & \text { (5 GA.) } \end{aligned}$ | $\begin{aligned} & 0.249 " \\ & \text { (3 GA.) } \end{aligned}$ | $\begin{aligned} & 0.280^{"} \\ & \text { (1 GA.) } \end{aligned}$ |
| 5' TO 10' | 2.51 | 2.51 | 2.5 | 2.51 | 2.51 | 2.51 | 2.5 |
| 11' TO 12' | $3.0{ }^{\prime}$ | $3.0{ }^{\prime}$ | $3.0{ }^{\prime}$ | $3.0{ }^{\prime}$ | $3.0{ }^{\prime}$ | $3.0{ }^{\prime}$ | $3.0{ }^{\prime}$ |
| 13' TO 14' | $3.5{ }^{\prime}$ | 3.5 | 3.5 | 3.5 | 3.5 | $3.5{ }^{\prime}$ | 3.5 |
| 15' TO 16' | $4.0{ }^{\prime}$ | $4.0{ }^{\prime}$ | $4.0{ }^{\prime}$ | $4.0{ }^{\prime}$ | $4.0{ }^{\prime}$ | $4.0{ }^{\prime}$ | $4.0{ }^{\prime}$ |
| 17' TO 18' | - | $4.5{ }^{\prime}$ | 4.51 | $4.5{ }^{\prime}$ | 4.51 | $4.5{ }^{\prime}$ | 4.51 |
| 19' TO 20' | - | - | 5.0' | 5.0' | 5.0' | 5.0' | 5.0' |

## Notes:

1. Follow AASHTO or NCSPA Guidelines for spans greater than $20^{\prime}$
2. Backfill shall be excellent quality material compacted to $90 \%$ proctor AASHTO T-99

3 . Add $2^{\prime}$ for rutting in un-maintained areas

| TABLE 10. HEAVY WHEEL LOAD (ALUMINUM) MIN. COVER FOR OFF HIGHWAY VEHICLES UP TO 175T GVW |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DIAMETER | WALL THICKNESS, IN INCHES |  |  |  |  |  |
| (OR SPAN) <br> IN FEET | 0.125" | 0.150" | 0.175" | 0.200" | 0.225" | 0.250" |
| 5' T0 9' | $3.0{ }^{\prime}$ | $3.0{ }^{\prime}$ | 2.5 | 2.5 | 2.5 | 2.5 |
| 10' TO 12' | -- | $4.0{ }^{\prime}$ | $4.0{ }^{\prime}$ | $4.0{ }^{\prime}$ | 3.5 | $3.0{ }^{\prime}$ |
| 13' TO 15' | -- | $5.0{ }^{\prime}$ | 4.51 | $4.5{ }^{\prime}$ | $4.0{ }^{\prime}$ | $4.0{ }^{\prime}$ |
| 16' TO 18' | -- | 5.0' | $5.5{ }^{\prime}$ | $5.0{ }^{\prime}$ | $5.0{ }^{\prime}$ | 4.51 |
| 19' TO 20' | -- | 6.0' | 6.5 | $6.0{ }^{\prime}$ | 5.51 | 5.51 |
| 19' TO 20' | - | - | $5.0{ }^{\prime}$ | $5.0{ }^{\prime}$ | 5.0' | 5.0' |

Notes:

1. Backfill shall be of excellent quality material compacted to $90 \%$ proctor AASHTO T-99
2. Add 2' for rutting in un-maintained areas
3. The use of crown ribs may enable crossing of construction equipment with less cover than indicated in the table above or permit the crossing of equipment greater than 175 tons GVW.
4. The use of crown ribs may accommodate spans greater than $20^{\prime}$. contact Contech for more information related to specific applications.


For minimum cover requirements for construction loads on structures with spans greater than 20' $\mathbf{0}^{\prime \prime}$, contact your local Contech representative.
Grade Separation Structure

## Structure End Treatments

Once the designer has selected a structure and has determined the structural requirements, attention should be turned to protecting the ends of the structure. Hydraulic efficiency, protection of the structure backfill, and structure alignment may dictate the usage of modified structure ends (bevels and skews), headwalls, or cut-off walls. The range of possible end treatments include but are not limited to:

## Square ended



## Beveled

(structure cut at an angle relative to horizontal plane)


## Step-beveled end



Elevation View

## Skewed

(structure cut at an angle relative to vertical plane)


Beveled and skewed


Skewed with concrete headwall


Ellipse End View

## Beveled with concrete slope collar



## Any of the above with concrete or sheet pile toe wall



Square ended structures are generally the most cost effective end treatment option. The square end should, at a minimum, project from sloping side fill enough to allow the invert to meet the toe of the slope. All structures can be supplied with square ends. Larger structures may need a headwall to prevent inlet flotation.

Beveled ends are often desirable because they can be supplied to match the side slope of an embankment. Beveled ends also provide for better hydraulic entrance efficiency when compared to square-ended structures. Whenever structures with full inverts and/or beveled ends are used, the designer should always consider a concrete toe wall to anchor the leading edge of the invert, thus precluding the possibility of hydraulic uplift forces lifting the invert of the structure.

Beveled ends on larger structures must be supported. A beveled section is comprised of incomplete rings of plates acting as retaining walls. Because of this, bevels should be limited to 1.5:1-2:1 angles. Flatter bevels may be considered but a rigid reinforced concrete slope collar may be necessary to stabilize the beveled end of the structure. Fully beveled ends are not recommended for pipe-arch and underpass shapes. Step bevels provide for better structural soundness.

Step-beveled ends minimize the number of cut or incomplete plate rings while still providing a sloped end. This also provides a stiffer leading edge at the invert. For this reason, step-beveled ends are desirable over fully beveled ends.

Recommended step-bevel dimensions are:

## - Round

Top step $=0.25 \times$ diameter
Bottom step $=0.25 \times$ diameter

## - Pipe-Arch and Underpass

Top and bottom steps match top and bottom longitudinal seam of plates (see sketch). Consult your Contech representative for exact dimensions and plate layout.

## - Horizontal Ellipses

Same as pipe-arch and underpass.

## - Arches

A single top step and a small (usually $6^{\prime \prime}$ high) bottom step are recommended for arch structures. The top step should be $0.25 \times$ rise.

Skewed Ends allow the designer to match the skew of the structure to the roadway. As with beveled ends, skewed ends are less stable because of incomplete plate rings. Soil loads at the structure end can act upon the extended end of the skew and cause deflection of the plates. Skew angles without a concrete headwall should be a maximum of 15 degrees.

The designer may use a reinforced concrete headwall or slope collar to support the skewed end. More commonly, the structure end will be skewed in combination with a beveled end (skewed to the roadway and beveled to match the side slope.) In this case, the same rules apply to maximum bevel angle and skew angle without a reinforced concrete structure surrounding the skewed and beveled end.

The designer must always consider "warping" the side slope fill to balance soil loads on each side of the structure (see drawing number 1008534B on page 28).


Figure 3. Suggested limits for skews to embankments unless the embankment is warped for support or full head walls are provided.

## Cast-in-place (C.I.P.) concrete headwalls are

 recommended whenever the designer requires improved hydraulic efficiency, the structure is skewed more than 15 degrees to the roadway or when the designer expects sustained high level flows that can cause scour and erosion at the entrance or exit ends of the structure. By erecting a rigid concrete headwall structure, the skew angle may go beyond 15 degrees.C.I.P. concrete headwalls are secured to the plate structure by the use of anchor bolts placed circumferentially at the end of the structure. Anchor bolts may either be straight $3 / 4$ " diameter or "hook" bolts. The spacing circumferentially and the choice of bolt type is a function of headwall design which is outside the scope of this document. Typical headwall details are shown on the next few pages. CAD details are available on request from a Contech representative.
C.I.P. Concrete slope collars placed around a beveled end structure guard against deflection of end plates, control erosion and backfill loss, and provide an aesthetic end treatment. They are anchored to the structure by the use of anchor bolts as with concrete headwalls.
C.I.P. Concrete Cut-off or Toe-walls should be considered on almost every hydraulic structure with an invert.
Undercutting on the inlet end can lead to loss of backfill, piping of water around the exterior of the structure, and undesirable uplift forces that can damage the structure. The structure should be well anchored to the wall with anchor bolts. Interlocking sheet piling may be driven below the wall to minimize the use of the concrete. Slope protection is also advised to preclude water entering the structure backfill.

Modular Block Headwalls can be utilized to provide an aesthetically pleasing headwall. If the structure is expected to be subjected to hydraulic forces, special consideration must be given to the possible loss of backfill through the block wall face and at the junction of the blocks with the structure. Geotextile fabrics placed in critical areas can minimize the loss of fill. The designer should also consider other factors such as but not limited to:

- Scouring forces acting on the footing of the wall.
- Rapid draw-down forces that can occur if the backfill becomes saturated.
- Settlement of the structure relative to the wall. Settlement joints may be necessary.

Contact your Contech representative for more details on modular block headwalls design.

## BridgeCor, SUPER-SPAN and SUPER-PLATE End Treatment

Any of the presented headwall options can be used with these structures.

## Aluminum Box Culvert End Treatment

Aluminum Box Culverts can be supplied with a pre-designed corrugated aluminum headwall and wingwall system. These headwalls are only provided on square ended (non-skew cut) structures. See the Aluminum Box Culvert section starting on page 64 for details.
Beveled ends are not allowed on Aluminum Box Culverts.
Skewed ends are allowed only with a concrete headwall.
C.I.P. concrete headwalls may be used and are required if the structure is to be skew cut. The structure may be anchored to the C.I.P. headwall in the same fashion as with steel structures discussed earlier. C.I.P. headwall standard designs are available from your Contech representative.

As with all corrugated metal structures with full inverts, a cut-off wall is a necessity on hydraulic structures. Aluminum Box Culverts with full inverts are provided with a bolt-on $26^{\prime \prime}$ deep toe wall plate. The designer should determine the depth to which the toe-wall should extend.

Contech Engineered Solutions advises the designer to take all necessary precautions to protect the ends of corrugated metal hydraulic structures. Damage to the structure ends may result in inlet blockage. The designer is also advised that whenever heavy debris flow is expected, the use of a large single span structure is recommended over smaller, multiple structures.
As with all contents of this manual, Contech Engineered Solutions cannot foresee all possible situations or events relating to the end treatment of structures. Therefore, this manual cannot be expected to serve as the sole reference on the subject and the designer should consult documents such as those published by FHWA or a local Department of Transportation for more complete information.

Appropriate end treatment design is beyond the scope of this catalog. Additional information can be obtained from the local D.O.T. guidelines, the FHWA Circular Memo, "Plans for Culvert Inlet and Outlet Structures", Sheets G-39-66 to G-42-66, 1996, and chapters within the AISI Handbook of Steel Drainage \& Highway Construction Products.



Typical End Treatments

Cut Off Wall \& Beveled End Treatments

# C 企NTECH <br> ENGINEERED SOLUTIONS 

(C) COPYRIGHT
CORRUGATED METAL PIPE STRUCTURES SKEWED TO FILL SLOPE

| DRAWN BY: J.C.S. | REV. BY: $\quad$ N/A | SCALE: | N/A |  |
| :--- | ---: | :--- | ---: | :--- |
| DATE: | $6-14-91$ | DATE: | $11-5-91$ | 1008534 B |

## Material, Design \& Installation Specifications

Following is an outline of applicable AASHTO and ASTM specifications. Additional specifications are available from the American Railroad Engineers and Maintenance of Way Association (AREMA), Manual for Railway Engineering for railroad projects

| Description | AASHTO | ASTM |
| :---: | :---: | :---: |
| Steel MULTI-PLATE |  |  |
| Material | M-167 | A-761 |
| Installation | Refer to AASHTO Standard Specifications for Highway Bridges (Sec. 26) | A-807 |
| Design | Refer to AASHTO Standard Specifications for Highway Bridges (Sec. 12) | A-796 |
| Aluminum Structural Plate |  |  |
| Material | M-219 | B-746 |
| Installation | M-219 - Refer to AASHTO Standard Specifications for Highway Bridges (Sec. 26.5) | B-789 |
| Design | Refer to AASHTO Standard Specifications for Highway Bridges (Sec. 12.6) | B-790 |
| Aluminum Box Culverts |  |  |
| Material | M-219 | B-864 |
| Installation | Refer to AASHTO Standard Specifications for Highway Bridges (Sec. 12.8) | N/A |
| Design | Refer to AASHTO Standard Specifications for Highway Bridges (Sec. 12.8) | N/A |
| SUPER-SPAN \& SUPER-PLATE |  |  |
| Material | M-167 (steel) and M-219 (Aluminum) | A-761 |
| Installation | Refer to AASHTO Standard Specifications for Highway Bridges (Sec. 12 and Sec. 26) | A-761 |
| Design | Refer to AASHTO Standard Specifications for Highway Bridges (Sec. 12.7) | N/A |
| BridgeCor |  |  |
| Material | M-167 | A-761 |
| Installation | Refer to AASHTO Standard Specifications for Highway Bridges (Sec. 26) | N/A |
| Design | Refer to AASHTO Standard Specifications for Highway Bridges (Sec. 12.8.9) | N/A |

Excerpts of these specifications are available from Contech Engineered Solutions LLC.


SUPER-SPAN grade separation structure with Bin-Wall end treatment

## MULTI-PLATE ${ }^{\circledR}$

## Made to perform, built to last.

Contech MULTI-PLATE structures provide designers of stormwater management systems underpasses and bridges with a versatile method of construction and a long history of strength, durability, and economy. A variety of shapes and sizes ensures that MULTI-PLATE structures fit most applications. Ease of design, construction, and proven reliability make them the frequent choice of experienced engineers.
MULTI-PLATE structures are made from sturdy, heavy gage, corrugated steel plates that are pre-formed to various shapes and sizes, then galvanized for long-term protection and performance. The plates are delivered to the job site and bolted together to form a MULTI-PLATE structure optimally suited for the project.

MULTI-PLATE is available in full round, arch, pipe-arch, horizontal and vertical ellipse, underpass, box culvert, and long-span shapes-all in a wide range of sizes. Since 1931, MULTI-PLATE has been proven to offer:

## Superior durability

MULTI-PLATE's heavy gage steel uses an industry standard 3 oz . per square foot galvanized coating capable of providing a service life of 75 years or longer. More information is covered on page 7 .
When selecting the proper material for an application, designers need to evaluate the soil side of the structure along with the corrosive and abrasive action due to the flow at the invert of the structure. The use of structural plate gives designers more structure shape options to help minimize the impact of abrasion on the invert of the structure.

## High load-carrying capacity

As a steel-soil interaction system, MULTI-PLATE is designed to carry high combined live and dead loads. High traffic loads and deep cover applications are a MULTI-PLATE specialty.

## Easier, faster installation

Prefabricated plates are assembled in the field, translating into finished construction in days instead of weeks as with most concrete structures.

## Versatility

MULTI-PLATE structures remove all of the shape, size and installation restrictions of precast or cast-in-place concrete.

Round

Vertical Ellipse



Pipe-Arch


Horizontal Ellipse


Single Radius

Arch



For square end structures on which headwalls are to be built, design should allow for a 2 " lip at each end.

TABLE 11. DETAILS OF UNCURVED MULTI-PLATE ${ }^{\oplus}$ SECTIONS


## Standard 6" x 2" Corrugation

| TABLE 12. APPROXIMATE WEIGHT OF MULTI-PLATE SECTIONS |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Pi | Net Length (Feet) | Galvanized, in Pounds, without Bolts ${ }^{(1)(2)}$ |  |  |  |  |  |  |  |  |
|  |  | Specified Thickness, Inches ${ }^{(3)}$ |  |  |  |  |  |  |  |  |
|  |  | $\begin{gathered} 0.111 \\ \text { (12Ga.) } \\ \hline \end{gathered}$ | $\begin{gathered} 0.140 \\ (10 \text { Ga.) } \end{gathered}$ | $\begin{gathered} 0.170 \\ (8 \mathrm{Ga} .) \end{gathered}$ | $\begin{gathered} 0.188 \\ (7 \mathrm{Ga} .) \end{gathered}$ | $\begin{gathered} 0.218 \\ (5 \mathrm{Ga} .) \end{gathered}$ | $\begin{gathered} 0.249 \\ (3 \mathrm{Ga} .) \end{gathered}$ | $\begin{gathered} 0.280 \\ (1 \text { Ga. }) \end{gathered}$ | $\begin{gathered} 0.318 \\ (5 / 16 \mathrm{In} .) \end{gathered}$ | $\begin{gathered} 0.375 \\ (3 / 8 \mathrm{In} .) \end{gathered}$ |
| 9 | 10 | 161 | 205 | 250 | 272 | 316 | 361 | 405 | 460 | 545 |
| 9 | 12 | 193 | 246 | 299 | 325 | 379 | 432 | 485 | 551 | 653 |
| 15 | 10 | 253 | 323 | 393 | 428 | 498 | 568 | 638 | 725 | 859 |
| 15 | 12 | 303 | 386 | 470 | 511 | 595 | 678 | 762 | 865 | 1026 |
| 18 | 10 | 299 | 382 | 465 | 506 | 589 | 671 | 754 | 856 | 1015 |
| 18 | 12 | 357 | 456 | 555 | 604 | 703 | 801 | 900 | 1022 | 1212 |
| 21 | 10 | 345 | 441 | 536 | 583 | 679 | 774 | 869 | 987 | 1170 |
| 21 | 12 | 412 | 526 | 640 | 697 | 810 | 924 | 1038 | 1179 | 1398 |
| 24 | 10 | 396 | 504 | 613 | 667 | 775 | 886 | 995 | 1130 | 1340 |
| 24 | 12 | 473 | 603 | 732 | 797 | 927 | 1060 | 1190 | 1351 | 1602 |

${ }^{(1)}$ Weights are based on a zinc coating of $3 \mathrm{Oz} . /$ sq. ft. of double exposed surface.
${ }^{(2)}$ All weights are subject to manufacturing tolerances.
${ }^{(3)}$ Specified thickness is a nominal galvanized thickness. Reference AASHTO M 167.


Unbalanced Channel for MULTI-PLATE ${ }^{\circledR}$ Arch

TABLE 13. NORMAL BOLT USAGE

| Plate Gages | Bolt Lengths |
| :---: | :---: |
| 12,10 and 8 | $114^{\prime \prime}$ and $1 \frac{1}{2 \prime \prime}$ |
| 7 and 5 | $11 / 2^{\prime \prime}$ and $13 / 4^{\prime \prime}$ |
| 3 and 1 | $11 / 2^{\prime \prime}$ and $2^{\prime \prime}$ |
| $5 / 16$ and $3 / 8^{*}$ | $2^{\prime \prime}$ and $21 / 2^{\prime \prime}$ |

* These are 7/8" diameter bolts.

Note: The longer bolts are used in 3 plate lap seams.

| TABLE 14. PHYSICAL PROPERTIES OF MULTI-PLATE ${ }^{\circledR}$ |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Gage | Specified Thickness, Inches | Uncoated <br> Thickness <br> $T$ (Inches) | Moment of Inertia I (In. ${ }^{\mathbf{4} / \mathbf{I n} \text {.) }}$ | Section Modulus S (In. $\left.{ }^{3} / \mathbf{I n}.\right)$ | Radius of Gyration r (Inches) | Area of Section (In. ${ }^{2} /$ Ft.) |
| 12 | 0.111 | 0.1046 | 0.0604 | 0.0574 | 0.682 | 1.556 |
| 10 | 0.140 | 0.1345 | 0.0782 | 0.0733 | 0.684 | 2.003 |
| 8 | 0.170 | 0.1644 | 0.0962 | 0.0888 | 0.686 | 2.449 |
| 7 | 0.188 | 0.1838 | 0.108 | 0.0989 | 0.688 | 2.739 |
| 5 | 0.218 | 0.2145 | 0.1269 | 0.1147 | 0.690 | 3.199 |
| 3 | 0.249 | 0.2451 | 0.1462 | 0.1302 | 0.692 | 3.658 |
| 1 | 0.280 | 0.2758 | 0.1658 | 0.1458 | 0.695 | 4.119 |
| 5/16 | 0.318 | 0.3125 | 0.190 | 0.164 | 0.698 | 4.671 |
| 3/8 | 0.380 | 0.375 | 0.232 | 0.195 | 0.704 | 5.613 |

TABLE 15. MULTI-PLATE ROUND PIPE

| Pipe Diameter |  | End Area, <br> Sq. Ft. | Pipe Diameter |  | End Area, <br> Sq. Ft. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| (Feet) | (Inches) |  | (Feet) | (Inches) |  |
| 5.0 | 60 | 19.1 | 16.0 | 192 | 204.4 |
| 5.5 | 66 | 23.2 | 16.5 | 198 | 217.5 |
| 6.0 | 72 | 27.8 | 17.0 | 204 | 231.0 |
| 6.5 | 78 | 32.7 | 17.5 | 210 | 244.9 |
| 7.0 | 84 | 38.1 | 18.0 | 216 | 259.2 |
| 7.5 | 90 | 43.9 | 18.5 | 222 | 274.0 |
| 8.0 | 96 | 50.0 | 19.0 | 228 | 289.1 |
| 8.5 | 102 | 56.6 | 19.5 | 234 | 304.7 |
| 9.0 | 108 | 63.6 | 20.0 | 240 | 320.6 |
| 9.5 | 114 | 71.0 | 20.5 | 246 | 337.0 |
| 10.0 | 120 | 78.8 | 21.0 | 252 | 353.8 |
| 10.5 | 126 | 87.1 | 21.5 | 258 | 371.0 |
| 11.0 | 132 | 95.7 | 22.0 | 264 | 388.6 |
| 11.5 | 138 | 104.7 | 22.5 | 270 | 406.6 |
| 12.0 | 144 | 114.2 | 23.0 | 276 | 425.0 |
| 12.5 | 150 | 124.0 | 23.5 | 282 | 443.8 |
| 13.0 | 156 | 134.3 | 24.0 | 288 | 463.0 |
| 13.5 | 162 | 144.9 | 24.5 | 294 | 482.6 |
| 14.0 | 168 | 156.0 | 25.0 | 300 | 502.7 |
| 14.5 | 174 | 1467.5 | 25.5 | 306 | 523.1 |
| 15.0 | 180 | 179.4 | 26.0 | 312 | 543.9 |
| 15.5 | 186 | 191.7 |  |  |  |



Figure 4. Round and 5\% Vertical Ellipse Pipe

| TABLE 16. PLATE ARRANGEMENT AND APPROXIMATE WEIGHT PER FOOT FOR MULTI-PLATE ROUND PIPE |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Pipe Diameter (inches) | Number of Plates Per Ring 12 through 1 Gage |  |  |  |  | Specified Thickness, Inches |  |  |  |  |  |  |  |  |
|  | Pi |  |  |  | Total Plates | 0.111 | 0.140 | 0.170 | 0.188 | 0.218 | 0.249 | 0.280 | with 7/8" <br> fasteners |  |
|  | 15 | 18 | 21 | 24 |  | 12 (Ga.) | (10 Ga.) | (8 Ga.) | (7 Ga.) | (5 Ga.) | (3 Ga.) | (1 Ga.) | 5/16 | 3/8 |
| 60 | 4 |  |  |  | 4 | 105 | 132 | 160 | 178 | 205 | 233 | 260 | 320 | 373 |
| 66 | 2 | 2 |  |  | 4 | 116 | 145 | 176 | 195 | 226 | 256 | 286 | 346 | 405 |
| 72 |  | 4 |  |  | 4 | 126 | 158 | 192 | 213 | 246 | 279 | 312 | 372 | 436 |
| 78 |  | 2 | 2 |  | 4 | 137 | 172 | 207 | 231 | 267 | 303 | 339 | 399 | 467 |
| 84 |  |  | 4 |  | 4 | 147 | 185 | 223 | 249 | 287 | 326 | 365 | 426 | 499 |
| 90 |  |  | 2 | 2 | 4 | 158 | 198 | 239 | 266 | 308 | 349 | 391 | 479 | 560 |
| 96 |  |  |  | 4 | 4 | 168 | 211 | 255 | 284 | 328 | 372 | 417 | 506 | 591 |
| 102 | 2 | 4 |  |  | 6 | 179 | 224 | 271 | 302 | 349 | 396 | 443 | 532 | 623 |
| 108 |  | 6 |  |  | 6 | 189 | 238 | 287 | 320 | 369 | 419 | 469 | 559 | 654 |
| 114 |  | 4 | 2 |  | 6 | 200 | 251 | 303 | 337 | 390 | 442 | 495 | 585 | 685 |
| 120 |  | 2 | 4 |  | 6 | 210 | 264 | 319 | 355 | 410 | 466 | 521 | 612 | 717 |
| 126 |  |  | 6 |  | 6 | 221 | 277 | 335 | 373 | 431 | 489 | 547 | 638 | 748 |
| 132 |  |  | 4 | 2 | 6 | 231 | 290 | 351 | 391 | 451 | 512 | 573 | 692 | 809 |
| 138 |  |  | 2 | 4 | 6 | 242 | 304 | 367 | 408 | 472 | 535 | 599 | 718 | 841 |
| 144 |  |  |  | 6 | 6 | 252 | 317 | 383 | 426 | 492 | 559 | 625 | 745 | 872 |
| 150 |  | 6 | 2 |  | 8 | 263 | 330 | 399 | 444 | 513 | 582 | 651 | 771 | 903 |
| 156 |  | 4 | 4 |  | 8 | 273 | 343 | 415 | 462 | 534 | 605 | 677 | 798 | 935 |
| 162 |  | 2 | 6 |  | 8 | 284 | 356 | 431 | 480 | 554 | 629 | 703 | 825 | 966 |
| 168 |  |  | 8 |  | 8 | 294 | 370 | 447 | 497 | 575 | 652 | 729 | 851 | 998 |
| 174 |  |  | 6 | 2 | 8 | 305 | 383 | 463 | 515 | 595 | 675 | 755 | 905 | 1,059 |
| 180 |  |  | 4 | 4 | 8 | 315 | 396 | 479 | 533 | 616 | 698 | 781 | 931 | 1,090 |
| 186 |  |  | 2 | 6 | 8 | 326 | 409 | 495 | 551 | 636 | 722 | 807 | 958 | 1,121 |
| 192 |  |  |  | 8 | 8 | 336 | 422 | 511 | 568 | 657 | 745 | 833 | 984 | 1,153 |
| 198 |  | 4 | 6 |  | 10 |  | 436 | 527 | 586 | 677 | 768 | 859 | 1,011 | 1,184 |
| 204 |  | 2 | 8 |  | 10 |  | 449 | 543 | 604 | 698 | 792 | 885 | 1,037 | 1,216 |
| 210 |  |  | 10 |  | 10 |  | 462 | 559 | 622 | 718 | 815 | 911 | 1,064 | 1,247 |
| 216 |  |  | 8 | 2 | 10 |  | 475 | 575 | 639 | 739 | 838 | 937 | 1,117 | 1,308 |
| 222 |  |  | 6 | 4 | 10 |  |  | 591 | 657 | 759 | 861 | 963 | 1,144 | 1,339 |
| 228 |  |  | 4 | 6 | 10 |  |  | 606 | 675 | 780 | 885 | 990 | 1,170 | 1,371 |
| 234 |  |  | 2 | 8 | 10 |  |  | 622 | 693 | 800 | 908 | 1016 | 1,197 | 1,402 |
| 240 |  |  |  | 10 | 10 |  |  | 638 | 710 | 821 | 931 | 1042 | 1,224 | 1,434 |
| 246 |  | 2 | 10 |  | 12 |  |  |  | 728 | 841 | 954 | 1068 | 1,250 | 1,465 |
| 252 |  |  | 12 |  | 12 |  |  |  | 746 | 862 | 978 | 1094 | 1,277 | 1,496 |
| 258 |  |  | 10 | 2 | 12 |  |  |  |  | 882 | 1001 | 1120 | 1,330 | 1,557 |
| 264 |  |  | 8 | 4 | 12 |  |  |  |  | 903 | 1024 | 1146 | 1,357 | 1,589 |
| 270 |  |  | 6 | 6 | 12 |  |  |  |  | 923 | 1048 | 1172 | 1,383 | 1,620 |
| 276 |  |  | 4 | 8 | 12 |  |  |  |  | 944 | 1071 | 1198 | 1,410 | 1,652 |
| 282 |  |  | 2 | 10 | 12 |  |  |  |  |  | 1094 | 1224 | 1,436 | 1,683 |
| 288 |  |  |  | 12 | 12 |  |  |  |  |  | 1117 | 1250 | 1,463 | 1,714 |
| 294 |  |  |  | 14 | 14 |  |  |  |  |  | 1141 | 1276 | 1,490 | 1,746 |
| 300 |  |  | 12 | 2 | 14 |  |  |  |  |  | 1164 | 1302 | 1,543 | 1,807 |
| 306 |  |  | 10 | 4 | 14 |  |  |  |  |  | 1187 | 1328 | 1,569 | 1,838 |
| 312 |  |  | 8 | 6 | 14 |  |  |  |  |  | 1211 | 1354 | 1,596 | 1,870 |

Note:

1. Dimensions are to inside crests of corrugations and are subject to manufacturing tolerances.
2. These plate arrangements will be furnished unless noted otherwise on assembly drawings.
3. Galvanized, with bolts and nuts.
4. Specified thickness is a nominal galvanized thickness.


Aggregate Tunnel

## MULTI-PLATE ${ }^{\circledR}$ Height of Cover Tables

Height-of-Cover Tables 18, 21, 24, 26 and 29 A are presented for the designer's convenience for use in routine applications.
They are based on the design procedures presented herein, using the following values for the soil and steel parameters:
Unit weight of soil - 120 pcf.
Relative density of compacted backfill - minimum 90\% standard per AASHTO T 99
Yield point of steel - 33,000 psi
 AASHTO HEIGHT OF COVER LIMITS H-20, HS-20, H-25, HS-25 LIVE LOADS

Thickness In Inches (Gage)

| (Maximum Cover Height Shown In Feet) |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Span Diameter (Ft.-In.) | Minimum Cover (Inches) | $\begin{gathered} 0.111 \\ \text { (12Ga.) } \end{gathered}$ | $\begin{gathered} 0.140 \\ (10 \text { Ga.) } \end{gathered}$ | $\begin{aligned} & 0.170 \\ & \text { ( } 8 \text { Ga.) } \end{aligned}$ | $\begin{aligned} & 0.188 \\ & \text { (7 Ga.) } \end{aligned}$ | $\begin{gathered} 0.218 \\ (5 \mathrm{Ga} .) \end{gathered}$ | $\begin{aligned} & 0.249 \\ & \text { (3 Ga.) } \end{aligned}$ | $\begin{aligned} & 0.280 \\ & \text { (1 Ga.) } \end{aligned}$ | $\begin{aligned} & 0.318 \\ & (5 / 16) \end{aligned}$ | $\begin{gathered} 0.375 \\ (3 / 8) \end{gathered}$ |
| 5-0 | 12 | 46 | 68 | 90 | 103 | 124 | 146 | 160 | 256 | 308 |
| 5-6 | 12 | 42 | 62 | 81 | 93 | 113 | 133 | 145 | 233 | 280 |
| 6-0 | 12 | 38 | 57 | 75 | 86 | 103 | 122 | 133 | 214 | 257 |
| 6-6 | 12 | 35 | 52 | 69 | 79 | 95 | 112 | 123 | 197 | 237 |
| 7-0 | 12 | 33 | 49 | 64 | 73 | 88 | 104 | 114 | 183 | 220 |
| 7-6 | 12 | 31 | 45 | 60 | 68 | 82 | 97 | 106 | 171 | 205 |
| 8-0 | 12 | 29 | 43 | 56 | 64 | 77 | 91 | 100 | 160 | 192 |
| 8-6 | 18 | 27 | 40 | 52 | 60 | 73 | 86 | 94 | 151 | 181 |
| 9-0 | 18 | 25 | 38 | 50 | 57 | 69 | 81 | 88 | 142 | 171 |
| $9-6$ | 18 | 24 | 36 | 47 | 54 | 65 | 77 | 84 | 135 | 162 |
| 10-0 | 18 | 23 | 34 | 45 | 51 | 62 | 73 | 80 | 128 | 154 |
| 10-6 | 18 | 22 | 32 | 42 | 49 | 59 | 69 | 76 | 122 | 147 |
| 11-0 | 18 | 21 | 31 | 40 | 46 | 56 | 66 | 72 | 116 | 140 |
| 11-6 | 18 | 20 | 29 | 39 | 44 | 54 | 63 | 69 | 111 | 134 |
| 12-0 | 18 | 19 | 28 | 37 | 43 | 51 | 61 | 66 | 107 | 128 |
| 12-6 | 24 | 18 | 27 | 36 | 41 | 49 | 58 | 64 | 102 | 123 |
| 13-0 | 24 | 17 | 26 | 34 | 39 | 47 | 56 | 61 | 98 | 118 |
| 13-6 | 24 | 17 | 25 | 33 | 38 | 46 | 54 | 59 | 95 | 114 |
| 14-0 | 24 | 16 | 24 | 32 | 36 | 44 | 52 | 57 | 91 | 110 |
| 14-6 | 24 | 16 | 23 | 31 | 35 | 42 | 50 | 55 | 88 | 106 |
| 15-0 | 24 | 15 | 22 | 30 | 34 | 41 | 48 | 53 | 85 | 102 |
| 15-6 | 24 | 15 | 22 | 29 | 33 | 40 | 47 | 51 | 82 | 99 |
| 16-0 | 24 |  | 21 | 28 | 32 | 38 | 45 | 50 | 80 | 96 |
| 16-6 | 30 |  | 20 | 27 | 31 | 37 | 44 | 48 | 77 | 93 |
| 17-0 | 30 |  | 20 | 26 | 30 | 36 | 43 | 47 | 75 | 90 |
| 17-6 | 30 |  | 19 | 25 | 29 | 35 | 41 | 45 | 73 | 88 |
| 18-0 | 30 |  |  | 25 | 28 | 34 | 40 | 44 | 71 | 85 |
| 18-6 | 30 |  |  | 24 | 27 | 33 | 39 | 43 | 69 | 83 |
| 19-0 | 30 |  |  | 23 | 27 | 32 | 38 | 42 | 67 | 81 |
| 19-6 | 30 |  |  | 23 | 26 | 31 | 37 | 41 | 65 | 79 |
| 20-0 | 30 |  |  |  | 25 | 31 | 36 | 40 | 64 | 77 |
| 20-6 | 36 |  |  |  | 25 | 30 | 35 | 39 | 62 | 75 |
| 21-0 | 36 |  |  |  |  | 29 | 34 | 38 | 61 | 73 |
| 21-6 | 36 |  |  |  |  | 28 | 34 | 37 | 59 | 71 |
| 22-0 | 36 |  |  |  |  | 28 | 33 | 36 | 58 | 70 |
| 22-6 | 36 |  |  |  |  | 27 | 32 | 35 | 57 | 68 |
| 23-0 | 36 |  |  |  |  |  | 31 | 34 | 55 | 67 |
| 23-6 | 36 |  |  |  |  |  | 30 | 34 | 54 | 65 |
| 24-0 | 36 |  |  |  |  |  |  | 33 | 53 | 64 |
| 24-6 | 42 |  |  |  |  |  |  | 32 | 51 | 62 |
| 25-0 | 42 |  |  |  |  |  |  | 32 | 49 | 60 |
| 25-6 | 42 |  |  |  |  |  |  | 31 | 48 | 58 |
| 26-0 | 42 |  |  |  |  |  |  |  | 46 | 56 |

Notes:

1. Tables based upon AASHTO Sec. 12 Standard Specifications for Highway Bridges.
2. H-20, HS-20, H-25, HS-25 live loads
3. Minimum cover is defined as the vertical distance from the top of the corrugated structure to the bottom of flexible or top of rigid pavement.
34 4. Minimum cover for off highway construction loads must be checked.
4. All covers are calculated using (4) 3/4" A449 bolts/ft. except .318 and .375 which uses ( 8 ) 7/8" A449 bolts/ ft .6 and 8 bolts/ft. are available for structures using $3 / 4^{\prime \prime}$ A449 bolts.

| TABLE 18. PLATE ARRANGEMENT AND APPROXIMATE WEIGHT PER FOOT FOR MULTI-PLATE ${ }^{\oplus}$ VERTICAL ELLIPSE SHAPES |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 5\% Vertical Ellipse ${ }^{(1)}$ |  | Area | Number of Plates Per Ring ${ }^{(2)}$ |  |  |  |  | Approximate Weight Per Foot of Structure, Lbs. ${ }^{(3)}$ |  |  |  |  |  |  |
| Nominal |  |  |  |  |  |  |  | Specified Thickness, Inches ${ }^{(4)}$ |  |  |  |  |  |  |
| Diameter $\mathbf{P i}^{(1)}$ | Horizontal Inches | Vertical Inches |  | Sq. Ft. | 15 Pi | 18 Pi | 21 Pi | 24 Pi | Total <br> Plates | $\begin{gathered} 0.111 \\ (12 \mathrm{Ga} .) \end{gathered}$ | $\begin{gathered} 0.140 \\ )(10 \mathrm{Ga} . \end{gathered}$ | $\begin{gathered} 0.170 \\ \text { (8 Ga.) } \end{gathered}$ | $\begin{gathered} 0.188 \\ (7 \mathrm{Ga} .) \end{gathered}$ | $\begin{gathered} 0.218 \\ \text { (5 Ga.) } \end{gathered}$ | $\begin{gathered} 0.249 \\ (3 \mathrm{Ga} .) \end{gathered}$ | $\begin{gathered} 0.280 \\ (1 \mathrm{Ga} .) \end{gathered}$ |
| 60 | 56 | 62 | 19 | 4 |  |  |  | 4 | 105 | 132 | 160 | 178 | 205 | 233 | 260 |
| 66 | 62 | 68 | 23 | 2 | 2 |  |  | 4 | 116 | 145 | 176 | 195 | 226 | 256 | 286 |
| 72 | 67 | 75 | 28 |  | 4 |  |  | 4 | 126 | 158 | 192 | 213 | 246 | 279 | 312 |
| 78 | 73 | 81 | 32 |  | 2 | 2 |  | 4 | 137 | 172 | 207 | 231 | 267 | 303 | 339 |
| 84 | 79 | 88 | 38 |  |  | 4 |  | 4 | 147 | 185 | 223 | 249 | 287 | 326 | 365 |
| 90 | 85 | 94 | 43 |  |  | 2 | 2 | 4 | 158 | 198 | 239 | 266 | 308 | 349 | 391 |
| 96 | 91 | 101 | 50 |  |  |  | 4 | 4 | 168 | 211 | 255 | 284 | 328 | 372 | 417 |
| 102 | 97 | 107 | 55 | 2 | 4 |  |  | 6 | 179 | 224 | 271 | 302 | 349 | 396 | 443 |
| 108 | 103 | 114 | 62 |  | 6 |  |  | 6 | 189 | 238 | 287 | 320 | 369 | 419 | 469 |
| 114 | 109 | 120 | 70 |  | 4 | 2 |  | 6 | 200 | 251 | 303 | 337 | 390 | 442 | 495 |
| 120 | 115 | 127 | 77 |  | 2 | 4 |  | 6 | 210 | 264 | 319 | 355 | 410 | 466 | 521 |
| 126 | 120 | 133 | 85 |  |  | 6 |  | 6 | 221 | 277 | 335 | 373 | 431 | 489 | 547 |
| 132 | 126 | 139 | 94 |  |  | 4 | 2 | 6 | 231 | 290 | 351 | 391 | 451 | 512 | 573 |
| 138 | 132 | 146 | 102 |  |  | 2 | 4 | 6 | 242 | 304 | 367 | 408 | 472 | 535 | 599 |
| 144 | 138 | 152 | 112 |  |  |  | 6 | 6 | 252 | 317 | 383 | 426 | 492 | 559 | 625 |
| 150 | 142 | 157 | 124 |  | 6 | 2 |  | 8 | 263 | 330 | 399 | 444 | 513 | 582 | 651 |
| 156 | 148 | 164 | 134 |  | 4 | 4 |  | 8 | 273 | 343 | 415 | 462 | 534 | 605 | 677 |
| 162 | 154 | 170 | 144 |  | 2 | 6 |  | 8 | 284 | 356 | 431 | 480 | 554 | 629 | 703 |
| 168 | 159 | 176 | 155 |  |  | 8 |  | 8 | 294 | 370 | 447 | 497 | 575 | 652 | 729 |
| 174 | 165 | 183 | 167 |  |  | 6 | 2 | 8 | 305 | 383 | 463 | 515 | 595 | 675 | 755 |
| 180 | 171 | 189 | 178 |  |  | 4 | 4 | 8 | 315 | 396 | 479 | 533 | 616 | 698 | 781 |
| 186 | 177 | 195 | 191 |  |  | 2 | 6 | 8 | 326 | 409 | 495 | 551 | 636 | 722 | 807 |
| 192 | 182 | 202 | 203 |  |  |  | 8 | 8 | 336 | 422 | 511 | 568 | 657 | 745 | 833 |
| 198 | 189 | 209 | 216 |  | 4 | 6 |  | 10 |  | 436 | 527 | 586 | 677 | 768 | 859 |
| 204 | 195 | 216 | 230 |  | 2 | 8 |  | 10 |  | 449 | 543 | 604 | 698 | 792 | 885 |
| 210 | 201 | 222 | 244 |  |  | 10 |  | 10 |  | 462 | 559 | 622 | 718 | 815 | 911 |
| 216 | 207 | 228 | 258 |  |  | 8 | 2 | 10 |  | 475 | 575 | 639 | 739 | 838 | 937 |
| 222 | 212 | 235 | 272 |  |  | 6 | 4 | 10 |  |  | 591 | 657 | 759 | 861 | 963 |
| 228 | 217 | 241 | 287 |  |  | 4 | 6 | 10 |  |  | 606 | 675 | 780 | 885 | 990 |
| 234 | 224 | 247 | 302 |  |  | 2 | 8 | 10 |  |  | 622 | 693 | 800 | 908 | 1016 |
| 240 | 229 | 254 | 318 |  |  |  | 10 | 10 |  |  | 638 | 710 | 821 | 931 | 1042 |
| 246 | 236 | 261 | 336 |  | 2 | 10 |  | 12 |  |  |  | 728 | 841 | 954 | 1068 |
| 252 | 241 | 267 | 352 |  |  | 12 |  | 12 |  |  |  | 746 | 862 | 978 | 1094 |
| 258 | 247 | 274 | 370 |  |  | 10 | 2 | 12 |  |  |  |  | 882 | 1001 | 1120 |
| 264 | 253 | 280 | 387 |  |  | 8 | 4 | 12 |  |  |  |  | 903 | 1024 | 1146 |
| 270 | 259 | 287 | 405 |  |  | 6 | 6 | 12 |  |  |  |  | 923 | 1048 | 1172 |
| 276 | 264 | 291 | 423 |  |  | 4 | 8 | 12 |  |  |  |  | 944 | 1071 | 1198 |
| 282 | 271 | 299 | 442 |  |  | 2 | 10 | 12 |  |  |  |  |  | 1094 | 1224 |
| 288 | 275 | 304 | 461 |  |  |  | 12 | 12 |  |  |  |  |  | 1117 | 1250 |
| 294 | 283 | 312 | 480 |  |  | 14 |  | 14 |  |  |  |  |  | 1141 | 1276 |
| 300 | 289 | 319 | 496 |  |  | 12 | 2 | 14 |  |  |  |  |  | 1164 | 1302 |
| 306 | 294 | 325 | 516 |  |  | 10 | 4 | 14 |  |  |  |  |  | 1187 | 1328 |
| 312 | 300 | 332 | 536 |  |  | 8 | 6 | 14 |  |  |  |  |  | 1211 | 1354 |

[^1]

Figure 5. Pipe-Arch


| $\begin{aligned} & \text { Span, } \\ & \text { Ft.-In. } \end{aligned}$ | $\begin{gathered} \text { Rise, } \\ \text { Ft.-In. } \end{gathered}$ | Pi | Total Plates | Number of Plates Per Ring ${ }^{(2)}$ |  |  |  |  |  |  |  | Approximate Weight Per Foot of Structure, Pounds ${ }^{(3)}$ |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |  | Specified Thickness, Inches |  |  |  |  |  |  |
|  |  |  |  | $\begin{aligned} & 9 \mathrm{Pi} \\ & \mathrm{C} \text { B } \end{aligned}$ | C 15 | B Pi | 18 |  | $\begin{gathered} 21 ~ P i \\ \text { B T } \end{gathered}$ |  |  | $\begin{gathered} 0.111 \\ \text { (12 Ga.) } \end{gathered}$ | $\begin{gathered} 0.140 \\ \text { (10 Ga.) } \end{gathered}$ | $\begin{gathered} 0.170 \\ (8 \text { Ga. }) \\ \hline \end{gathered}$ | $\begin{gathered} 0.188 \\ \text { (7 Ga.) } \end{gathered}$ | $\begin{gathered} 0.218 \\ \text { (5 Ga.) } \end{gathered}$ | $\begin{gathered} 0.249 \\ \text { (3 Ga.) } \end{gathered}$ | $\begin{gathered} 0.280 \\ (1 \mathrm{Ga} .) \end{gathered}$ |
| 6-1 | 4-7 | 66 | 5 | 2 |  | 11 |  | 1 |  |  |  | 116 | 145 | 176 | 195 | 226 | 256 | 286 |
| 6-4 | 4-9 | 69 | 5 | 2 |  | 1 |  | 2 |  |  |  | 124 | 152 | 184 | 204 | 236 | 268 | 299 |
| 6-9 | 4-11 | 72 | 5 | 2 |  |  | 1 | 2 |  |  |  | 126 | 158 | 192 | 213 | 246 | 279 | 312 |
| 7-0 | 5-1 | 75 | 5 | 2 |  |  | 1 | 1 | 1 |  |  | 131 | 165 | 200 | 222 | 257 | 291 | 326 |
| 7-3 | 5-3 | 78 | 5 | 2 |  |  | 1 |  | 2 |  |  | 137 | 172 | 207 | 231 | 267 | 303 | 339 |
| 7-8 | 5-5 | 81 | 5 | 2 |  |  |  |  | 12 |  |  | 142 | 178 | 215 | 240 | 277 | 314 | 352 |
| 7-11 | 5-7 | 84 | 5 | 2 |  |  |  |  | 11 |  | 1 | 147 | 185 | 223 | 249 | 287 | 326 | 365 |
| 8-2 | 5-9 | 87 | 5 | 2 |  |  |  |  | 1 |  | 2 | 152 | 191 | 231 | 258 | 298 | 338 | 378 |
| 8-7 | 5-11 | 90 | 5 | 2 |  |  |  |  |  | 1 | 2 | 158 | 198 | 239 | 266 | 308 | 349 | 391 |
| 8-10 | 6-1 | 93 | 6 | 2 |  | 1 |  | 2 |  | 1 |  | 163 | 205 | 247 | 275 | 318 | 361 | 404 |
| 9-4 | 6-3 | 96 | 7 | 21 |  | I | 1 | 2 |  |  |  | 168 | 211 | 255 | 284 | 328 | 372 | 417 |
| 9-6 | 6-5 | 99 | 7 | 21 |  |  | 1 | 3 |  |  |  | 173 | 218 | 263 | 293 | 339 | 384 | 430 |
| 9-9 | 6-7 | 102 | 7 | 21 |  |  | 1 | 2 | 1 |  |  | 179 | 224 | 271 | 302 | 349 | 396 | 443 |
| 10-3 | 6-9 | 105 | 7 | 2 |  | 2 |  | 2 | 1 |  |  | 184 | 231 | 279 | 311 | 359 | 407 | 456 |
| 10-8 | 6-11 | 108 | 7 | 2 |  | 1 | 1 | 2 | 1 |  |  | 189 | 238 | 287 | 320 | 369 | 419 | 469 |
| 10-11 | 7-1 | 111 | 7 | 2 |  | 1 | 1 | 1 | 2 |  |  | 194 | 244 | 295 | 329 | 380 | 431 | 482 |
| 11-5 | 7-3 | 114 | 7 | 2 |  |  | 2 | 1 | 2 |  |  | 200 | 251 | 303 | 337 | 390 | 442 | 495 |
| 11-7 | 7-5 | 117 | 7 | 2 |  |  | 2 |  | 3 |  |  | 205 | 257 | 311 | 346 | 400 | 454 | 508 |
| 11-10 | 7-7 | 120 | 7 | 2 |  |  | 2 |  | 2 |  | 1 | 210 | 264 | 319 | 355 | 410 | 466 | 521 |
| 12-4 | 7-9 | 123 | 7 | 2 |  |  | 1 |  | 12 |  | 1 | 215 | 271 | 327 | 364 | 421 | 477 | 534 |
| 12-6 | 7-11 | 126 | 7 | 2 |  |  | 1 |  | 11 |  | 2 | 221 | 277 | 335 | 373 | 431 | 489 | 547 |
| 12-8 | 8-1 | 129 | 7 | 2 |  |  | 1 |  | 1 |  | 3 | 226 | 284 | 343 | 382 | 441 | 501 | 560 |
| 12-10 | 8-4 | 132 | 8 | 2 |  |  |  | 3 | 11 |  |  | 231 | 290 | 351 | 391 | 451 | 512 | 573 |
| 13-3 | 9-4 | 138 | 7 |  | 2 |  | 2 |  |  |  | 3 | 242 | 304 | 367 | 408 | 472 | 535 | 599 |
| 13-6 | 9-6 | 141 | 8 |  | 2 |  | 2 | 3 | 1 |  |  | 247 | 310 | 375 | 417 | 482 | 547 | 612 |
| 14-0 | 9-8 | 144 | 8 |  | 2 |  | 1 | 3 | 11 |  |  | 252 | 317 | 383 | 426 | 492 | 559 | 625 |
| 14-2 | 9-10 | 147 | 8 |  | 2 |  | 1 | 2 | 12 |  |  | 257 | 323 | 391 | 435 | 503 | 570 | 638 |
| 14-5 | 10-0 | 150 | 8 |  | 2 |  | 1 | 1 | 13 |  |  | 263 | 330 | 399 | 444 | 513 | 582 | 651 |
| 14-11 | 10-2 | 153 | 8 |  | 2 |  |  | 1 | 23 |  |  | 268 | 337 | 407 | 453 | 523 | 594 | 664 |
| 15-4 | 10-4 | 156 | 8 |  | 2 |  |  | 1 | 13 | 1 |  | 273 | 343 | 415 | 462 | 534 | 605 | 677 |
| 15-7 | 10-6 | 159 | 8 |  | 2 |  |  |  | 14 | 1 |  | 278 | 350 | 423 | 471 | 544 | 617 | 690 |
| 15-10 | 10-8 | 162 | 8 |  | 2 |  |  |  | 13 | 1 | 1 | 284 | 356 | 431 | 480 | 554 | 629 | 703 |
| 16-3 | 10-10 | 165 | 8 |  | 2 |  |  |  | 3 | 2 | 1 | 289 | 363 | 439 | 488 | 564 | 640 | 716 |
| 16-6 | 11-0 | 168 | 8 |  | 2 |  |  |  | 2 | 2 | 2 | 294 | 370 | 447 | 497 | 575 | 652 | 729 |
| 17-0 | 11-2 | 171 | 9 |  | 2 | 1 | 2 |  | 2 |  | 2 | 299 | 376 | 455 | 506 | 585 | 663 | 742 |
| 17-2 | 11-4 | 174 | 9 |  | 2 | 1 | 2 |  | 1 |  | 3 | 305 | 383 | 463 | 515 | 595 | 675 | 755 |
| 17-5 | 11-6 | 177 | 9 |  | 2 | 1 | 2 |  |  |  | 4 | 310 | 389 | 471 | 524 | 605 | 687 | 768 |
| 17-11 | 11-8 | 180 | 9 |  | 2 |  | 3 |  |  |  | 4 | 315 | 396 | 479 | 533 | 616 | 698 | 781 |
| 18-1 | 11-10 | 183 | 10 |  | 2 |  | 3 | 2 | 3 |  |  | 320 | 403 | 487 | 542 | 626 | 710 | 794 |
| 18-7 | 12-0 | 186 | 10 |  | 2 |  | 2 | 2 | 13 |  |  | 326 | 409 | 495 | 551 | 636 | 722 | 807 |
| 18-9 | 12-2 | 189 | 10 |  | 2 |  | 2 | 1 | 14 |  |  | 331 | 416 | 503 | 559 | 646 | 733 | 820 |
| 19-3 | 12-4 | 192 | 10 |  | 2 |  | 1 | 1 | 24 |  |  | 336 | 422 | 511 | 568 | 657 | 745 | 833 |
| 19-6 | 12-6 | 195 | 10 |  | 2 |  | 1 |  | 25 |  |  | 341 | 429 | 519 | 577 | 667 | 757 | 846 |
| 19-8 | 12-8 | 198 | 10 |  | 2 |  | 1 |  | 24 |  | 1 |  | 436 | 527 | 586 | 677 | 768 | 859 |
| 19-11 | 12-10 | 201 | 10 |  | 2 |  | 1 |  | 23 |  | 2 |  | 442 | 535 | 595 | 687 | 780 | 872 |
| 20-5 | 13-0 | 204 | 10 |  | 2 |  |  |  | 33 |  | 2 |  | 449 | 543 | 604 | 698 | 792 | 885 |
| 20-7 | 13-2 | 207 | 10 |  | 2 |  |  |  | 32 |  | 3 |  | 455 | 551 | 613 | 708 | 803 | 898 |

$$
\mathrm{C}=\text { Corner } \mathrm{B}=\text { Bottom } \mathrm{T}=\text { Top }
$$

${ }^{(1)}$ Dimensions are to inside crests of corrugations and are subject to manufacturing tolerances.
${ }^{(2)}$ These plate arrangements will be furnished unless noted otherwise on assembly drawings
${ }^{(3)}$ Galvanized, with bolts and nuts.
Some pipe-arch sizes with 18 -inch corner radius are not shown. Those not shown are almost duplicate sizes of pipe-arches shown with 31 -inch corner radius. The 31 -inch corner radius structures have a much lower $R_{1} / R_{c}$ ratio resulting in lower corner pressures. See design pages. Some pipe-arch structures are furnished with double curved plates.

| TABLE 21. MULTI-PLATE® PIPE-ARCH $6^{\prime \prime} \times 2^{\prime \prime}$ <br> AASHTO HEIGHT OF COVER LIMITS H-20, HS-20, H-25, HS-25 LIVE LOADS |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Span Diameter (Ft.-In.) | $\begin{gathered} \text { Rise } \\ \text { (Ft.-In.) } \end{gathered}$ | Minimum Cover (Inches) | Corner Radius (Inches) | $\begin{gathered} 0.111 \\ \text { (12Ga.) } \end{gathered}$ | $\begin{gathered} 0.140 \\ (10 \mathrm{Ga} .) \end{gathered}$ | $\begin{gathered} 0.170 \\ \text { ( } 8 \mathrm{Ga} . \text { ) } \end{gathered}$ | $\begin{gathered} 0.188 \\ \text { ( } 7 \mathrm{Ga} . \text { ) } \end{gathered}$ | $\begin{gathered} 0.218 \\ (5 \mathrm{Ga} .) \end{gathered}$ | $\begin{gathered} 0.249 \\ \text { (3 Ga.) } \end{gathered}$ | $\begin{gathered} 0.280 \\ (1 \text { Ga.) } \end{gathered}$ |
| (Maximum Cover Heights Shown in Feet) |  |  |  |  |  |  |  |  |  |  |
| 6-1 | 4-7 | 12 | 18 | 16 | 16 | 16 | 16 | 16 | 16 | 16 |
| 6-4 | 4-9 | 12 | 18 | 15 | 15 | 15 | 15 | 15 | 15 | 15 |
| 6-9 | 4-11 | 12 | 18 | 14 | 14 | 14 | 14 | 14 | 14 | 14 |
| 7-0 | 5-1 | 12 | 18 | 14 | 14 | 14 | 14 | 14 | 14 | 14 |
| 7-3 | 5-3 | 12 | 18 | 13 | 13 | 13 | 13 | 13 | 13 | 13 |
| 7-8 | 5-5 | 12 | 18 | 13 | 13 | 13 | 13 | 13 | 13 | 13 |
| 7-11 | 5-7 | 12 | 18 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| 8-2 | 5-9 | 18 | 18 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| 8-7 | 5-11 | 18 | 18 | 11 | 11 | 11 | 11 | 11 | 11 | 11 |
| 8-10 | 6-1 | 18 | 18 | 11 | 11 | 11 | 11 | 11 | 11 | 11 |
| 9-4 | 6-3 | 18 | 18 | 10 | 10 | 10 | 10 | 10 | 10 | 10 |
| 9-6 | 6-5 | 18 | 18 | 10 | 10 | 10 | 10 | 10 | 10 | 10 |
| 9-9 | 6-7 | 18 | 18 | 10 | 10 | 10 | 10 | 10 | 10 | 10 |
| 10-3 | 6-9 | 18 | 18 | 9 | 9 | 9 | 9 | 9 | 9 | 9 |
| 10-8 | 6-11 | 18 | 18 | 9 | 9 | 9 | 9 | 9 | 9 | 9 |
| 10-11 | 7-1 | 18 | 18 | 9 | 9 | 9 | 9 | 9 | 9 | 9 |
| 11-5 | 7-3 | 18 | 18 | 8 | 8 | 8 | 8 | 8 | 8 | 8 |
| 11-7 | 7-5 | 18 | 18 | 8 | 8 | 8 | 8 | 8 | 8 | 8 |
| 11-10 | 7-7 | 18 | 18 | 8 | 8 | 8 | 8 | 8 | 8 | 8 |
| 12-4 | 7-9 | 24 | 18 | 8 | 8 | 8 | 8 | 8 | 8 | 8 |
| 12-6 | 7-11 | 24 | 18 | 8 | 8 | 8 | 8 | 8 | 8 | 8 |
| 12-8 | 8-1 | 24 | 18 | 7 | 7 | 7 | 7 | 7 | 7 | 7 |
| 12-10 | 8-4 | 24 | 18 | 7 | 7 | 7 | 7 | 7 | 7 | 7 |
| 13-3 | 9-4 | 24 | 31 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| 13-6 | 9-6 | 24 | 31 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| 14-0 | 9-8 | 24 | 31 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| 14-2 | 9-10 | 24 | 31 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| 14-5 | 10-0 | 24 | 31 | 11 | 11 | 11 | 11 | 11 | 11 | 11 |
| 14-11 | 10-2 | 24 | 31 | 11 | 11 | 11 | 11 | 11 | 11 | 11 |
| 15-4 | 10-4 | 24 | 31 | 11 | 11 | 11 | 11 | 11 | 11 | 11 |
| 15-7 | 10-6 | 24 | 31 | 11 | 11 | 11 | 11 | 11 | 11 | 11 |
| 15-10 | 10-8 | 24 | 31 | 10 | 10 | 10 | 10 | 10 | 10 | 10 |
| 16-3 | 10-10 | 30 | 31 | 10 | 10 | 10 | 10 | 10 | 10 | 10 |
| 16-6 | 11-0 | 30 | 31 | 10 | 10 | 10 | 10 | 10 | 10 | 10 |
| 17-0 | 11-2 | 30 | 31 | 10 | 10 | 10 | 10 | 10 | 10 | 10 |
| 17-2 | 11-4 | 30 | 31 | 10 | 10 | 10 | 10 | 10 | 10 | 10 |
| 17-5 | 11-6 | 30 | 31 | 9 | 9 | 9 | 9 | 9 | 9 | 9 |
| 17-11 | 11-8 | 30 | 31 | 9 | 9 | 9 | 9 | 9 | 9 | 9 |
| 18-1 | 11-10 | 30 | 31 | 9 | 9 | 9 | 9 | 9 | 9 | 9 |
| 18-7 | 12-0 | 30 | 31 | 9 | 9 | 9 | 9 | 9 | 9 | 9 |
| 18-9 | 12-2 | 30 | 31 | 9 | 9 | 9 | 9 | 9 | 9 | 9 |
| 19-3 | 12-4 | 30 | 31 | N/A | 8 | 8 | 8 | 8 | 8 | 8 |
| 19-6 | 12-6 | 30 | 31 | N/A | 8 | 8 | 8 | 8 | 8 | 8 |
| 19-8 | 12-8 | 30 | 31 | N/A | 8 | 8 | 8 | 8 | 8 | 8 |
| 19-11 | 12-10 | 30 | 31 | N/A | 8 | 8 | 8 | 8 | 8 | 8 |
| 20-5 | 13-0 | 36 | 31 | N/A | 8 | 8 | 8 | 8 | 8 | 8 |
| 20-7 | 13-2 | 36 | 31 | N/A | 8 | 8 | 8 | 8 | 8 | 8 |

Notes:

1. Tables based upon AASHTO Sec. 12 Standard Specifications for Highway Bridges.
2. $\mathrm{H}-20, \mathrm{HS}-20, \mathrm{H}-25, \mathrm{HS}-25$ live loads.
3. Minimum cover is defined as the vertical distance from the top of the corrugated structure to the bottom of flexible or top of rigid pavement.
4. Minimum cover for off highway construction loads must be checked.

## Additional Notes for PIPE-ARCH HOC Table

1. Maximum cover requires minimum 4000 psf allowable bearing capacity for backfill around haunch of PIPE-ARCH.
2. Maximum cover limited by corner bearing pressure.

TABLE 22. PLATE ARRANGEMENT AND APPROXIMATE WEIGHT PER FOOT FOR SINGLE RADIUS MULTI-PLATE® ${ }^{\text {ARCH }}$

| Arch Arc Length Pi(1) | Number of Plates Per Ring ${ }^{(2)}$ |  |  |  |  |  | Approximate Weight Per Foot of Structure, Pounds ${ }^{(2)}$ |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  | Specified Thickness, Inches |  |  |  |  |  |  |
|  | 9 Pi | 15 Pi | 18 Pi | 21 Pi | 24 Pi | Total Plates | $\begin{gathered} 0.111 \\ \text { (12Ga.) } \end{gathered}$ | $\begin{gathered} 0.140 \\ \text { (10 Ga.) } \end{gathered}$ | $\begin{gathered} 0.170 \\ (8 \text { Ga. }) \end{gathered}$ | $\begin{gathered} 0.188 \\ (7 \mathrm{Ga} .) \end{gathered}$ | $\begin{gathered} 0.218 \\ (5 \mathrm{Ga} .) \end{gathered}$ | $\begin{gathered} 0.249 \\ (3 \mathrm{Ga} .) \end{gathered}$ | $\begin{gathered} 0.280 \\ (1 \text { Ga.) } \end{gathered}$ |
| 24 |  |  |  |  | 1 | 1 | 42 | 53 | 64 | 71 | 82 | 93 | 104 |
| 27 | 1 |  | 1 |  |  | 2 | 47 | 59 | 72 | 80 | 92 | 105 | 117 |
| 30 |  | 2 |  |  |  | 2 | 53 | 66 | 80 | 89 | 103 | 116 | 130 |
| 33 |  | 1 | 1 |  |  | 2 | 58 | 73 | 88 | 98 | 113 | 128 | 143 |
| 36 |  | 1 |  | 1 |  | 2 | 63 | 79 | 96 | 107 | 123 | 140 | 156 |
| 39 |  |  | 1 | 1 |  | 2 | 68 | 86 | 104 | 115 | 133 | 151 | 169 |
| 42 |  |  | 1 |  | 1 | 2 | 74 | 92 | 112 | 124 | 144 | 163 | 182 |
| 45 |  |  |  | 1 | 1 | 2 | 79 | 99 | 120 | 133 | 154 | 175 | 195 |
| 48 |  |  |  |  | 2 | 2 | 84 | 106 | 128 | 142 | 164 | 186 | 208 |
| 51 |  | 1 | 2 |  |  | 3 | 89 | 112 | 136 | 151 | 174 | 198 | 221 |
| 54 |  |  | 3 |  |  | 3 | 95 | 119 | 144 | 160 | 185 | 210 | 234 |
| 57 |  |  | 2 | 1 |  | 3 | 100 | 125 | 152 | 169 | 195 | 221 | 247 |
| 60 |  |  | 1 | 2 |  | 3 | 105 | 132 | 160 | 178 | 205 | 233 | 260 |
| 63 |  |  |  | 3 |  | 3 | 110 | 139 | 168 | 186 | 215 | 244 | 273 |
| 66 |  |  |  | 2 | 1 | 3 | 116 | 145 | 176 | 195 | 226 | 256 | 286 |
| 69 |  |  |  | 1 | 2 | 3 | 121 | 152 | 184 | 204 | 236 | 268 | 299 |
| 72 |  |  |  |  | 3 | 3 | 126 | 158 | 192 | 213 | 246 | 279 | 312 |
| 75 |  |  | 3 | 1 |  | 4 | 131 | 165 | 200 | 222 | 257 | 291 | 326 |
| 78 |  |  | 2 | 2 |  | 4 | 137 | 172 | 207 | 231 | 267 | 303 | 339 |
| 81 |  |  | 1 | 3 |  | 4 | 142 | 178 | 215 | 240 | 277 | 314 | 352 |
| 84 |  |  | 2 |  | 2 | 4 | 147 | 185 | 223 | 249 | 287 | 326 | 365 |
| 87 |  |  |  | 3 | 1 | 4 | 152 | 191 | 231 | 258 | 298 | 338 | 378 |
| 90 |  |  |  | 2 | 2 | 4 | 158 | 198 | 239 | 266 | 308 | 349 | 391 |
| 93 |  |  |  | 1 | 3 | 4 | 163 | 205 | 247 | 275 | 318 | 361 | 404 |
| 96 |  |  | 3 | 2 |  | 5 | 168 | 211 | 255 | 284 | 328 | 372 | 417 |
| 99 |  |  | 2 | 3 |  | 5 | 173 | 218 | 263 | 293 | 339 | 384 | 430 |
| 102 |  |  | 1 | 4 |  | 5 | 179 | 224 | 271 | 302 | 349 | 396 | 443 |
| 105 |  |  |  | 5 |  | 5 | 184 | 231 | 279 | 311 | 359 | 407 | 456 |
| 108 |  |  |  | 4 | 1 | 5 |  | 238 | 287 | 320 | 369 | 419 | 469 |
| 111 |  |  |  | 3 | 2 | 5 |  | 244 | 295 | 329 | 380 | 431 | 482 |
| 114 |  |  |  | 2 | 3 | 5 |  | 251 | 303 | 337 | 390 | 442 | 495 |
| 117 |  |  |  | 1 | 4 | 5 |  | 257 | 311 | 346 | 400 | 454 | 508 |
| 120 |  |  |  |  | 5 | 5 |  | 264 | 319 | 355 | 410 | 466 | 521 |
| 123 |  |  | 1 | 5 |  | 6 |  |  | 327 | 364 | 421 | 477 | 534 |
| 126 |  |  | 3 |  | 3 | 6 |  |  | 335 | 373 | 431 | 489 | 547 |
| 129 |  |  |  | 5 | 1 | 6 |  |  | 343 | 382 | 441 | 501 | 560 |
| 132 |  |  |  | 4 | 2 | 6 |  |  |  | 391 | 451 | 512 | 573 |
| 135 |  |  |  | 3 | 3 | 6 |  |  |  | 400 | 462 | 524 | 586 |
| 138 |  |  |  | 2 | 4 | 6 |  |  |  | 408 | 472 | 535 | 599 |
| 141 |  |  |  | 1 | 5 | 6 |  |  |  | 417 | 482 | 547 | 612 |
| 144 |  |  | 1 | 6 |  | 7 |  |  |  |  | 492 | 559 | 625 |
| 147 |  |  |  | 7 |  | 7 |  |  |  |  | 503 | 570 | 638 |

[^2]| TABLE 23. MULTI-PLATE ${ }^{\circledR}$ ARCHES ${ }^{(1)}$ |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Dimensions |  | Waterway Area Ft. ${ }^{2}$ | Rise/Span Ratio | Radius Inches | Nominal Arc Length Pi |
| Span, Feet | Rise, Ft.-In. |  |  |  |  |
| 6.0 | 1-10 | 7.9 | 0.30 | 41 | 27 |
|  | 2-4 | 10.0 | 0.38 | 37 | 30 |
|  | 3-2 | 15.0 | 0.53 | 36 | 36 |
| 7.0 | 2-5 | 12.1 | 0.34 | 45 | 33 |
|  | 2-10 | 14.9 | 0.41 | 43 | 36 |
|  | 3-8 | 20.4 | 0.52 | 42 | 42 |
| 8.0 | 2-11 | 17.0 | 0.36 | 51 | 39 |
|  | 3-4 | 20.3 | 0.42 | 49 | 42 |
|  | 4-2 | 26.6 | 0.52 | 48 | 48 |
| 9.0 | 2-11 | 19.2 | 0.33 | 59 | 42 |
|  | 3-11 | 26.5 | 0.43 | 55 | 48 |
|  | 4-8 | 33.6 | 0.52 | 54 | 54 |
| 10.0 | 3-6 | 25.4 | 0.35 | 64 | 48 |
|  | 4-5 | 33.5 | 0.44 | 61 | 54 |
|  | 5-3 | 41.4 | 0.52 | 60 | 60 |
| 11.0 | 3-6 | 27.8 | 0.32 | 73 | 51 |
|  | 4-6 | 36.9 | 0.41 | 68 | 57 |
|  | 5-9 | 50.0 | 0.52 | 66 | 66 |
| 12.0 | 4-1 | 35.3 | 0.34 | 78 | 57 |
|  | 5-0 | 45.2 | 0.42 | 73 | 63 |
|  | 6-3 | 59.4 | 0.52 | 72 | 72 |
| 13.0 | 4-1 | 38.1 | 0.33 | 87 | 60 |
|  | 5-1 | 48.9 | 0.40 | 81 | 66 |
|  | 6-9 | 69.7 | 0.52 | 78 | 78 |
| 14.0 | 4-8 | 47.0 | 0.31 | 91 | 66 |
|  | 5-7 | 58.5 | 0.38 | 86 | 72 |
|  | 7-3 | 80.7 | 0.44 | 84 | 84 |
| 15.0 | 4-8 | 48.9 | 0.52 | 101 | 69 |
|  | 5-8 | 62.8 | 0.33 | 93 | 75 |
|  | 6-7 | 74.8 | 0.44 | 91 | 81 |
|  | 7-9 | 92.6 | 0.52 | 90 | 90 |
| 16.0 | 5-3 | 60.1 | 0.31 | 105 | 75 |
|  | 7-1 | 86.2 | 0.42 | 97 | 87 |
|  | 8-4 | 105.3 | 0.52 | 96 | 96 |
| 17.0 | 5-3 | 63.4 | 0.31 | 115 | 78 |
|  | 7-2 | 91.9 | 0.42 | 103 | 90 |
|  | 8-10 | 118.8 | 0.52 | 102 | 102 |
| 18.0 | 5-9 | 74.8 | 0.32 | 119 | 84 |
|  | 7-8 | 104.6 | 0.43 | 109 | 96 |
|  | 8-11 | 126.0 | 0.50 | 108 | 105 |
| 19.0 | 6-4 | 87.1 | 0.33 | 123 | 90 |
|  | 8-3 | 118.1 | 0.43 | 115 | 102 |
|  | 9-5 | 140.7 | 0.50 | 114 | 111 |
| 20.0 | 6-4 | 91.0 | 0.32 | 133 | 93 |
|  | 8-3 | 124.4 | 0.42 | 122 | 105 |
|  | 10-0 | 156.3 | 0.50 | 120 | 117 |
| 21.0 | 6-11 | 104.6 | 0.33 | 137 | 99 |
|  | 8-10 | 139.2 | 0.42 | 128 | 111 |
|  | 10-6 | 172.6 | 0.50 | 126 | 123 |
| 22.0 | 6-11 | 109.3 | 0.32 | 146 | 102 |
|  | 8-11 | 145.9 | 0.40 | 135 | 114 |
|  | 11-0 | 189.8 | 0.50 | 132 | 129 |
| 23.0 | 8-0 | 133.6 | 0.35 | 147 | 111 |
|  | 9-10 | 171.1 | 0.43 | 140 | 123 |
|  | 11-6 | 207.8 | 0.50 | 138 | 135 |
| 24.0 | 8-6 | 149.4 | 0.36 | 152 | 117 |
|  | 10-4 | 188.3 | 0.43 | 146 | 129 |
|  | 12-0 | 226.6 | 0.50 | 144 | 141 |
| 25.0 | 8-7 | 155.6 | 0.34 | 160 | 120 |
|  | 10-10 | 206.3 | 0.43 | 152 | 135 |
|  | 12-6 | 246.2 | 0.50 | 150 | 147 |
| 26.0 | 8-7 | 161.4 | 0.33 | 169 | 123 |
|  | 11-0 | 214.9 | 0.42 | 158 | 138 |
|  | 13-1 | 266.7 | 0.50 | 156 | 153 |



Figure 6. Arch


MULTI-PLATE Arch Pedestrian Underpass

1) Dimensions are to inside crests of corrugations are are subject to manufacturing tolerances.
To determine proper gage, use Table 24 and design information found on Pages 13-18.
For additional arch sizes, see your Contech ${ }^{\circledR}$ representative.

| TABLE 24. MULTI-PLATE ${ }^{\oplus}$ ARCH $6^{\prime \prime}$ X $2^{\prime \prime}$ <br> AASHTO HEIGHT OF COVER LIMITS H-20, HS-20, H-25, HS-25 LIVE LOADS |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Span |  | Minimum |  |  |  | Thick | s in Inch | Gage) |  |  |  |
| (Ft.-In.) | (Ft.-In.) | Cover (Inches) | $\begin{gathered} 0.111 \\ \text { (12 Ga.) } \end{gathered}$ | $\begin{gathered} 0.140 \\ \text { (10 Ga.) } \end{gathered}$ | $0.170$ <br> (8 Ga.) | $\begin{gathered} 0.188 \\ (7 \mathrm{Ga} .) \end{gathered}$ | $\begin{gathered} 0.218 \\ (5 \mathrm{Ga} .) \end{gathered}$ | $0.249$ <br> (3 Ga.) | $\begin{gathered} 0.280 \\ (1 \mathrm{Ga} .) \end{gathered}$ | $\begin{aligned} & 0.318 \\ & (5 / 16) \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.375 \\ & (3 / 8) \end{aligned}$ |
| 6-0 | 1-10 | 12 | 39 | 57 | 75 | 86 | 103 | 122 | 133 | 214 | 257 |
|  | $\begin{aligned} & 2-4 \\ & 3-2 \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |
| 7-0 | $\begin{gathered} 2-5 \\ 2-10 \\ 3-8 \end{gathered}$ | 12 | 34 | 49 | 64 | 73 | 88 | 104 | 114 | 183 | 220 |
| 8-0 | $\begin{gathered} 2-11 \\ 3-4 \\ 4-2 \end{gathered}$ | 12 | 29 | 43 | 56 | 64 | 77 | 91 | 100 | 160 | 192 |
| 9-0 | $\begin{gathered} 2-11 \\ 3-11 \\ 4-8 \end{gathered}$ | 18 | 26 | 38 | 50 | 57 | 69 | 81 | 88 | 142 | 171 |
| 10-0 | $\begin{aligned} & 3-6 \\ & 4-5 \\ & 5-3 \end{aligned}$ | 18 | 26 | 38 | 50 | 57 | 69 | 81 | 88 | 142 | 172 |
| 11-0 | $\begin{aligned} & 3-6 \\ & 4-6 \\ & 5-9 \end{aligned}$ | 18 | 21 | 31 | 40 | 46 | 56 | 66 | 72 | 116 | 140 |
| 12-0 | $\begin{aligned} & 4-1 \\ & 5-0 \\ & 6-3 \end{aligned}$ | 18 | 19 | 28 | 37 | 43 | 51 | 61 | 66 | 107 | 128 |
| 13-0 | $\begin{aligned} & 4-1 \\ & 5-1 \\ & 6-9 \end{aligned}$ | 24 | 18 | 26 | 34 | 39 | 47 | 56 | 61 | 98 | 118 |
| 14-0 | $\begin{aligned} & 4-8 \\ & 5-7 \\ & 7-3 \end{aligned}$ | 24 | 17 | 24 | 32 | 36 | 44 | 52 | 57 | 91 | 110 |
| 15-0 | $\begin{aligned} & 4-8 \\ & 5-8 \\ & 6-7 \\ & 7-9 \end{aligned}$ | 24 | 15 | 22 | 30 | 34 | 41 | 48 | 53 | 85 | 102 |
| 16-0 | $\begin{aligned} & 5-3 \\ & 7-1 \\ & 8-4 \end{aligned}$ | 24 | 14 | 21 | 28 | 32 | 38 | 45 | 50 | 80 | 96 |
| 17-0 | $\begin{gathered} 5-3 \\ 7-2 \\ 8-10 \end{gathered}$ | 30 | 14 | 20 | 26 | 30 | 36 | 43 | 47 | 75 | 90 |
| 18-0 | $\begin{gathered} 5-9 \\ 7-8 \\ 8-11 \end{gathered}$ | 30 | 13 | 19 | 25 | 28 | 34 | 40 | 44 | 71 | 85 |
| 19-0 | $\begin{aligned} & 6-4 \\ & 8-3 \\ & 9-5 \end{aligned}$ | 30 | 12 | 18 | 23 | 27 | 32 | 38 | 42 | 67 | 81 |
| 20-0 | $\begin{gathered} 6-4 \\ 8-3 \\ 10-0 \end{gathered}$ | 30 |  | 17 | 22 | 25 | 31 | 36 | 40 | 64 | 77 |
| 21-0 | $\begin{aligned} & 6-11 \\ & 8-10 \\ & 10-6 \end{aligned}$ | 36 |  | 16 | 21 | 24 | 29 | 34 | 38 | 61 | 73 |
| 22-0 | $\begin{aligned} & 6-11 \\ & 8-11 \\ & 11-0 \end{aligned}$ | 36 |  |  | 20 | 23 | 28 | 33 | 36 | 58 | 70 |
| 23-0 | $\begin{gathered} 8-0 \\ 9-10 \\ 11-6 \end{gathered}$ | 36 |  |  | 19 | 22 | 27 | 31 | 34 | 55 | 67 |
| 24-0 | $\begin{gathered} 8-6 \\ 10-4 \\ 12-0 \end{gathered}$ | 36 |  |  | 18 | 21 | 25 | 30 | 33 | 53 | 64 |
| 25-0 | $\begin{gathered} 8-7 \\ 10-10 \\ 12-6 \end{gathered}$ | 42 |  |  |  | 20 | 24 | 29 | 32 | 49 | 60 |
| 26-0 | $\begin{gathered} 8-7 \\ 11-0 \\ 13-1 \end{gathered}$ | 42 |  |  |  |  | 23 | 28 | 30 | 46 | 56 |

Notes:

1. Tables based upon AASHTO Sec. 12 Standard Specifications for Highway Bridges.
2. H-20, HS-20, H-25, HS-25 Live Loads.
3. Minimum cover is defined as the vertical distance from the top of the corrugated structure to the bottom of flexible or top of rigid pavement.
4. Minimum cover for off highway construction loads must be checked.
5. Footing reactions provided by supplier.

| TABLE 25. MULTI-PLATE ${ }^{\text {® }}$ HORIZONTAL ELLIPSE ${ }^{(1)}$ |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Structure <br> Number ${ }^{(2)}$ | Span, Ft.-In. | Rise, Ft.-In. | Area, Sq. Ft. | $\begin{gathered} \mathbf{R}_{\mathbf{t}} \\ \text { Inches } \end{gathered}$ | $\begin{gathered} \mathbf{R}_{\mathrm{s}} \\ \text { Inches } \end{gathered}$ | Total Pi |
| 24E15 | 7-4 | 5-6 | 31.6 | 54 | 27 | 78 |
| 27 E 15 | 8-1 | 5-9 | 36.4 | 61 | 27 | 84 |
| 30E15 | 8-10 | 6-0 | 41.4 | 68 | 27 | 90 |
| 30E18 | 9-2 | 6-9 | 48.2 | 68 | 32 | 96 |
| 33E15 | 9-7 | 6-4 | 46.7 | 75 | 27 | 96 |
| 33 E 18 | 9-11 | 7-0 | 54.0 | 75 | 32 | 102 |
| 36 El 5 | 10-4 | 6-7 | 52.2 | 82 | 27 | 102 |
| 36E18 | 10-8 | 7-3 | 60.1 | 82 | 32 | 108 |
| 36E21 | 11-0 | 8-0 | 68.2 | 82 | 38 | 114 |
| 39 E 15 | 11-1 | 6-10 | 58.1 | 88 | 27 | 108 |
| 39 E 18 | 11-4 | 7-6 | 66.4 | 88 | 32 | 114 |
| 39 E 21 | 11-8 | 8-3 | 75.1 | 88 | 38 | 120 |
| $39 E 24$ | 12-0 | 8-11 | 84.1 | 88 | 43 | 126 |
| 42E15 | 11-9 | 7-1 | 64.2 | 95 | 27 | 114 |
| 42E18 | 12-1 | 7-10 | 73.0 | 95 | 32 | 120 |
| 42E21 | 12-5 | 8-6 | 82.2 | 95 | 38 | 126 |
| 42E24 | 12-9 | 9-2 | 91.7 | 95 | 43 | 132 |
| 45 E 15 | 12-6 | 7-4 | 70.5 | 102 | 27 | 120 |
| 45E18 | 12-10 | 8-1 | 79.9 | 102 | 32 | 126 |
| 45E21 | 13-2 | 8-9 | 89.6 | 102 | 38 | 132 |
| 45E24 | 13-6 | 9-6 | 99.6 | 102 | 43 | 138 |
| 48E18 | 13-7 | 8-4 | 87.1 | 109 | 32 | 132 |
| 48 E 21 | 13-11 | 9-0 | 97.3 | 109 | 38 | 138 |
| 48 E 24 | 14-3 | 9-9 | 107.8 | 109 | 43 | 144 |
| 48 E 27 | 14-7 | 10-5 | 118.7 | 109 | 49 | 150 |
| 48 E 30 | 14-11 | 11-2 | 129.9 | 109 | 54 | 156 |

(1) Dimensions are to inside crests of corrugations and are subject to manufacturing tolerances.
${ }^{(2)}$ Plate arrangements can be determined by the structure number, i.e., 45 E 21 has a 24 pi and 21 pi plate in the top and bottom $(24 \mathrm{pi}+21 \mathrm{pi}=45 \mathrm{pi})$ and a 21 pi plate in each side .

Note:
Horizontal ellipse shapes are intended for use in low cover applications where a relatively wide, low centered flow area is required. Because of their relatively large top radii, special attention must be directed to providing proper backfill support to maintain shape.


Figure 7. Horizontal Ellipse

| TABLE 26. MULTI-PLATE ${ }^{\circledR}$ HORIZONTAL ELLIPSE $6^{\prime \prime}$ X $2^{\prime \prime}$ AASHTO HEIGHT OF COVER LIMITS H-20, HS-20, H-25, HS-25 LIVE LOADS |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | 12 Gage ${ }^{(1)}$ |
|  |  |  |  | Maximum Cover (In Feet) Over Horizontal Ellipse |
| Structure Number | Span <br> Ft.-In. | Rise, Ft.-In. | Cover (Inches) | Pressure of 2 Tons per Ft. ${ }^{2}$ |
| 24E15 | 7-4 | 5-6 | 12 | 16 |
| 27E15 | 8-1 | 5-9 | 18 | 14 |
| 30 E 15 | 8-10 | 6-0 | 18 | 13 |
| 30E18 | 9-2 | 6-9 | 18 | 15 |
| 33 E 15 | 9-7 | 6-4 | 18 | 11 |
| 33 E 18 | 9-11 | 7-0 | 18 | 14 |
| 36E15 | 10-4 | 6-7 | 18 | 10 |
| 36E18 | 10-8 | 7-3 | 18 | 13 |
| 36E21 | 11-0 | 8-0 | 18 | 15 |
| $39 \mathrm{E15}$ | 11-1 | 6-10 | 18 | 10 |
| 39 E 18 | 11-4 | 7-6 | 18 | 12 |
| 39 E 21 | 11-8 | 8-3 | 18 | 14 |
| 39E24 | 12-0 | 8-11 | 18 | 16 |
| 42E15 | 11-9 | 7-1 | 18 | 9 |
| 42E18 | 12-1 | 7-10 | 24 | 11 |
| 42E21 | 12-5 | 8-6 | 24 | 13 |
| 42E24 | 12-9 | 9-2 | 24 | 15 |
| 45E15 | 12-6 | 7-4 | 24 | 8 |
| 45E18 | 12-10 | 8-1 | 24 | 10 |
| 45E21 | 13-2 | 8-9 | 24 | 12 |
| 45E24 | 13-6 | 9-6 | 24 | 14 |
| 48 E 18 | 13-7 | 8-4 | 24 | 9 |
| 48 E 21 | 13-11 | 9-0 | 24 | 11 |
| 48 E 24 | 14-3 | 9-9 | 24 | 13 |
| 48 E 27 | 14-7 | 10-5 | 24 | 14 |
| 48E30 | 14-11 | 11-2 | 24 | 16 |

(1) Heavier gages may be supplied.

## Notes:

1. Tables based upon AASHTO Sec. 12 Standard Specifications for Highway Bridges.
2. H-20, HS-20, H-25 \& HS-25 Live Loads.
3. Minimum cover is defined as the vertical distance from the top of the corrugated
structure to the bottom of flexible or top of rigid pavement.
4. Minimum cover for off highway construction loads must be checked.


| TABLE 27. MULTI-PLATE ${ }^{®}$ ( |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Span, <br> St.-In. | Rise, <br> Ft.-In. | Area, <br> Sq. Ft. | $\mathbf{R}_{\mathbf{t}}$ <br> Inches | $\mathbf{R}_{\mathbf{s}}$ <br> Inches | $\mathbf{R}_{\mathbf{c}}$ <br> Inches | $\mathbf{R}_{\mathbf{b}}$ <br> Inches |
| $12-2$ | $11-0$ | 107 | 67 | 93 | 38 | 134 |
| $12-11$ | $22-3$ | 116 | 73 | 95 | 38 | 144 |
| $13-2$ | $11-11$ | 126 | 73 | 103 | 38 | 159 |
| $13-10$ | $12-3$ | 136 | 77 | 108 | 38 | 164 |
| $14-1$ | $12-10$ | 147 | 77 | 115 | 38 | 182 |
| $14-6$ | $13-5$ | 158 | 78 | 130 | 38 | 174 |
| $14-10$ | $14-0$ | 169 | 79 | 136 | 38 | 192 |
| $15-6$ | $14-4$ | 180 | 84 | 138 | 38 | 201 |
| $15-9$ | $15-1$ | 192 | 83 | 150 | 38 | 212 |
| $16-4$ | $15-5$ | 204 | 86 | 157 | 38 | 215 |
| $16-5$ | $16-1$ | 217 | 88 | 158 | 38 | 271 |
| $16-9$ | $16-3$ | 224 | 89 | 167 | 38 | 247 |
| $17-3$ | $17-0$ | 239 | 90 | 174 | 47 | 215 |
| $18-4$ | $16-11$ | 252 | 100 | 157 | 47 | 249 |
| $19-2$ | $17-2$ | 266 | 105 | 156 | 47 | 264 |
| $19-6$ | $17-7$ | 280 | 107 | 158 | 47 | 297 |
| $20-4$ | $17-9$ | 295 | 113 | 156 | 47 | 314 |

${ }^{11}$ To nearest whole number. Dimensions are to inside crests and are subject to manufacturing tolerances. Smaller (junior) underpasses are also available.


MULTI-PLATE Underpass


Figure 8. Underpass
${ }^{(1)}$ Dimensions are to inside crests of corrugations and are subject to manufacturing tolerances.

| TABLE 28. PLATE ARRANGEMENT FOR MULTI-PLATE ${ }^{\circledR}$ UNDERPASS |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Span, Ft.In. ${ }^{(1)}$ | Rise, Ft.In. ${ }^{(1)}$ | Total Pi | Numbers of Nominal Pi Width Plates ${ }^{(2)}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  | Total Plates Per Ring |
|  |  |  | Top |  |  |  | Sides |  |  |  |  | Corners |  | Bottom |  |  |  |  |
|  |  |  | 15 | 18 | 21 | 24 | 9 | 15 | 18 | 21 | 24 | 15 | 18 | 15 | 18 | 21 | 24 |  |
| 12-2 | 11-0 | 141 |  | 1 | 1 |  |  |  |  | 2 |  | 2 |  | 2 |  |  |  | 8 |
| 12-11 | 11-3 | 147 |  |  | 2 |  |  |  |  | 2 |  | 2 |  | 1 | 1 |  |  | 8 |
| 13-2 | 11-11 | 153 |  |  | 2 |  |  |  |  |  | 2 | 2 |  | 1 | 1 |  |  | 8 |
| 13-10 | 12-3 | 159 |  |  | 1 | 1 |  |  |  |  | 2 | 2 |  |  | 2 |  |  | 8 |
| 14-1 | 12-10 | 165 |  |  | 1 | 1 | 2 |  | 2 |  |  | 2 |  |  | 2 |  |  | 10 |
| 14-6 | 13-5 | 171 |  |  |  | 2 | 2 |  | 2 |  |  | 2 |  |  | 1 | 1 |  | 10 |
| 14-10 | 14-0 | 177 |  |  |  | 2 |  | 4 |  |  |  | 2 |  |  | 1 | 1 |  | 10 |
| 15-6 | 14-4 | 18 | 1 | 2 |  |  |  | 4 |  |  |  | 2 |  |  |  | 2 |  | 11 |
| 15-9 | 15-1 | 189 | 1 | 2 |  |  |  | 2 | 2 |  |  | 2 |  |  |  | 2 |  | 11 |
| 16-4 | 15-5 | 195 |  | 3 |  |  |  | 2 | 2 |  |  | 2 |  |  |  | 1 | 1 | 11 |
| 16-5 | 16-1 | 201 |  | 2 | 1 |  |  |  | 4 |  |  | 2 |  |  |  | 2 |  | 11 |
| 16-9 | 16-3 | 204 |  | 2 | 1 |  |  |  | 4 |  |  | 2 |  |  |  | 1 | 1 | 11 |
| 17-3 | 17-0 | 210 |  | 2 | 1 |  |  |  | 4 |  |  |  | 2 |  |  | 1 | 1 | 11 |
| 18-4 | 16-11 | 216 |  | 1 | 2 |  |  |  | 4 |  |  |  | 2 |  |  |  | 2 | 11 |
| 19-2 | 17-2 | 222 |  |  | 3 |  |  |  | 4 |  |  |  | 2 | 1 | 2 |  |  | 12 |
| 19-6 | 17-7 | 228 |  |  | 3 |  |  |  | 2 | 2 |  |  | 2 | 1 | 2 |  |  | 12 |
| 20-4 | 17-9 | 234 |  |  | 2 | 1 |  |  | 2 | 2 |  |  | 2 |  | 3 |  |  | 12 |

${ }^{(1)}$ Dimensions are to inside crests of corrugations and are subject to manufacturing tolerances.
${ }^{(2)}$ These plate arrangements will be furnished unless noted otherwise on assembly drawings.
${ }^{(3)}$ Smaller (junior) underpasses are also available.

${ }^{(1)}$ Dimensions are to inside crests of corrugations and are subject to manufacturing tolerances.
${ }^{(2)}$ Galvanized, with bolts and nuts.

| TABLE 29 A. MULTI-PLATE ${ }^{@}$ UNDERPASS H-20, HS-20, H-25, HS-25 LIVE LOADS MAXIMUM |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Size ${ }^{(1)}$ <br> Bearing Span, Ft.-In | Rise, Ft.-In. | Radius, Inches R Corner | Minimum <br> Specified <br> Thickness <br> Required, Inches | Cover, Inches | Maximum Height of Cover Over Underpass for Corner Pressures of 2 Tons per Sq. Ft. |
| 12-2 | 11-0 | 38 | 0.111 | 24 | 22 |
| 12-11 | 11-3 | 38 |  |  | 20 |
| 13-2 | 11-11 | 38 |  |  | 20 |
| 13-10 | 12-3 | 38 |  |  | 19 |
| 14-1 | 12-10 | 38 |  |  | 19 |
| 14-6 | 13-5 | 38 |  |  | 19 |
| 14-10 | 14-0 | 38 |  |  | 19 |
| 15-6 | 14-4 | 38 |  |  | 15 |
| 15-9 | 15-1 | 38 | 0.111 | 24 | 15 |
| 16-4 | 15-5 | 38 | 0.140 | 36 | 15 |
| 16-5 | 16-1 | 38 |  |  | 14 |
| 19-9 | 16-3 | 38 |  |  | 14 |
| 17-3 | 17-0 | 47 | 0.140 |  | 17 |
| 18-4 | 16-11 | 47 | 0.170 |  | 16 |
| 192 | 17-2 | 47 | 0.170 |  | 15 |
| 19-6 | 17-7 | 47 | 0.170 |  | 15 |
| 20-4 | 17-9 | 47 | 0.188 | 36 | 14 |

[^3]

Golf Cart Underpass

## Galvanized Steel Structural Plate Specification

Scope: This specification covers the manufacture and installation of the galvanized steel structural plate structure detailed in the plans.

Material: The galvanized steel structural plate structure shall consist of plate and appurtenant items as shown on the plans and shall confirm to the requirements of AASHTO M 167 /ASTM A 761. All manufacturing processes, including corrugating, punching, curving and galvanizing, shall be performed within the United States using raw materials made in the United States.

Assembly bolts and nuts shall be galvanized and meet the provisions of ASTM A 449, Type 1 and ASTM A-563, Grade C, respectively.

Assembly: The structure shall be assembled in accordance with the shop drawings provided by the manufacturer and per the manufacturer's recommendations. Bolts shall be tightened using an applied torque of between 100 and 300 ft .-lbs.

Installation: The structure shall be installed in accordance with the plans and specifications, the manufacturer's recommendations, and the AASHTO Standard Specifications for Highway Bridges, Section 26 (Division II).

Backfill: The structure shall be backfilled using clean, well graded granular material that meets the requirements of AASHTO M 145 for soil classification A-1, A-2 or A-3. Backfill must be placed symmetrically on each side of the structure in 6 to 8 -inch lifts. Each lift shall be compacted to a minimum of 90 percent density per AASHTO T 99.


Hot-Dip Galvanizing Process

Note: Construction loads that exceed highway load limits are not allowed on the structure without approval from the Engineer.

## Galvanized Steel Key-Hole Sloł Structural Plate Specification

Scope: This specification covers the manufacture and installation of the galvanized steel structural plate structure detailed in the plans.

Material: The galvanized steel structural plate structure shall consist of plates and appurtenant items as shown on the plans and shall conform to the requirements of AASHTO M 167/ ASTM A761 except the longitudinal seam bolt holes shall be key-hole shaped as shown in the plans. All manufacturing processes including corrugating, punching, curving and galvanizing, shall be performed within the United States using raw materials made in the United States.

Assembly bolts and nuts shall be galvanized and meet the provisions of ASTM A 449, Type 1 and ASTM A-563, Grade C, respectively.

Assembly: The structure shall be assembled in accordance with the shop drawings provided by the manufacturer and per the manufacturer's recommendations. Bolts shall be tightened using an applied torque of between 100 and 300 ft .-lbs.

Installation: The structure shall be installed in accordance with the plans and specifications, the manufacturer's recommendations, and the AASHTO Standard Specifications for Highway Bridges, Section 26 (Division II.)

Backfill: The structure shall be backfilled using clean, well graded granular material that meets the requirements of AASHTO M 145 for soil classifications A-1. Backfill must be placed symmetrically on each side of the structure in 6- to 8 -inch lifts. Each lift shall be compacted to a minimum of 90 percent density per AASHTO T 180. Backfill limits shall be in accordance with the details shown on the plans Reference ASTM D 1557.

Note: Construction loads that exceed highway load limits are not allowed on the structure without approval from the Project Engineer.

## Installation

A successful installation is dependent on these five critical components being followed:

- Good foundation
- Use of structural backfill
- 8 " lifts of backfill evenly placed on both sides of the structure
- Adequate compaction of backfill
- Adequate minimum cover over the structure


## Required elements

Satisfactory site preparation, trench excavation and bedding and backfill operations are essential to develop the strength of any flexible conduit. In order to obtain proper strength while preventing settlement, it is necessary that the soil envelope around the structure be of good granular material, properly placed, and carefully compacted.

Pipe-arch and underpass shapes pose special installation problems not found in other shapes. These two shapes generate high corner bearing pressures against the side fill and foundation. Therefore, special installation care must be implemented to achieve a composite soil structure.

A qualified Engineer should be engaged to design a proper foundation, adequate bedding, and backfill.

```
DURING INSTALLATION AND PRIOR TO THE CONSTRUCTION OF PERMANENT EROSION CONTROL AND END TREATMENT PROTECTION, SPECIAL PRECAUTIONS MAY BE NECESSARY. THE STRUCTURE MUST BE PROTECTED FROM UNBALANCED LOADS AND FROM ANY STRUCTURAL LOADS OR HYDRAULIC FORCES THAT MAY BEND OR DISTORT THE UNSUPPORTED ENDS OF THE STRUCTURE. EROSION OR WASH OUT OF PREVIOUSLY PLACED SOIL SUPPORT MUST BE PREVENTED TO ENSURE THAT THE STRUCTURE MAINTAINS ITS LOAD CAPACITY.
```


## Trench excavation

If the adjacent embankment material is structurally adequate, the trench requires only a bottom clear width of the structure's span plus sufficient room for compaction equipment.

## Bedding

Proper bedding preparation is critical to both structure performance and service life. The bed should be constructed to avoid distortions that may create undesirable stresses in the structure and/or rapid deterioration of the roadway. The bed should be free of rock formations, protruding stones, and frozen matter that may cause unequal settlement.

It is recommended that the bedding be stable, well graded granular material. Placing the structure on the bedding surface is generally accomplished by one of the two following methods:

- Shaping the bedding surface to conform to the lower section of the structure
- Carefully tamping a granular or select material beneath the haunches to achieve a well-compacted condition

Using one of these two methods ensures satisfactory compaction beneath the haunches.

## Backfill

Satisfactory backfill material, proper placement and compaction are key factors in obtaining maximum strength and stability.

The backfill material should be free of rocks, frozen lumps, and foreign material that can cause hard spots or decompose to create voids. Backfill material should be well graded granular material that meets the requirements of AASHTO M 145 for soil classifications A-1, A-2, or A-3. Backfill must be placed symmetrically on each side of the structure in six-inch loose lifts. Each lift is to be compacted to a minimum of 90 percent density per AASHTO T 99.

A high percentage of silt or fine sand in the native soils suggests the need for a well graded granular backfill material to prevent soil migration.

During backfill, only small tracked vehicles (D-4 or smaller) should be near the structure as fill progresses above the crown and to the finished grade. The Engineer and Contractor are cautioned that the minimum cover may need to be increased to handle temporary construction vehicle loads (larger than D-4).
For more information, refer to ASTM A 807 and AASHTO Standard Specifications for Highway Bridges Div. II Construction Section 26.

## Bolting

If the plates are well aligned, the torque applied with a power wrench need not be excessive. Bolts should be torque initially to a minimum 100 foot pounds and a maximum 300 foot pounds. A good plate fit is far better than high torque.

Complete detailed assembly instructions and drawings are provided with each structure.

## Aluminum Structural Plate Lightweight and Lower Installed Cost

Contech Aluminum Structural Plate gives you all the advantages of steel MULTI-PLATE, plus the lightweight, which adds to the ease of installation when compared to traditional concrete structures.

Aluminum structural plate weighs $1 / 50$ as much as reinforced concrete pipe in an equivalent size. This weight factor reduces assembly and equipment costs, helps gain access to remote sites and allows easy handling of long, preassembled structures.

## Lower job site unloading costs

Lightweight plates and reinforcing ribs arrive at the job site in strapped and nested bundles. Individual plates and ribs are generally light enough to be handled by one worker. Bundles can be handled with light-duty lifting equipment.

## Lower job site assembly costs

Most structures contain plate and rib sizes that can be assembled without lifting equipment. As a quality assurance


Lifting of Aluminum Pipe Arch



Underpass


Pipe-Arch


Horizontal Ellipse


Single Radius Arch

## Product Details

## Description of plates

Aluminum Structural Plate's corrugation pattern has a 9-inch pitch and 2-1/2 inch depth. The corrugations are at right angles to the length of the structure.

Thickness. Nominal plate thicknesses are available from $0.125^{\prime \prime}$ to $0.250^{\prime \prime}$ in uniform increments of $0.025^{\prime \prime}$.
(Uncurved plates are available in $0.100^{\prime \prime}$ plate thickness.)
Lengths. Individual circumferential plate lengths are noted in terms of $N\left(N=9.625^{\prime \prime}\right.$ or $9-5 / 8$ or 3 pi). Standard plates are fabricated in net covering lengths in one " N " increments from:

8N (77.00"), through 20N (192.52").
The N nomenclature translated circumference directly into nominal diameter in inches. For example, two 10 N plates give a diameter of $60^{\prime \prime}(2 \times 10 \mathrm{~N} \times 3 \mathrm{pi})$, three 12 N plates $=108^{\prime \prime}(3 \times 12 \mathrm{~N} \times 3$ pi), etc. Various plate lengths are used to obtain a specific structure shape and size.

Widths. All standard plates have a net width of $4^{\prime}-6^{\prime \prime}$.



| TABLE 30. SECTION PROPERTIES OF PLATES ONLY ${ }^{1}$ |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $9^{\prime \prime}$ X 2-1/2" |  |  |  |  |  |
|  | CORRUGATION |  |  |  |  |$]$

${ }^{1}$ Design Yield Stress is 24 ksi .
${ }^{2} 0.100^{\prime \prime}$ Thickness can not be curved.

TABLE 31. PLATE \& RIB COMPOSITE SECTION PROPERTIES

| Rib Type | Metal Thickness, Inches |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0.125 | 0.150 | 0.175 | 0.200 | 0.225 | 0.250 |
|  | Plastic Moment Capacity, $\mathrm{M}_{\mathrm{p}}$ ( kip-ft./ft. ) |  |  |  |  |  |
| No Rib Type II | 2.65 | 3.18 | 3.71 | 4.24 | 4.77 | 5.30 |
|  | 4.62 | 5.46 | 6.04 | 6.61 | 7.17 | 7.74 |
|  | 6.18 | 7.25 | 7.94 | 8.60 | 9.25 | 9.87 |
|  | 7.41 | 8.66 | 9.48 | 10.26 | 11.00 | 11.71 |
|  | 10.63 | 12.13 | 13.08 | 14.05 | 15.03 | 16.02 |
| Type IV @ | 5.87 | 6.82 | 7.43 | 8.04 | 8.63 | 9.21 |
|  | 8.32 | 9.59 | 10.39 | 11.14 | 11.85 | 12.55 |
|  | 10.42 | 11.90 | 12.84 | 13.72 | 14.57 | 15.39 |
|  | 16.45 | 18.46 | 19.41 | 20.38 | 21.37 | 22.37 |
| Type VI | 8.74 | 9.51 | 10.24 | 10.95 | 11.64 | 12.32 |
|  | 13.76 | 14.33 | 15.16 | 16.19 | 17.36 | 17.48 |
|  | 20.09 | 20.56 | 20.79 | 21.30 | 21.74 | 22.58 |
|  | 32.24 | 34.35 | 36.46 | 38.54 | 39.88 | 40.63 |

TABLE 32. SECTION PROPERTIES OF ALSP REINFORCING RIB

|  | Type VI Rib | Type IV Rib | Type II Rib |
| :---: | :---: | :---: | :---: |
| Alloy | 6061-T6 | 6061-T6 | 6061-T6 |
| Area | 3.62 in. ${ }^{2}$ | 2.27 in. ${ }^{2}$ | 1.71 in. ${ }^{2}$ |
| Center of Mass | $\begin{aligned} & X_{c}=0.91 \text { inches } \\ & Y_{c}=2.27 \text { inches } \end{aligned}$ | $\begin{gathered} X_{c}=0.652 \text { inches } \\ Y_{c}=1.76 \text { inches } \end{gathered}$ | $\begin{gathered} X_{c}=0.645 \text { inches } \\ Y_{c}=1.02 \text { inches } \end{gathered}$ |
| Moment of Inertia | $\begin{aligned} & \mathrm{I}_{\mathrm{xc}}=9.700 \mathrm{in} .^{4} \\ & \mathrm{I}_{\mathrm{yc}}=1.014 \mathrm{in} .^{4} \end{aligned}$ | $\begin{aligned} & \mathrm{l}_{\mathrm{xc}}=3.555 \mathrm{in} .^{4} \\ & \mathrm{I}_{\mathrm{yc}}=1.050 \mathrm{in}^{4} \end{aligned}$ | $\begin{aligned} & \mathrm{I}_{\mathrm{xc}}=1.802 \mathrm{in} .^{4} \\ & \mathrm{I}_{\mathrm{yc}}=0.787 \mathrm{in}^{4} \end{aligned}$ |
| Radius of Gyration | $\begin{aligned} & R_{\mathrm{xc}}=1.636 \text { inches } \\ & R_{\mathrm{yc}}=0.529 \text { inches } \end{aligned}$ | $\begin{aligned} & R_{\mathrm{xc}}=1.251 \text { inches } \\ & R_{\mathrm{yc}}=0.680 \text { inches } \end{aligned}$ | $\begin{aligned} & R_{\mathrm{xc}}=1.026 \text { inches } \\ & R_{\mathrm{yc}}=0.678 \text { inches } \end{aligned}$ |
| Section Modulus | $\mathrm{S}_{\mathrm{x}}=4.38{\mathrm{in} .^{3}}$ | $\mathrm{S}_{\mathrm{x}}=1.90{\mathrm{in} .^{3}}$ | $\mathrm{S}_{\mathrm{x}}=1.046 \mathrm{in} .^{3}$ |
| Plastic Modulus | $\mathrm{Z}_{\mathrm{x}}=5.66 \mathrm{in}^{3}{ }^{3}$ | $\mathrm{Z}_{\mathrm{x}}=2.68 \mathrm{in}^{3}{ }^{3}$ | $\mathrm{Z}_{\mathrm{x}}=1.705 \mathrm{in} .^{3}$ |
| Plastic Moment | $M_{p}=16.52 \mathrm{kip}-\mathrm{ft}$. | $M_{p}=7.81$ kip-ft. | $M_{p}=4.97$ kip-ft. |
| Yield Strength | $\mathrm{F}_{\mathrm{y}}=35 \mathrm{ksi}$ | $\mathrm{F}_{\mathrm{y}}=35 \mathrm{ksi}$ | $\mathrm{F}_{\mathrm{y}}=35 \mathrm{ksi}$ |
| Tensile Strength | $\mathrm{F}_{\mathrm{u}}=38 \mathrm{ksi}$ | $\mathrm{F}_{\mathrm{u}}=38 \mathrm{ksi}$ | $\mathrm{F}_{\mathrm{u}}=38 \mathrm{ksi}$ |
| Minimum Curving Radius | 104 in . | 104 in . | 60 in . |



Type II Rib


Type IV Rib


Type VI Rib

Height of Cover and Details Tables - HS-20 Loading
Round, Vertical Ellipse

| TABLE 33. ROUND STRUCTURES (H-20, HS-20 LIVE LOAD) |  |  |  |  |  |  |  |  | TABLE 34. ROUND, ELLIPSE DETAILS |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Metal Thickness (Inches) — Reinforcing Rib Type-Rib Spacing (Inches) (Maximum Cover - Ft.) |  |  |  |  |  |  |  |  | EllipseDimensions(inches) |  | Total N |  |  |
|  |  | Approx. | Minimum Height-of-Cover (Feet) |  |  |  |  |  |  |  |  |  | Rib |
| Diameter |  | Area |  |  |  |  |  |  | Span | Rise | Structure | Round | Ellipse |
| (ft.-In.) | (inches) | (sq. ft.) | 1.25 | 1.50 | 2.00 | 2.50 | 3.00 | 3.50 |  |  |  |  |  |
| 6-0 | 72 | 27.5 | . 125 | . 125 | . 125 | . 125 | . 125 | . 125 | 67 | 75 | 24 |  |  |
|  |  |  | (37) | (37) | (37) | (37) | (37) | (37) |  |  |  |  |  |
| 6-6 | 78 | 32.4 | . 175 | . 125 | . 125 | . 125 | . 125 | . 125 | 73 | 81 | 26 |  |  |
| 7-0 | 84 | 37.8 | (50) | (32) | (32) | (32) | (32) | (32) | 79 | 88 | 28 |  |  |
| 7-6 | 90 | 43.6 | . 250 | . 150 | . 125 | . 125 | . 125 | . 125 | 85 | 94 | 30 |  |  |
| 8-0 | 96 | 49.7 | (64) | (37) | (28) | (28) | (28) | (28) | 91 | 101 | 32 |  |  |
| 8-6 | 102 | 56.3 |  | . 200 | . 125 | . 125 | . 125 | . 125 | 97 | 107 | 34 |  |  |
| 9-0 | 108 | 63.3 |  | (45) | (25) | (25) | (25) | (25) | 103 | 114 | 36 |  |  |
| 9-6 | 114 | 70.7 |  |  | . 125 | . 125 | . 125 | . 125 | 109 | 120 | 38 |  |  |
| 10-0 | 120 | 78.5 |  |  | (22) | (22) | (22) | (22) | 115 | 127 | 40 | 10 |  |
| 10-6 | 126 | 86.7 | .150-11-9 | .125-II-18 | .125-11-27 | . 125 | . 125 | . 125 | 120 | 133 | 42 | 10 |  |
| 11-0 | 132 | 95.4 | (27) | (20) | (20) | (20) | (20) | (20) | 126 | 139 | 44 | 10 |  |
| 11-6 | 138 | 104.4 |  | .125-11-9 | .125-11-27 | . 125 | . 125 | . 125 | 132 | 146 | 46 | 10 | 11 |
| 12-0 | 144 | 113.9 |  | (18) | (18) | (18) | (18) | (18) | 138 | 152 | 48 | 12 | 11 |
| 12-6 | 150 | 123.7 |  | .150-11-9 | .125-11-27 | . 150 | . 125 | . 125 | 142 | 157 | 50 | 12 | 12 |
| 13-0 | 156 | 134.0 |  | (23) | (17) | (23) | (17) | (17) | 148 | 164 | 52 | 12 | 12 |
| 13-6 | 162 | 144.7 |  | .200-11-9 | .125-11-18 | .125-11-27 | . 150 | . 150 | 153 | 170 | 54 | 12 | 13 |
| 14-0 | 168 | 155.7 |  | (29) | (16) | (16) | (21) | (21) | 159 | 176 | 56 | 12 | 13 |
| 14-6 | 174 | 167.2 |  | .250-II-9 | .125-II-9 | .125-11-27 | .125-11-27 | .125-11-54 | 165 | 18/3 | 58 | 13 | 14 |
| 15-0 | 180 | 179.1 |  | (34) | (15) | (15) | (15) | (15) | 171 | 189 | 60 | 13 | 14 |
| 15-6 | 186 | 191.4 |  |  | .125-II-9 | .125-11-27 | .150-11-54 | .150-11-54 | 177 | 195 | 62 | 14 | 15 |
| 16-0 | 192 | 204.2 |  |  | (14) | (14) | (18) | (18) | 182 | 202 | 64 | 14 | 15 |
| 16-6 | 198 | 217.3 |  |  | .150-II-9 | .150-11-27 | .150-11-27 | .150-11-27 | 189 | 209 | 66 | 15 | 16 |
| 17-0 | 204 | 230.8 |  |  | (17) | (17) | (17) | (17) | 195 | 215 | 68 | 15 | 16 |
| 17-6 | 210 | 274.8 | .200-VI-9 | .175-VI-9 | .175-IV-18 | .175-11-27 | .175-11-54 | .175-11-54 | 200 | 222 | 70 | 16 | 16 |
| 18-0 | 216 | 259.1 | (22) | (19) | (19) | (19) | (19) | (19) | 206 | 228 | 72 | 16 | 16 |
| 18-6 | 222 | 273.9 |  | .175-VI-9 | .175-VI-18 | .175-IV-27 | .175-11-54 | .175-11-54 | 212 | 235 | 74 | 16 | 17 |
| 19-0 | 228 | 289.1 |  | (18) | (18) | (18) | (18) | (18) | 217 | 241 | 76 | 18 | 18 |
| 19-6 | 234 | 304.7 |  | .200-VI-9 | .200-VI-18 | .200-IV-27 | .200-IV-54 | .200-IV-54 | 224 | 247 | 78 | 18 | 17 |
| 20-0 | 240 | 321.0 |  | (20) | (20) | (20) | (20) | (20) | 229 | 254 | 80 | 18 | 18 |
| 20-6 | 246 | 337.0 |  | .225-VI-9 | .225-VI-18 | .225-IV-27 | .225-II-27 | .225-II-27 | 235 | 260 | 82 | 18 | 19 |
| 21-0 | 252 | 354.0 |  | (22) | (22) | (22) | (22) | (22) | $\begin{array}{lllll}241 & 267 & 84 & 20 & 20\end{array}$ |  |  |  |  |
| Notes for Aluminum Structural Plate HOC Tables: <br> 1. Table based on AASHTO Sec. 12 Standard Specifications for Highway Bridges. <br> 2. $\mathrm{H}-20, \mathrm{HS}-20$ Live Load. (Call your local Contech representative for $\mathrm{H}-25$ and $\mathrm{HS}-25$ Loading.) <br> 3. Minimum cover is defined as the vertical distance from the top of the corrugated structure to the bottom of flexible or top of rigid pavement. <br> 4. Minimum cover for off highway construction loads must be checked. <br> 5. Greater cover heights possible with heavier gage and rib combinations. <br> 6. Plate and rib combinations shown meet or exceed AASHTO Sec. 12.6 Standard Specifications for Highway Bridges. <br> 7. Minimum cover heights < span/8 determined by moment capacity analysis. <br> 8. Contact your local Contech representative for information regarding vertical ellipse shapes. |  |  |  |  |  |  |  |  | Notes: <br> 1. $N=9.625^{\prime \prime}\left(9^{\left.5 / 8^{\prime \prime}\right)}\right.$. <br> 2. Dimensions are to inside corrugation crests and are subject to manufacturing tolerances. <br> 3. Minimum reinforcing rib length, if required. Ribs are not available for vertical ellipse structures less than 46 N . <br> 4. Areas shown are for round pipe. Areas for vertical ellipses are slightly less |  |  |  |  |



## Pipe-Arch

TABLE 35. PIPE-ARCH DETAILS $(1,2,3,6)$

| Span(Ft.-In.) | $\begin{gathered} \text { Rise } \\ (\text { Ft.-In. }) \end{gathered}$ | Approx. Area (Sq. Ft.) | Inside Radius (Inches) |  | Arc Length $\mathbf{N}^{(4)}$ |  |  | Total $\mathbf{N}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Crown |  |  | Invert |  |  |  |
|  |  |  | $\left(R_{t}\right)$ | ( $\mathrm{R}_{\mathrm{i}}$ ) | Crown | Haunch | Invert | Structure | $\begin{aligned} & \mathbf{R i b}^{(6)} \\ & (\mathrm{Min}) \end{aligned}$ |
| 6-7 | 5-8 | 29.6 | 41.5 | 69.9 | 8 | 7 | 3 | 25 |  |
| 6-11 | 5-9 | 31.9 | 43.7 | 102.9 | 9 | 7 | 3 | 26 |  |
| 7-3 | 5-11 | 34.3 | 45.6 | 188.3 | 10 | 7 | 3 | 27 |  |
| 7-9 | 6-0 | 36.8 | 51.6 | 83.8 | 9 | 7 | 5 | 28 |  |
| 8-1 | 6-1 | 39.3 | 53.3 | 108.1 | 10 | 7 | 5 | 29 |  |
| 8-5 | 6-3 | 41.9 | 54.9 | 150.1 | 11 | 7 | 5 | 30 |  |
| 8-10 | 6-4 | 44.5 | 63.3 | 93.0 | 10 | 7 | 7 | 31 | 11 |
| 9-3 | 6-5 | 47.1 | 64.4 | 112.6 | 11 | 7 | 7 | 32 | 10 |
| 9-7 | 6-6 | 49.9 | 65.4 | 141.6 | 12 | 7 | 7 | 33 | 11 |
| 9-11 | 6-8 | 52.7 | 66.4 | 188.7 | 13 | 7 | 7 | 34 | 10 |
| 10-3 | 6-9 | 55.5 | 67.4 | 278.8 | 14 | 7 | 7 | 35 | 11 |
| 10-9 | 6-10 | 58.4 | 77.5 | 139.6 | 13 | 7 | 9 | 36 | 12 |
| 11-1 | 7-0 | 61.4 | 77.8 | 172.0 | 14 | 7 | 9 | 37 | 11 |
| 11-5 | 7-1 | 64.4 | 78.2 | 222.0 | 15 | 7 | 9 | 38 | 12 |
| 11-9 | 7-2 | 67.5 | 78.7 | 309.5 | 16 | 7 | 9 | 39 | 13 |
| 12-3 | 7-3 | 70.5 | 90.8 | 165.2 | 15 | 7 | 11 | 40 | 14 |
| 12-7 | 7-5 | 73.7 | 90.5 | 200.0 | 16 | 7 | 11 | 41 | 13 |
| 12-11 | 7-6 | 77.0 | 90.4 | 251.7 | 17 | 7 | 11 | 42 | 14 |
| 13-1 | 8-2 | 83.0 | 88.8 | 143.6 | 18 | 6 | 13 | 43 | 13 |
| 13-1 | 8-4 | 86.8 | 81.7 | 300.8 | 21 | 6 | 11 | 44 | 14 |
| 13-11 | 8-5 | 90.3 | 100.4 | 132.0 | 18 | 6 | 15 | 45 | 13 |
| 14-0 | 8-7 | 94.2 | 90.3 | 215.7 | 21 | 6 | 13 | 46 | 14 |
| 13-11 | 9-5 | 101.5 | 86.2 | 159.3 | 23 | 5 | 14 | 47 | 14 |
| 14-3 | 9-7 | 105.7 | 87.2 | 176.3 | 24 | 5 | 14 | 48 | 13 |
| 14-8 | 9-8 | 109.9 | 90.9 | 166.2 | 24 | 5 | 15 | 49 | 13 |
| 14-11 | 9-10 | 114.2 | 91.8 | 183.0 | 25 | 5 | 15 | 50 | 14 |
| 15-4 | 10-0 | 118.6 | 95.5 | 173.0 | 25 | 5 | 16 | 51 | 14 |
| 15-7 | 10-2 | 123.1 | 96.4 | 189.6 | 26 | 5 | 16 | 52 | 15 |
| 16-1 | 10-4 | 127.6 | 100.2 | 179.7 | 26 | 5 | 17 | 53 | 15 |
| 16-4 | 10-6 | 132.3 | 101.0 | 196.1 | 27 | 5 | 17 | 54 | 14 |
| 16-9 | 10-8 | 136.9 | 105.0 | 186.5 | 27 | 5 | 18 | 55 | 16 |
| 17-0 | 10-10 | 141.8 | 105.7 | 202.5 | 28 | 5 | 18 | 56 | 17 |
| 17-3 | 11-0 | 146.7 | 106.5 | 221.7 | 29 | 5 | 18 | 57 | 17 |
| 17-9 | 11-2 | 151.6 | 110.4 | 208.9 | 29 | 5 | 19 | 58 | 16 |
| 18-0 | 11-4 | 156.7 | 111.1 | 227.3 | 30 | 5 | 19 | 59 | 17 |
| 18-5 | 11-6 | 161.7 | 115.8 | 215.3 | 30 | 5 | 20 | 60 | 17 |
| 18-8 | 11-8 | 167.0 | 115.8 | 233.7 | 31 | 5 | 20 | 61 | 18 |
| 19-2 | 11-9 | 172.2 | 119.9 | 221.5 | 31 | 5 | 21 | 62 | 18 |
| 19-5 | 11-11 | 177.6 | 120.5 | 239.7 | 32 | 5 | 21 | 63 | 19 |
| 19-10 | 12-1 | 182.9 | 124.7 | 227.7 | 32 | 5 | 22 | 64 | 19 |
| 20-1 | 12-3 | 188.5 | 125.2 | 245.3 | 33 | 5 | 22 | 65 | 18 |
| 20-1 | 12-6 | 194.4 | 122.5 | 310.8 | 35 | 5 | 21 | 66 | 18 |
| 20-10 | 12-7 | 199.7 | 130.0 | 251.2 | 34 | 5 | 23 | 67 | 19 |
| 21-1 | 12-9 | 205.5 | 130.5 | 270.9 | 35 | 5 | 23 | 68 | 19 |
| 21-6 | 12-11 | 211.2 | 134.8 | 257.3 | 35 | 5 | 24 | 69 | 20 |
| 20-1 | 13-11 | 216.6 | 124.0 | 225.4 | 34 | 7 | 20 | 68 | 19 |
| 20-7 | 14-3 | 224.0 | 126.2 | 257.6 | 36 | 7 | 20 | 70 | 19 |
| 21-5 | 14-7 | 241.5 | 133.0 | 238.6 | 36 | 7 | 22 | 72 | 19 |
| 21-11 | 14-11 | 254.7 | 135.0 | 270.0 | 38 | 7 | 22 | 74 | 19 |

## Notes

1. $N=9.625^{\prime \prime}\left(9-5 / 8^{\prime \prime}\right)$.
2. Dimensions are to inside corrugation crests and are subject to manufacturing tolerances.
3. To determine the proper gage, use information on Page 53, Table 36.
4. The Arc Length $N$ column reflects the peripheral length of a certain radius Actual plate make-up, in a ring for a pipe-arch structure, will vary because of multiple radii in a single plate.
5. Haunch Radius $\left(R_{h}\right)=31.75^{\prime \prime}$ except for the last four structures shown, which have a haunch radius $\left(R_{h}\right)=47.0^{\prime \prime}$
6. Minimum reinforcing rib length, if required.


TABLE 36. PIPE-ARCH STRUCTURES (H-20, HS-20 LIVE LOAD)

| TABLE 36. PIPE-ARCH STRUCTURES (H-20, HS-20 LIVE LOAD) |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Metal Thickness (Inches) - Reinforcing Rib Type — Rib Spacing (Inches) <br> (Maximum Cover-Ft.) |  |  |  |  |  |  |  |  |
| Span | Rise | Approx. |  | Minim | um Heigh | -of-Cover | (Feet) |  |
| (Ft.-In.) | (Ft.-In.) | (Sq. Ft.) | 1.25 | 1.50 | 2.00 | 2.50 | 3.00 | 3.50 |
| 6-7 | 5-8 | 29.6 | . 175 | . 125 | . 125 | . 125 | . 125 | . 125 |
| 6-11 | 5-9 | 31.9 | (24) | (24) | (24) | (24) | (24) | (24) |
| 7-3 | 5-11 | 34.3 | 250 | . 150 | . 125 | . 125 | . 125 | . 125 |
| 7-9 | 6-0 | 36.8 | (19) | (19) | (19) | (19) | (19) | (19) |
| 8-1 | 6-1 | 39.3 |  |  |  |  |  |  |
| 8-5 | 6-3 | 41.9 |  | . 200 | . 125 | . 125 | . 125 | . 125 |
| 8-10 | 6-4 | 44.5 |  | (16) | (16) | (16) | (16) | (16) |
| 9-3 | 6-5 | 47.1 | .125-11-9 | .125-II-27 | . 125 | . 125 | . 125 | . 125 |
| 9-7 | 6-6 | 49.9 | (15) | (15) | (15) | (15) | (15) | (15) |
| 9-11 | 6-8 | 52.7 |  |  |  |  |  |  |
| 10-3 | 6-9 | 55.5 |  | .150-II-18 | .125-II-27 | . 125 | . 125 | . 125 |
| 10-9 | 6-10 | 58.4 |  | (13) | (13) | (13) | (13) | (13) |
| 11-1 | 7-0 | 61.4 |  |  |  |  |  |  |
| 11-5 | 7-1 | 64.4 |  | .125-11-9 | .125-11-27 | . 125 | . 125 | . 125 |
| 11-9 | 7-2 | 67.5 |  | (13) | (13) | (13) | (13) | (13) |
| 12-3 | 7-3 | 70.5 |  |  | .125-11-27 | . 150 | . 125 | . 125 |
| 12-7 | 7-5 | 73.7 |  |  | (11) | (11) | (11) | (11) |
| 12-11 | 7-6 | 77.0 |  |  |  |  |  |  |
| 13-1 | 8-2 | 83.0 |  |  |  |  |  |  |
| 13-1 | 8-4 | 86.8 |  |  |  |  |  |  |
| 13-11 | 8-5 | 90.3 |  |  | .125-11-18 | .125-11-27 | . 125 | . 125 |
| 14-0 | 8-7 | 94.2 |  |  | (10) | (10) | (10) | (10) |
| 13-11 | 9-5 | 101.5 |  |  |  |  |  |  |
| 14-3 | 9-7 | 105.7 |  |  | .125-11-9 | .125-11-27 | . 125 | . 125 |
| 14-8 | 9-8 | 109.9 |  |  | (11) | (11) | (11) | (11) |
| 14-11 | 9-10 | 114.2 |  |  |  |  |  |  |
| 15-4 | 10-0 | 118.6 |  |  | .125-11-9 | .125-11-27 | . 150 | . 125 |
| 15-7 | 10-2 | 123.1 |  |  | (9) | (9) | (9) | (9) |
| 16-1 | 10-4 | 127.6 |  |  |  |  |  |  |
| 16-4 | 10-6 | 132.3 |  |  |  |  |  |  |
| 16-9 | 10-8 | 136.9 |  |  | .125-VI-18 | .125-11-18 | .125-11-54 | . 150 |
| 17-0 | 10-10 | 141.8 |  |  | (8) | (8) | (8) | (8) |
| 17-3 | 11-0 | 146.7 |  |  |  |  |  |  |
| 17-9 | 11-2 | 151.6 |  |  |  |  |  |  |
| 18-0 | 11-4 | 156.7 |  |  | .125-VI-27 | .125-IV-27 | .125-IV-54 | . 175 |
| 18-5 | 11-6 | 161.7 |  |  | (8) | (8) | (8) | (8) |
| 18-8 | 11-8 | 167.0 |  |  |  |  |  |  |
| 19-2 | 11-9 | 172.2 |  |  | .150-IV-9 | .150-IV-27 | .150-IV-54 | . 200 |
| 19-5 | 11-11 | 177.6 |  |  | (7) | (7) | (7) | (7) |
| 19-10 | 12-1 | 182.9 |  |  |  |  |  |  |
| 20-1 | 12-3 | 188.5 |  |  | .175-IV-9 | .175-IV-27 | .175-IV-54 | 200 |
| 20-1 | 12-6 | 194.4 |  |  | (7) | (7) | (7) | (7) |
| 20-1 | 13-11 | 199.7 |  |  |  |  |  |  |
| 20-7 | 14-3 | 205.5 |  |  |  |  |  |  |
| 20-10 | 12-7 | 211.2 |  |  |  |  |  |  |
| 21-1 | 12-9 | 216.6 |  |  | .150-VI-18 | .175-IV-18 | .150-IV-54 | .150-IV-54 |
| 21-6 | 12-11 | 224.0 |  |  | (11) | (11) | (1) | (1) |
| 21-5 | 14-7 | 241.5 |  |  |  |  |  |  |
| 21-11 | 14-11 | 254.7 |  |  |  |  |  |  |

Notes:

1. Tables based upon AASHTO Sec. 12 Standard Specifications for Highway Bridges.
2. H-20, HS-20 Live Loads. (Call your Contech representative for $\mathrm{HS}-25$ and $\mathrm{H}-25$ loading.)
3. Minimum cover is defined as the vertical distance from the top of the corrugated structure to the bottom of flexible or top of rigid pavement.
4. Minimum cover for off highway construction loads must be checked.
5. Plate and rib combinations shown meet or exceed AASHTO Sec. 12.6 Standard Specifications for Highway Bridges.
6. Minimum cover heights < span/8 determined by moment capacity analysis.
7. Backfill in haunch area min. 4,000 psf bearing capacity.

## Single Radius Arch

| Span (Ft.-In.) | $\begin{gathered} \text { Rise } \\ \text { (Ft.-In.) } \end{gathered}$ | TABLE 37. ARCH DETAILS (1,2,3,6) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Approx Area (Sq. Ft.) | Radius (Inches) | Rise/ <br> Span <br> Ratio | Total $\mathbf{N}$ |  | $\begin{gathered} \text { Span } \\ \text { (Ft.-In.) } \end{gathered}$ | $\begin{gathered} \text { Rise } \\ \text { (Ft.-In.) } \end{gathered}$ | Approx. Area (Sq. Ft.) | Radius (Inches) | Rise/ Span Ratio | Total N |  |
|  |  |  |  |  | Structure | Rib ${ }^{(4)}$ |  |  |  |  |  | Structure | Rib ${ }^{(4)}$ |
| 5-0 | 1-9 | 6.5 | 31.75 | . 36 | 8 |  | 17-0 | 5-3 | 63.5 | 114.25 | . 31 | 26 | 16 |
|  | 2-3 | 8.5 | 30.25 | . 44 | 9 |  |  | 6-3 | 77.9 | 107.00 | . 37 | 28 | 16 |
|  | 2-7 | 10.4 | 30.00 | . 52 | 10 |  |  | 7-2 | 91.7 | 103.50 | . 42 | 30 | 16 |
| 6-0 | 1-10 | 7.8 | 40.50 | . 30 | 9 |  |  | 8-0 | 105.2 | 102.25 | . 47 | 32 | 16 |
|  | 2-4 | 10.2 | 37.25 | . 38 | 10 |  |  | 8-10 | 118.7 | 102.00 | . 52 | 34 | 16 |
|  | 2-9 | 12.6 | 36.25 | . 46 | 11 |  | 18-0 | 5-9 | 74.8 | 118.75 | . 32 | 28 | 18 |
|  | 3-2 | 14.9 | 36.00 | . 52 | 12 |  |  | 6-9 | 89.9 | 112.50 | . 38 | 30 | 18 |
| 7-0 | 2-4 | 12.0 | 45.25 | . 34 | 11 |  |  | 7-8 | 104.5 | 109.25 | . 43 | 32 | 18 |
|  | 2-10 | 14.8 | 43.00 | . 40 | 12 |  |  | 8-6 | 118.8 | 108.25 | . 47 | 34 | 18 |
|  | 3-3 | 17.5 | 42.00 | . 46 | 13 |  |  | 8-11 | 125.9 | 108.00 | . 50 | 35 | 17 |
|  | 3-8 | 20.3 | 42.00 | . 52 | 14 |  | 19-0 | 6-4 | 86.9 | 123.50 | . 33 | 30 | 18 |
| 8-0 | 2-11 | 17.0 | 50.50 | . 36 | 13 |  |  | 7-4 | 102.7 | 118.00 | . 38 | 32 | 18 |
|  | 3-4 | 20.2 | 48.75 | . 42 | 14 |  |  | 8-2 | 118.0 | 115.25 | . 43 | 34 | 18 |
|  | 4-2 | 26.4 | 48.00 | . 52 | 16 |  |  | 9-0 | 133.2 | 114.25 | . 48 | 36 | 18 |
| 9-0 | 2-11 | 19.1 | 59.00 | . 33 | 14 | 8 |  | 9-5 | 140.7 | 114.00 | . 50 | 37 | 17 |
|  | 3-10 | 26.3 | 54.50 | . 43 | 16 |  | 20-0 | 6-4 | 91.2 | 132.50 | . 32 | 31 | 19 |
|  | 4-8 | 33.4 | 54.00 | . 50 | 18 |  |  | 7-4 | 108.4 | 125.75 | . 37 | 33 | 19 |
| 10-0 | 3-6 | 25.3 | 64.00 | . 35 | 16 | 10 |  | 8-3 | 124.4 | 122.25 | . 41 | 35 | 19 |
|  | 4-5 | 33.3 | 60.50 | . 44 | 18 | 10 |  | 9-2 | 140.4 | 120.50 | . 46 | 37 | 19 |
|  | 5-2 | 41.2 | 60.00 | . 52 | 20 | 9 |  | 10-0 | 156.3 | 120.00 | . 50 | 39 | 19 |
| 11-0 | 3-6 | 27.8 | 72.75 | . 32 | 17 | 11 |  | 10-4 | 164.2 | 120.00 | . 52 | 40 | 20 |
|  | 4-6 | 36.8 | 67.50 | . 41 | 19 | 11 | 21-0 | 6-4 | 95.4 | 142.00 | . 30 | 32 | 20 |
|  | 5-8 | 49.8 | 66.00 | . 52 | 22 | 10 |  | 7-5 | 113.5 | 133.75 | . 35 | 34 | 20 |
| 12-0 | 4-1 | 35.3 | 77.50 | . 34 | 19 | 11 |  | 8-4 | 130.7 | 129.25 | . 40 | 36 | 20 |
|  | 5-0 | 45.0 | 73.25 | . 42 | 21 | 11 |  | 9-3 | 147.6 | 127.50 | . 44 | 38 | 20 |
|  | 6-3 | 59.3 | 72.00 | . 52 | 24 | 12 |  | 10-1 | 164.3 | 126.00 | . 48 | 40 | 20 |
| 13-0 | 4-1 | 38.1 | 86.50 | . 31 | 20 | 12 |  | 10-10 | 181.0 | 126.00 | . 52 | 42 | 20 |
|  | 5-1 | 48.9 | 80.50 | . 39 | 22 | 12 | 22-0 | 6-11 | 109.2 | 142.25 | . 31 | 34 | 20 |
|  | 5-11 | 59.3 | 78.25 | . 46 | 24 | 12 |  | 7-11 | 127.9 | 139.00 | . 36 | 36 | 20 |
|  | 6-9 | 69.5 | 78.00 | . 52 | 26 | 12 |  | 8-11 | 146.0 | 135.00 | . 40 | 38 | 20 |
| 14-0 | 4-8 | 46.9 | 91.25 | . 33 | 22 | 14 |  | 9-9 | 163.6 | 133.00 | . 44 | 40 | 20 |
|  | 5-7 | 58.4 | 86.00 | . 40 | 24 | 14 |  | 10-7 | 181.1 | 132.00 | . 48 | 42 | 20 |
|  | 6-5 | 69.5 | 84.25 | . 46 | 26 | 14 |  | 11-5 | 198.6 | 132.00 | . 52 | 44 | 20 |
|  | 7-3 | 80.6 | 84.00 | . 52 | 28 | 14 | 23-0 | 7-6 | 123.8 | 151.00 | . 33 | 36 | 20 |
| 15-0 | 4-8 | 50.0 | 100.50 | . 31 | 23 | 15 |  | 8-0 | 133.6 | 147.25 | . 35 | 37 | 21 |
|  | 5-8 | 62.6 | 93.50 | . 38 | 25 | 15 |  | 8-6 | 143.2 | 144.50 | . 37 | 38 | 20 |
|  | 6-7 | 74.7 | 91.00 | . 44 | 27 | 15 |  | 8-11 | 152.7 | 142.25 | . 39 | 39 | 21 |
|  | 7-5 | 86.5 | 90.00 | . 49 | 29 | 15 |  | 9-5 | 162.0 | 140.75 | . 41 | 40 | 20 |
|  | 7-9 | 92.5 | 90.00 | . 52 | 30 | 14 |  | 9-10 | 171.3 | 139.50 | . 43 | 41 | 21 |
| 16-0 | 5-3 | 60.0 | 105.00 | . 32 | 25 | 15 |  | 10-3 | 180.5 | 139.00 | . 45 | 42 | 20 |
|  | 6-2 | 73.3 | 99.25 | . 39 | 27 | 15 |  | 10-8 | 189.6 | 138.25 | . 47 | 43 | 21 |
|  | 7-1 | 86.2 | 96.75 | . 44 | 29 | 15 |  | 11-1 | 198.8 | 138.0 | . 48 | 44 | 20 |
|  | 7-11 | 98.9 | 96.00 | . 49 | 31 | 15 |  | 11-6 | 207.9 | 138.00 | . 50 | 45 | 21 |
|  | 8-3 | 105.2 | 96.00 | . 52 | 32 | 14 |  | 11-11 | 217.1 | 138.00 | . 52 | 46 | 20 |

## Notes

1. $\mathrm{N}=9.625^{\prime \prime}\left(9-5 / 8^{\prime \prime}\right)$.

Dimensions to inside corrugation crests are subject to manufacturing tolerances
. To determine proper gage, use the information on Page 55, Table 38.
4. Reinforcing rib length, if required.
5. The aluminum receiving angle is a separate item.
6. Arch shapes shown are single radius with a rise/span ratio of 0.30 or greater.


TABLE 38. ARCH STRUCTURES (H-20, HS-20 LIVE LOAD)

| TABLE 38. ARCH STRUCTURES (H-20, HS-20 LIVE LOAD) |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Span Metal Thickness (Inches) - Reinforcing Rib Type-Rib Spacing (Inches) <br> RiseApprox. <br> Area <br>  <br> $\quad$(Maximum Cover-Ft.) <br> Minimum Height of Cover (feet)  |  |  |  |  |  |  |  |  |
| (Ft.-In.) | (Ft.-In.) | (Sq. Ft.) | 1.25 | 1.50 | 2.00 | 2.50 | 3.00 | 3.50 |
| 5-0 | 1-9 | 6.5 | . 125 | . 125 | . 125 | . 125 | . 125 | . 125 |
|  | 2-3 | 8.5 | (45) | (45) | (45) | (45) | (45) | (45) |
|  | 2-7 | 10.4 |  |  |  |  |  |  |
| 6-0 | $1-10$ $2-4$ | 7.8 10.2 | 0.13 | . 125 | . 125 | . 125 | .125 | .125 |
|  | 3-2 | 14.9 |  |  |  |  |  |  |
| 7-0 | 2-4 | 12.0 | . 175 | . 125 | . 125 | . 125 | . 125 | . 125 |
|  | 2-10 | 14.8 | (50) | (32) | (32) | (32) | (32) | (32) |
|  | 3-3 | 17.5 |  |  |  |  |  |  |
|  | 3-8 | 20.3 |  |  |  |  |  |  |
| 8-0 | 2-11 | 17.0 | . 250 | . 150 | . 125 | . 125 | . 125 | . 125 |
|  | 3-4 | 20.2 | (64) | (37) | (28) | (28) | (28) | (28) |
|  | 4-2 | 26.4 |  |  |  |  |  |  |
| 9-0 | 2-11 | 19.1 |  | . 200 | . 125 | . 125 | . 125 | . 125 |
|  | 3-10 | 26.3 |  | (45) | (25) | (25) | (25) | (25) |
|  | 4-8 | 33.4 |  |  |  |  |  |  |
| 10-0 | 3-6 | 25.3 | .125-11-9 | .125-II-18 | . 125 | . 125 | . 125 | . 125 |
|  | 4-5 | 33.3 | (22) | (22) | (22) | (22) | (22) | (22) |
|  | 5-2 | 41.2 |  |  |  |  |  |  |
| 11-0 | 3-6 | 27.8 |  | . 125 -II-18 | .125-II-27 | . 125 | . 125 | . 125 |
|  | 4-6 | 36.8 |  | (20) | (20) | (20) | (20) | (20) |
|  | 5-8 | 49.8 |  |  |  |  |  |  |
| 12-0 | 4-1 | 35.3 |  | .125-II-9 | .125-II-27 | . 125 | . 125 | . 125 |
|  | 5-0 | 45.0 |  | (18) | (18) | (18) | (18) | (18) |
|  | 6-3 | 59.3 |  |  |  |  |  |  |
| 13-0 | 4-1 | 38.1 |  | .150-II-9 | .125-11-27 | . 150 | . 125 | . 125 |
|  | 5-1 | 48.9 |  | (23) | (17) | (23) | (17) | (17) |
|  | 5-11 | 59.3 |  |  |  |  |  |  |
|  | 6-9 | 69.5 |  |  |  |  |  |  |
| 14-0 | 4-8 | 46.9 |  | 200-II-9 | .125-11-18 | .125-11-27 | . 125 | . 125 |
|  | 5-7 | 58.4 |  | (29) | (16) | (16) | (16) | (16) |
|  | 6-5 | 69.5 |  |  |  |  |  |  |
|  | 7-3 | 80.6 |  |  |  |  |  |  |
| 15-0 | 4-8 | 50.0 |  | .250-II-9 | .125-II-9 | . $125-11-27$ | . 125 | . 125 |
|  | 5-8 | 62.6 |  | (34) | (15) | (15) | (15) | (15) |
|  | 6-7 | 74.7 |  |  |  |  |  |  |
|  | 7-5 | 86.5 |  |  |  |  |  |  |
|  | 7-9 | 92.5 |  |  |  |  |  |  |
| 16-0 | 5-3 | 60.0 |  |  | .125-III-9 | . $125-11-27$ | . 150 | . 125 |
|  | 6-2 | 73.3 |  |  | (14) | (14) | (18) | (14) |
|  | 7-1 | 86.2 |  |  |  |  |  |  |
|  | 7-11 | 98.9 |  |  |  |  |  |  |
|  | 8-3 | 105.2 |  |  |  |  |  |  |
| 17-0 | 5-3 | 63.5 |  |  | .225-II-18 | .150-II-27 | . 175 | . 150 |
|  | 6-3 | 77.9 |  |  | (17) | (17) | (20) | (17) |
|  | 7-2 | 91.7 |  |  |  |  |  |  |
|  | 8-0 | 105.2 |  |  |  |  |  |  |
|  | 8-10 | 118.7 |  |  |  |  |  |  |
| 18-0 | 5-9 | 74.8 | .200-VI-9 | .150-VI-9 | .175-IV-18 | .125-1V-27 | . 200 | . 175 |
|  | 6-9 | 89.9 | (22) | (16) | (19) | (12) | (22) | (19) |
|  | 7-8 | 104.5 |  |  |  |  |  |  |
|  | 8-6 | 118.8 |  |  |  |  |  |  |
|  | 8-11 | 125.9 |  |  |  |  |  |  |
| 19-0 | 6-4 | 86.9 |  | .150-VI-9 | .125-VI-18 | .125-IV-27 | .125-IV-54 | .125-IV-54 |
|  | 7-4 | 102.7 |  | (15) | (11) | (11) | (11) | (11) |
|  | 8-2 | 118.0 |  |  |  |  |  |  |
|  | 9-0 | 133.2 |  |  |  |  |  |  |
|  | 9-5 | 140.7 |  |  |  |  |  |  |
| 20-0 | 6-4 | 91.2 |  | .150-VI-9 | .150-VI-9 | .150-1V-27 | .175-II-54 | . 200 |
|  | 7-4 | 108.4 |  | (15) | (15) | (15) | (16) | (20) |
|  | 8-3 | 124.4 |  |  |  |  |  |  |
|  | 9-2 | 140.4 |  |  |  |  |  |  |
|  | 10-0 | 156.3 |  |  |  |  |  |  |
|  | 10-4 | 164.2 |  |  |  |  |  |  |
| 21-0 | 6-4 | 95.4 |  | .175-VI-9 | .175-VI-18 | .175-IV-18 | .175-11-54 | . 225 |
|  | 7-5 | 113.5 |  | (16) | (16) | (16) | (16) | (22) |
|  | 8-4 | 130.7 |  |  |  |  |  |  |
|  | 9-3 | 147.6 |  |  |  |  |  |  |
|  | 10-1 | 164.3 |  |  |  |  |  |  |
|  | 10-10 | 181.0 |  |  |  |  |  |  |
| 22-0 | 6-11 | 109.2 |  | .225-VI-9 | . $175-\mathrm{VI}-18$ | .175-1V-18 | .175-IV-27 | 250 |
|  | 8-0 | 127.9 |  | (21) | (16) | (16) | (16) | (23) |
|  | 8-11 | 146.0 |  |  |  |  |  |  |
|  | 9-9 | 163.6 |  |  |  |  |  |  |
|  | 10-7 | 181.1 |  |  |  |  |  |  |
|  | 11-5 | 198.6 |  |  |  |  |  |  |
| 23-0 | $7-6$ | 123.8 |  |  | .250-VI-18 | .250-VI-18 | .225-IV-54 | .250-11-27 |
|  | 8-0 | 133.6 |  |  | (23) | (17) | (20) | (22) |
|  | 8-6 | 143.2 |  |  |  |  |  |  |
|  | 8-11 | 152.7 |  |  |  |  |  |  |
|  | 9-5 | 162.0 |  |  |  |  |  |  |
|  | 9-10 | 171.3 |  |  |  |  |  |  |
|  | 10-3 | 180.5 |  |  |  |  |  |  |
|  | 10-8 | 189.6 |  |  |  |  |  |  |
|  | 11-1 | 198.8 |  |  |  |  |  |  |
|  | 11-6 | 207.9 |  |  |  |  |  |  |
|  | 11-11 | 217.1 |  |  |  |  |  |  |

* Greater max. cover heights are available for each span by use of heavier gages.

Notes for Aluminum Structural Plate HOC Tables.

1. Tables based upon AASHTO Sec. 12 Standard Specifications for Highway Bridges.
2. H-20, HS-20 Live Loads. (Call your local Contech representative for $\mathrm{H}-25$ and $\mathrm{HS}-25$ Loading.)
3. Minimum cover is defined as the vertical distance from the top of the corrugated structure to the bottom of flexible or top of rigid pavement.
4. Minimum cover for off highway construction loads must be checked.
5. Plate and rib combinations shown meet or exceed AASHTO Sec. 12.6 Standard Specifications for Highway Bridges.
6. Minimum cover heights < span/8 determined by moment capacity analysis.
7. Greater cover heights possible with other plate thickness/rib combinations.
8. Arch footing reaction provided by supplier.


Aluminum Receiving Channel


## Underpass

## TABLE 39. PEDESTRIAN/ANIMAL UNDERPASS DETAILS ${ }^{(1,2,3,7)}$

| $\begin{gathered} \text { Span } \\ \text { (Ft.-In.) } \end{gathered}$ | $\begin{gathered} \text { Rise } \\ \text { (Ft.-In.) } \end{gathered}$ | Approx. Area (Sq. Ft.) | Inside Radius (Inches) ${ }^{(5)}$ |  |  | Arc Length (Inches) ${ }^{(4)}$ |  |  |  | Total N |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Crown ( $\mathrm{R}_{\mathrm{t}}$ ) | Side ( $\mathrm{R}_{\mathrm{s}}$ ) | Haunch ( $\mathrm{R}_{\mathrm{h}}$ ) | Crown | Side | Haunch | Bottom | Structure | Rib ${ }^{(6)}$ |
| 6-1 | 5-9 | 28 | 31.8 | 48.2 | 31.8 | 43.0 | 20.5 | 68.6 | 9.2 | 24 |  |
| 6-3 | 6-1 | 30 | 31.8 | 51.3 | 31.8 | 50.2 | 28.6 | 60.7 | 11.1 | 25 |  |
| 6-3 | 6-5 | 32 | 31.8 | 55.0 | 31.8 | 56.5 | 36.8 | 53.9 | 11.6 | 26 |  |
| 6-2 | 6-11 | 34 | 31.8 | 71.3 | 31.8 | 70.4 | 38.0 | 51.3 | 10.2 | 27 | N/A |
| 6-4 | 7-3 | 37 | 31.8 | 72.4 | 31.8 | 67.3 | 45.0 | 50.0 | 11.6 | 28 |  |
| 6-3 | 7-9 | 39 | 31.8 | 74.7 | 31.8 | 69.2 | 54.0 | 45.7 | 9.8 | 29 |  |
| 6-5 | 8-1 | 42 | 31.8 | 75.8 | 31.8 | 66.9 | 60.5 | 44.4 | 11.3 | 30 |  |

## TABLE 40. VEHICULAR UNDERPASS DETAILS(12,3,7)

| TABLE 40. VEHICULAR UNDERPASS DETAILS $(1,2,3,7)$ |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Span <br> (Ft.-In.) | Rise (Ft.-In | Approx. Area <br> .)(Sq. Ft.) | Inside Radius (Inches) |  |  |  |  | Arc Length $\mathbf{N}$ |  |  | Total N |  |
|  |  |  | Crown ( $\mathrm{R}_{\mathrm{t}}$ ) | Side ( $\mathrm{R}_{\mathrm{s}}$ ) | Haunch ( $\mathrm{R}_{\mathrm{h}}$ ) | ( $\mathrm{R}_{\mathrm{i}}$ ) | Crown | Side | Inver <br> Haunch | Bottom | Structure | Rib ${ }^{(6)}$ |
| 12-1 | 11-0 | 107.5 | 70 | 83 | 38 | 133 | 13 | 8 | 4 | 10 | 47 | 10 |
| 12-10 | 11-2 | 116.6 | 75 | 83 | 38 | 144 | 14 | 8 | 4 | 11 | 49 | 11 |
| 13-0 | 12-0 | 126.7 | 74 | 93 | 38 | 152 | 14 | 9 | 4 | 11 | 51 | 11 |
| 13-8 | 12-4 | 136.7 | 78 | 96 | 38 | 158 | 15 | 9 | 4 | 12 | 53 | 12 |
| 14-0 | 12-11 | 147.4 | 79 | 102 | 38 | 174 | 15 | 10 | 4 | 12 | 55 | 12 |
| 14-6 | 13-5 | 156.7 | 76 | 144 | 38 | 192 | 16 | 9 | 5 | 13 | 57 | 12 |
| 14-9 | 14-1 | 169.8 | 81 | 118 | 38 | 182 | 16 | 11 | 4 | 13 | 59 | 12 |
| 15-5 | 14-5 | 179.2 | 80 | 158 | 38 | 217 | 17 | 10 | 5 | 14 | 61 | 13 |
| 15-7 | 15-2 | 193.6 | 85 | 132 | 38 | 195 | 17 | 12 | 4 | 14 | 63 | 13 |
| 16-3 | 15-6 | 206.1 | 89 | 135 | 38 | 201 | 18 | 12 | 4 | 15 | 65 | 13 |
| 16-5 | 16-0 | 216.0 | 87 | 170 | 38 | 330 | 19 | 12 | 5 | 14 | 67 | 13 |
| 16-8 | 16-4 | 222.3 | 86 | 188 | 38 | 277 | 19 | 12 | 5 | 15 | 68 | 13 |
| 17-3 | 17-1 | 238.4 | 89 | 182 | 48 | 219 | 19 | 12 | 6 | 15 | 70 | 16 |
| 18-5 | 16-11 | 252.0 | 99 | 159 | 48 | 262 | 20 | 12 | 6 | 16 | 72 | 17 |
| 19-0 | 17-3 | 266.0 | 103 | 166 | 48 | 264 | 21 | 12 | 6 | 17 | 74 | 18 |
| 19-7 | 17-7 | 280.2 | 107 | 160 | 48 | 315 | 21 | 13 | 6 | 17 | 76 | 18 |
| 20-5 | 17-9 | 294.4 | 113 | 158 | 48 | 336 | 22 | 13 | 6 | 18 | 78 | 19 |

Notes

1. $N=9.625^{\prime \prime}\left(9-5 / 8^{\prime \prime}\right)$.
2. Dimensions are to inside corrugation crests and are subject to manufacturing tolerances. The designer should allow sufficient clearance for manufacturing tolerances and installation deflection.
3. To determine proper gage, use information on Page 57, Table 41.
4. The Arc Length $N$ or Inches column reflects the peripheral length of a certain radius. Actual plate make-up, in a ring for an underpass structure, will vary because of multiple radii in a single plate.
5. The bottoms of pedestrian/animal underpasses are nearly flat.
6. Mimimum reinforcing rib length, if required. (Ribs are not available for pedestrian underpass shapes.)
7. See sidefill and foundation design on Page 57.


Pedestrian Underpass


Vehicular Underpass

TABLE 41. UNDERPASS STRUCTURES (H-20, HS-20 LIVE LOAD)
Metal Thickness (Inches) - Reinforcing Rib Type - Rib Spacing (Inches)
(Maximum Cover - Ft.)

| $\begin{gathered} \text { Span } \\ (\mathrm{Ft} .-\mathrm{In} .) \end{gathered}$ | $\begin{gathered} \text { Rise } \\ \text { (Ft.-In.) } \end{gathered}$ | Approx. Area (Sq. Ft.) | Minimum Height-of-Cover (Feet) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 1.25 | 1.50 | 2.00 | 2.50 | 3.00 | 3.50 |
| 6-1 | 5-9 | 28 | . 150 | . 125 | . 125 | . 125 | . 125 | . 125 |
| 6-3 | 6-1 | 30 | (46) | (33) | (33) | (33) | (33) | (33) |
| 6-3 | 6-5 | 32 |  |  |  |  |  |  |
| 6-2 | 6-11 | 34 |  |  |  |  |  |  |
| 6-4 | 7-3 | 37 |  |  |  |  |  |  |
| 6-3 | 7-9 | 39 |  |  |  |  |  |  |
| 6-5 | 8-1 | 42 |  |  |  |  |  |  |
| 12-1 | 11-0 | 107.5 |  | .125-11-9 | .125-11-27 | . 125 | . 125 | . 125 |
|  |  |  |  | (18) | (18) | (18) | (18) | (18) |
| 12-10 | 11-2 | 116.6 |  | .150-II-9 | .125-11-27 | . 150 | . 125 | . 125 |
| 13-0 | 12-0 | 126.7 |  | (17) | (17) | (17) | (17) | (17) |
| 13-8 | 12-4 | 136.7 |  | 200-11-9 | .125-11-18 | .125-11-27 | .125-11-54 | .125-11-54 |
| 14-0 | 12-11 | 147.4 |  | (16) | (16) | (16) | (16) | (16) |
| 14-6 | 13-5 | 156.7 |  | .250-11-9 | .125-11-18 | .125-11-27 | . $125-11-54$ | .125-II-54 |
| 14-9 | 14-1 | 169.8 |  | (16) | (16) | (16) | (16) | (16) |
| 15-5 | 14-5 | 179.2 |  |  | .125-11-9 | .125-11-27 | .150-11-54 | .150-II-54 |
| 15-7 | 15-2 | 193.6 |  |  | (15) | (15) | (15) | (15) |
| 16-3 | 15-6 | 206.1 |  |  | .150-II-9 | .150-11-27 | .150-11-27 | .150-II-27 |
| 16-5 | 16-0 | 216.0 |  |  | (14) | (14) | (14) | (14) |
| 16-8 | 16-4 | 222.3 |  |  |  |  |  |  |
| 17-3 | 17-1 | 238.4 |  |  | .175-II-9 | .175-11-27 | .175-11-54 | . 175 |
| 18-5 | 16-11 | 252.0 |  |  | (9) | (9) | (9) | (9) |
| 19-0 | 17-3 | 266.0 |  | .200-VI-9 | .200-VI-18 | .200-II-18 | .200-11-54 | . 200 |
| 19-7 | 17-7 | 280.2 |  | (13) | (13) | (13) | (13) | (13) |



Underpass Section

Note

1. Maximum cover based on allowable corner bearing pressure of approximately $4,000 \mathrm{psf}(2 \mathrm{tsf})$.

## Notes for Tables 33, 36, 38, 41 and 43

1. The tables are presented for the designer's convenience in selecting metal thickness, reinforcing rib type and rib spacing for minimum cover applications. For structures with maximum covers greater than those shown in the table, heavier plate may possibly be used. Call your Contech representative.
2. Allowable cover (minimum and maximum) is measured from the outside valley of the crown plate to the bottom of flexible pavement or from the outside valley of the crown plate to the top of rigid pavement. Minimum cover is measured at the lowest fill area subjected to possible wheel loads (typically at the roadway shoulder). Minimum cover must be maintained in unpaved areas. Maximum cover is measured at the highest fill and/or the highest pavement elevation.
3. To find the minimum material requirements for the aluminum structural plate structure:
A. Locate the structure required.
B. Select the cover in the top row that is equal to or less than that required for the project.
C. The table selection shows metal thickness, rib type, rib spacing and maximum cover. Example: . 150-11-27 $=0.150^{\prime \prime}$ - thick plate structure with Type II ribs at $27^{\prime \prime}$ on centers on the crown.
4. The tables are based on the following:
A. Design specifications: Section 12 of AASHTO's Standard Specifications for Highway Bridges and ASTM B 790.
B. Standard $\mathrm{H}-20, \mathrm{HS}-20$ wheel loads. Consult a Contech representative for special loading conditions.
C. AASHTO M145 backfill materials classified as A-1, A-2, or A-3 compacted to 90\% density per AASHTO T99. Unit weight of soil: $120 \mathrm{Lb} . / \mathrm{Cu}$. Ft.
D. Yield point of aluminum: 24,000 psi for plate, 35,000 psi for reinforcing ribs.
E. Allowable corner bearing pressure of approximately 4,000 psf (2 tsf) for horizontal ellipses, pipe-arches, and underpasses.

## Sidefill and foundation design

Horizontal ellipse, pipe-arch and underpass shapes generate high bearing pressures against the sidefill and foundation in the areas of the smaller radius haunches. The height of cover is directly affected by these bearing pressures. The surrounding soil and foundation, therefore, must be checked to ensure that they are adequate to react against these pressures without excessive strain. Bearing pressures immediately adjacent to the plate can be approximated by the following formula:
$P_{c}=\left[\gamma\left(H_{c}\right)+L L\right] \quad\binom{R_{t}}{R_{h}}$
$\mathrm{P}_{\mathrm{c}}=$ Corner Bearing Pressure (Lb./Sq.Ft.)
$\gamma=$ Unit Weight of Soil (Lb./Cu. Ft.)
$\mathrm{H}_{\mathrm{c}}=$ Height-of-Cover (feet)
LL = Wheel Load Pressure at Cover Depth (Lb./Sq. Ft.)
$R_{\mathrm{t}}=$ Radius, crown (inches) (See Tables 34 through 39)
$R_{h}=$ Radius, haunch (inches) (See Tables 34 through 39)
( $R_{s}=R_{h}$ for Horizontal Ellipse)

## Ellipse

| TABLE 42. HORIZONTAL ELLIPSE DETAILS $(1,2,4)$ |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Structure <br> Number | $\begin{aligned} & \text { Span } \\ & \text { Ft.-In. } \end{aligned}$ | $\begin{gathered} \text { Rise } \\ \text { Ft.-In. } \end{gathered}$ | Area (Sq. Ft.) |  | Approx. $\mathrm{R}_{\mathrm{s}}$ Inches | Total <br> Structure | N ${ }^{\text {Rib }}{ }^{(3)}$ |
| 10 E 6 | 9-2 | 6-8 | 48.4 | 68 | 32 | 32 | 11 |
| 11 E 6 | 9-11 | 7-0 | 54.3 | 75 | 32 | 34 | 12 |
| 12 E 6 | 10-7 | 7-3 | 59.6 | 81 | 32 | 36 | 13 |
| 12 E 7 | 10-11 | 7-11 | 68.0 | 81 | 37 | 38 | 13 |
| 13 E 6 | 11-4 | 7-6 | 66.2 | 88 | 32 | 38 | 14 |
| 13 E 7 | 11-8 | 8-3 | 74.8 | 88 | 37 | 40 | 14 |
| 13 E 8 | 12-0 | 8-11 | 83.8 | 88 | 43 | 42 | 14 |
| 14 E 6 | 12-1 | 7-9 | 72.8 | 95 | 32 | 40 | 15 |
| 14 E 7 | 12-5 | 8-6 | 82.0 | 95 | 37 | 42 | 15 |
| 14 E 8 | 12-9 | 9-2 | 91.5 | 95 | 43 | 44 | 15 |
| 15 E 6 | 12-10 | 8-1 | 79.7 | 102 | 32 | 42 | 16 |
| 15 E 7 | 13-2 | 8-9 | 89.4 | 102 | 37 | 44 | 16 |
| 15 E8 | 13-6 | 9-6 | 99.4 | 102 | 43 | 46 | 16 |
| 16 E 6 | 13-7 | 8-4 | 86.8 | 109 | 32 | 44 | 17 |
| 16 E 7 | 13-11 | 9-0 | 97.1 | 109 | 37 | 46 | 17 |
| 16E8 | 14-3 | 9-9 | 107.6 | 109 | 43 | 48 | 17 |
| 16 E 9 | 14-7 | 10-5 | 118.5 | 109 | 49 | 50 | 17 |
| 16 E 10 | 14-11 | 11-2 | 129.7 | 109 | 54 | 52 | 17 |



Installation of Aluminum Horizontal Ellipses


Larger sizes are available. Contact your Contech representative.

## Notes

1. $N=9.625^{\prime \prime}\left(9{ }^{5 / 8 \prime}\right)$.
2. Dimensions are to inside corrugation crests and are subject to manufacturing tolerances.
3. Minimum reinforcing rib length, if required.

TABLE 43. HORIZONTAL ELLIPSE STRUCTURES (H-20, HS-20 LIVE LOAD)
Metal Thickness (Inches) — Reinforcing Rib Type-Rib Spacing (Inches) (Maximum Cover-Ft.)

| $\begin{gathered} \text { Span } \\ \text { (Ft.-In.) } \end{gathered}$ | $\begin{gathered} \text { Rise } \\ \text { (Ft.-In.) } \end{gathered}$ | Area (Sq. Ft.) | Approx. Minimum Height-of-Cover (Feet) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 1.25 | 1.50 | 2.00 | 2.50 | 3.00 | 3.50 |
| 9-2 | 6-8 | 48 | .125-II-9 | .125-II-18 | . 125 | . 125 | . 125 | . 125 |
| 9-11 | 7-0 | 54 | (14) | (14) | (14) | (14) | (14) | (14) |
| 10-7 | 7-3 | 60 | .150-11-9 | .125-11-18 | .225-II-27 | . 125 | . 125 | . 125 |
| 10-11 | 7-11 | 68 | (13) | (13) | (11) | (13) | (13) | (13) |
| 11-4 | 7-6 | 66 | .225-II-9 | .225-II-9 | .225-II-27 | . 125 | . 125 | . 125 |
| 11-8 | 8-3 | 75 | (1) | (11) | (1) | (11) | (11) | (11) |
| 12-0 | 8-11 | 84 |  |  |  |  |  |  |
| 12-1 | 7-9 | 73 |  |  |  |  |  |  |
| 12-5 | 8-6 | 82 |  | .150-II-9 | .125-II-27 | . 150 | . 125 | . 125 |
| 12-9 | 9-2 | 92 |  | (10) | (10) | (10) | (10) | (10) |
| 12-10 | 8-1 | 80 |  |  |  |  |  |  |
| 13-2 | 8-9 | 89 | .175-VI-18 | .175-VI-18 | .175-IV-27 | 125-II-27 | . 125 | . 125 |
| 13-6 | 9-6 | 99 | (9) | (9) | (9) | (9) | (9) | (9) |
| 13-7 | 8-4 | 87 |  |  |  |  |  |  |
| 13-11 | 9-0 | 97 |  |  |  |  |  |  |
| 14-3 | 9-9 | 108 | .125-VI-9 | .175-VI-18 | .175-IV-27 | 125-1I-27 | . 125 | . 125 |
| 14-7 | 10-5 | 119 | (11) | (11) | (11) | (11) | (11) | (11) |
| 14-11 | 11-2 | 130 |  |  |  |  |  |  |

## Notes for Aluminum Structural Plate HOC Tables

1. Tables based upon AASHTO Sec. 12 Standard Specifications for Highway Bridges.
2. H-20, HS-20 Live Loads. (Call your local Contech representative for H-25, HS-25 Loading.)
3. Minimum cover is defined as the vertical distance from the top of the corrugated structure to the bottom of flexible or top of rigid pavement.
4. Minimum cover for off highway construction loads must be checked.
5. Plate and rib combinations shown meet or exceed AASHTO Sec. 12.6 Standard Specifications for Highway Bridges
6. Minimum cover heights < span/8 determined by moment capacity analysis.
7. Backfill in haunch area min. 4,000 psf bearing capacity.

TABLE 44. APPROXIMATE HANDLING WEIGHT OF STRUCTURE (POUNDS PER FOOT)

| Total N | Nominal Thickness (Inches) |  |  |  |  |  | Bolts per Foot of Structure | Plates per Ring in a Structure* |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | . 125 | . 150 | . 175 | . 200 | . 225 | . 250 |  |  |
| 8 | 19 | 23 | 26 | 29 | 32 | 35 | 6.9 | 1 |
| 9 | 21 | 25 | 28 | 32 | 35 | 39 | 7.1 | 1 |
| 10 | 23 | 27 | 31 | 35 | 38 | 43 | 7.3 | 1 |
| 11 | 25 | 30 | 34 | 38 | 42 | 46 | 7.6 | 1 |
| 12 | 27 | 32 | 37 | 41 | 45 | 50 | 7.8 | 1 |
| 13 | 29 | 34 | 39 | 44 | 49 | 54 | 8.0 | 1 |
| 14 | 31 | 37 | 42 | 47 | 52 | 58 | 8.2 | 1 |
| 15 | 36 | 43 | 49 | 54 | 60 | 66 | 13.6 | 1 |
| 16 | 38 | 45 | 52 | 57 | 63 | 70 | 13.8 | 1 |
| 17 | 40 | 48 | 54 | 60 | 67 | 74 | 14.0 | 1 |
| 18 | 42 | 50 | 57 | 63 | 70 | 77 | 14.2 | 1 |
| 19 | 44 | 52 | 60 | 66 | 73 | 81 | 14.4 | 2 |
| 20 | 46 | 55 | 62 | 70 | 77 | 85 | 14.7 | 2 |
| 21 | 48 | 57 | 65 | 73 | 80 | 89 | 14.9 | 2 |
| 22 | 51 | 59 | 68 | 76 | 83 | 93 | 15.1 | 2 |
| 23 | 52 | 62 | 70 | 79 | 87 | 96 | 15.3 | 2 |
| 24 | 54 | 64 | 73 | 82 | 90 | 100 | 15.6 | 2 |
| 25 | 56 | 66 | 76 | 85 | 94 | 104 | 15.8 | 2 |
| 26 | 58 | 69 | 79 | 88 | 97 | 108 | 16.0 | 2 |
| 27 | 59 | 71 | 81 | 91 | 100 | 112 | 16.2 | 2 |
| 28 | 61 | 73 | 84 | 94 | 104 | 115 | 16.4 | 2 |
| 29 | 67 | 80 | 91 | 101 | 112 | 124 | 21.8 | 2 |
| 30 | 69 | 82 | 93 | 104 | 115 | 128 | 22.0 | 2 |
| 31 | 71 | 84 | 96 | 107 | 118 | 132 | 22.2 | 2 |
| 32 | 73 | 87 | 99 | 110 | 122 | 135 | 22.7 | 2 |
| 33 | 75 | 89 | 102 | 113 | 125 | 139 | 22.7 | 2 |
| 34 | 77 | 91 | 104 | 116 | 129 | 143 | 22.9 | 2 |
| 35 | 79 | 94 | 107 | 120 | 132 | 146 | 23.1 | 2 |
| 36 | 80 | 96 | 110 | 123 | 135 | 150 | 23.3 | 2 |
| 37 | 82 | 98 | 112 | 126 | 139 | 154 | 23.6 | 3 |
| 38 | 84 | 101 | 115 | 129 | 142 | 158 | 23.8 | 3 |
| 39 | 86 | 103 | 118 | 132 | 146 | 162 | 24.0 | 3 |
| 40 | 88 | 105 | 121 | 135 | 149 | 165 | 24.2 | 3 |
| 41 | 90 | 108 | 123 | 138 | 152 | 169 | 24.4 | 3 |
| 42 | 92 | 110 | 126 | 141 | 156 | 173 | 24.7 | 3 |
| 43 | 98 | 116 | 133 | 148 | 164 | 181 | 30.0 | 3 |
| 44 | 100 | 118 | 135 | 151 | 167 | 185 | 30.2 | 3 |
| 45 | 102 | 121 | 138 | 154 | 170 | 189 | 30.4 | 3 |
| 46 | 103 | 123 | 141 | 157 | 174 | 193 | 30.7 | 3 |
| 47 | 105 | 125 | 144 | 160 | 177 | 197 | 30.9 | 3 |
| 48 | 107 | 128 | 146 | 163 | 180 | 200 | 31.1 | 3 |
| 49 | 109 | 130 | 149 | 166 | 184 | 204 | 31.3 | 3 |
| 50 | 111 | 133 | 152 | 169 | 187 | 208 | 31.6 | 3 |
| 51 | 113 | 135 | 154 | 173 | 191 | 212 | 31.8 | 3 |
| 52 | 115 | 137 | 157 | 176 | 194 | 215 | 32.0 | 3 |
| 53 | 117 | 140 | 160 | 179 | 197 | 219 | 32.2 | 3 |
| 54 | 119 | 142 | 163 | 182 | 201 | 223 | 32.4 | 4 |
| 55 | 121 | 144 | 165 | 185 | 204 | 227 | 32.7 | 4 |
| 56 | 123 | 147 | 168 | 188 | 208 | 231 | 32.9 | 4 |
| 57 | 128 | 153 | 175 | 195 | 215 | 239 | 38.2 | 4 |
| 58 | 130 | 155 | 177 | 198 | 219 | 243 | 38.4 | 4 |
| 59 | 132 | 157 | 180 | 201 | 222 | 247 | 38.7 | 4 |
| 60 | 134 | 160 | 183 | 204 | 226 | 250 | 38.9 | 4 |
| 61 | 136 | 162 | 186 | 207 | 229 | 254 | 39.1 | 4 |
| 62 | 138 | 164 | 188 | 210 | 232 | 258 | 39.3 | 4 |
| 63 | 140 | 167 | 191 | 213 | 236 | 262 | 39.6 | 4 |
| 64 | 142 | 169 | 194 | 216 | 239 | 266 | 39.8 | 4 |
| 65 | 144 | 171 | 196 | 219 | 243 | 269 | 40.0 | 4 |
| 66 | 146 | 174 | 199 | 223 | 246 | 273 | 40.2 | 4 |
| 67 | 148 | 176 | 202 | 226 | 249 | 277 | 40.4 | 4 |
| 68 | 150 | 178 | 205 | 229 | 253 | 281 | 40.7 | 4 |
| 69 | 151 | 181 | 207 | 232 | 256 | 285 | 40.9 | 4 |
| 70 | 153 | 183 | 210 | 235 | 260 | 288 | 41.1 | 4 |
| 71 | 159 | 189 | 217 | 242 | 267 | 297 | 46.4 | 4 |
| 72 | 161 | 192 | 219 | 245 | 271 | 300 | 46.7 | 4 |
| 73 | 163 | 194 | 222 | 248 | 274 | 304 | 46.9 | 4 |
| 74 | 165 | 196 | 225 | 251 | 278 | 308 | 47.1 | 4 |
| 75 | 167 | 199 | 228 | 254 | 281 | 312 | 47.3 | 5 |
| 76 | 169 | 201 | 230 | 257 | 284 | 316 | 47.6 | 5 |
| 77 | 170 | 203 | 233 | 260 | 288 | 319 | 47.8 | 5 |
| 78 | 172 | 206 | 236 | 263 | 291 | 323 | 48.0 | 5 |

## Notes

1. Handling weights are approximate and include bolts and nuts.
2. To obtain the estimated total weight and bolt count per foot of the structure, use the Total N value of a structure (see Tables 34, 35, 37, 39, 40 and 42).
3. If a structure has reinforcing ribs, see Tables 45-47 for additional weight and bolt count.
4. For an arch, deduct 5.33 bolts per foot from column titled "Bolts per Foot of Structure."
5. On an arch, bolts and nuts for receiving angles are not included above.
6. Values in the column titled "Plates per Ring in a Structure" will be furnished unless noted otherwise on the assembly drawings.

* Round or arch only


## Reinforcing Rib Design

When circumferential ribs are used with Aluminum Structural Plate, they reinforce the structure to reduce minimum cover and provide added stiffness. These circumferential ribs are bolted to the structure's crown at spacings of $9^{\prime \prime}, 18^{\prime \prime}, 27^{\prime \prime}$ or $54^{\prime \prime}$ centers.

| TABLE 45. ADDED HANDLING WEIGHT AND ADDITIONAL BOLTS PER FOOT OF STRUCTURE FOR TYPE II REINFORCING RIB |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Total $\mathbf{N}$ of Rib | 9" o.c. |  | 18" o.c. |  | 27" o.c. |  | 54" o.c. |  |
|  | Wt/ft | Bolts/ft | Wt/ft | Bolts/ft | Wt/ft | Bolts/ft | Wt/ft | Bolts/ft |
| 5 | 15.7 | 7.3 | 7.7 | 3.3 | 5.0 | 2.0 | 2.3 | 0.7 |
| 6 | 18.6 | 8.6 | 9.1 | 3.9 | 5.9 | 2.3 | 2.7 | 0.8 |
| 7 | 21.5 | 9.8 | 10.5 | 4.4 | 6.8 | 2.7 | 3.2 | 0.9 |
| 8 | 24.3 | 11.0 | 11.9 | 5.0 | 7.7 | 3.0 | 3.6 | 1.0 |
| 9 | 27.2 | 12.2 | 13.3 | 5.6 | 8.7 | 3.3 | 4.0 | 1.1 |
| 10 | 30.1 | 13.4 | 14.7 | 6.1 | 9.6 | 3.7 | 4.5 | 1.2 |
| 11 | 32.9 | 14.7 | 16.1 | 6.7 | 10.5 | 4.0 | 4.9 | 1.3 |
| 12 | 35.8 | 15.9 | 17.5 | 7.2 | 11.4 | 4.3 | 5.3 | 1.4 |
| 13 | 38.7 | 17.1 | 18.9 | 7.8 | 12.3 | 4.7 | 5.7 | 1.6 |
| 14 | 41.5 | 18.3 | 20.3 | 8.3 | 13.2 | 5.0 | 6.2 | 1.7 |
| 15 | 44.4 | 19.6 | 21.7 | 8.9 | 14.2 | 5.3 | 6.6 | 1.8 |
| 16 | 47.3 | 20.8 | 23.1 | 9.4 | 15.1 | 5.7 | 7.0 | 1.9 |
| 17 | 50.2 | 22.0 | 24.5 | 10.0 | 16.0 | 6.0 | 7.4 | 2.0 |


| TABLE 46. ADDED HANDLING WEIGHT AND ADDITIONAL BOLTS PER FOOT OF STRUCTURE FOR TYPE IV REINFORCING RIB |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Total N of Rib | 9" o.c. |  | 18" o.c. |  | 27" o.c. |  | 54" o.c. |  |
|  | Wt/ft | Bolts/ft | Wt/ft | Bolts/ft | Wt/ft | Bolts/ft | Wt/ft | Bolts/ft |
| 5 | 20.0 | 7.3 | 9.8 | 3.3 | 6.4 | 2.0 | 3.0 | 0.7 |
| 6 | 23.7 | 8.6 | 11.6 | 3.9 | 7.6 | 2.3 | 3.6 | 0.8 |
| 7 | 27.4 | 9.8 | 13.4 | 4.4 | 8.8 | 2.7 | 4.2 | 0.9 |
| 8 | 31.0 | 11.0 | 15.2 | 5.0 | 10.0 | 3.0 | 4.7 | 1.0 |
| 9 | 34.7 | 12.2 | 17.1 | 5.6 | 11.2 | 3.3 | 5.3 | 1.1 |
| 10 | 38.4 | 13.4 | 18.9 | 6.1 | 12.4 | 3.7 | 5.9 | 1.2 |
| 11 | 42.1 | 14.7 | 20.7 | 6.7 | 13.5 | 4.0 | 6.4 | 1.3 |
| 12 | 45.8 | 15.9 | 22.5 | 7.2 | 14.7 | 4.3 | 7.0 | 1.4 |
| 13 | 49.4 | 17.1 | 24.3 | 7.8 | 15.9 | 4.7 | 7.5 | 1.6 |
| 14 | 53.1 | 18.3 | 26.1 | 8.3 | 17.1 | 5.0 | 8.1 | 1.7 |
| 15 | 56.8 | 19.6 | 27.9 | 8.9 | 18.3 | 5.3 | 8.7 | 1.8 |
| 16 | 60.5 | 20.8 | 29.7 | 9.4 | 19.5 | 5.7 | 9.2 | 1.9 |
| 17 | 64.1 | 22.0 | 31.5 | 10.0 | 20.7 | 6.0 | 9.8 | 2.0 |

TABLE 47. ADDED HANDLING WEIGHT AND ADDITIONAL BOLTS PER FOOT OF STRUCTURE FOR TYPE VI REINFORCING RIB

| Total N of Rib | 9" o.c. |  | 18" o.c. |  | 27" o.c. |  | 54" o.c. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Wt/ft | Bolts/ft | Wt/ft | Bolts/ft | Wt/ft | Bolts/ft | Wt/ft | Bolts/ft |
| 5 | 28.8 | 7.3 | 14.2 | 3.3 | 9.4 | 2.0 | 4.5 | 0.7 |
| 6 | 34.1 | 8.6 | 16.9 | 3.9 | 11.1 | 2.3 | 5.3 | 0.8 |
| 7 | 39.4 | 9.8 | 19.5 | 4.4 | 12.8 | 2.7 | 6.2 | 0.9 |
| 8 | 44.8 | 11.0 | 22.1 | 5.0 | 14.6 | 3.0 | 7.0 | 1.0 |
| 9 | 50.1 | 12.2 | 24.7 | 5.6 | 16.3 | 3.3 | 7.8 | 1.1 |
| 10 | 55.4 | 13.4 | 27.4 | 6.1 | 18.0 | 3.7 | 8.7 | 1.2 |
| 11 | 60.8 | 14.7 | 30.0 | 6.7 | 19.8 | 4.0 | 9.5 | 1.3 |
| 12 | 66.1 | 15.9 | 32.7 | 7.2 | 21.5 | 4.3 | 10.4 | 1.4 |
| 13 | 71.4 | 17.1 | 35.3 | 7.8 | 23.2 | 4.7 | 11.2 | 1.6 |
| 14 | 76.8 | 18.3 | 37.9 | 8.3 | 25.0 | 5.0 | 12.0 | 1.7 |
| 15 | 82.1 | 19.6 | 40.6 | 8.9 | 26.7 | 5.3 | 12.9 | 1.8 |
| 16 | 87.4 | 20.8 | 43.2 | 9.4 | 28.5 | 5.7 | 13.7 | 1.9 |
| 17 | 92.8 | 22.0 | 45.8 | 10.0 | 30.2 | 6.0 | 14.5 | 2.0 |

## Notes

1. Bolts and nuts are included in the column titled "Wt/Ft."
2. For Total $N$ of rib on a structure, see Tables $34,35,37,39,40$ and 42.

Rib Assembly Socket


Type II Rib


Type IV Rib


Type VI Rib


Mimimum curving values are 60" for Type II Ribs and 104" for Type IV and Type VI Ribs.

## Aluminum Structural Plate Specification

Scope: This specification covers the manufacture and installation of the Aluminum Structural Plate structure detailed in the plans.

Material: The Aluminum Structural Plate structure shall consist of plates and appurtenant items as shown on the plans and shall conform to the requirements of AASHTO 219 and ASTM B 746. The corrugated plate (and ribs if required) shall be curved and bolt hole punched at the plant. Plate thickness and rib spacings shall be as indicated on the plans. All manufacturing processes including corrugating, punching, and curving, shall be performed within the United States.

Bolts and nuts shall conform to the requirements of ASTM A307 or A449 for steel fasteners or ASTM F467 and F468 for aluminum fasteners.

Assembly: The structure shall be assembled in accordance with the shop drawings provided by the manufacturer
and per the manufacturer's recommendations. Bolts shall be tightened using an applied torque of between 90 and 135 ft .-lbs.

Installation: The structure shall be installed in accordance with the plans and specifications, the manufacturer's recommendations and the AASHTO Standard Specifications for Highway Bridges, Section 26 (Division II).

Backfill: The structure shall be backfilled using clean, well graded granular material that meets the requirements of AASHTO M 145 for soil classifications A-1, A-2 or A3. Backfill must be placed symmetrically on each side of the structure in 6 to 8 inch lifts. Each lift shall be compacted to a minimum of 90 percent density per AASHTO T 99.

Note: Construction loads that exceed highway load limits are not allowed on the structure without approval from the Project Engineer.


Assembly of Aluminum Structural Plate Single Radius Arch

## Installation

## Required elements

Satisfactory site preparation, trench excavation, bedding and backfill operations are essential to develop the strength of any flexible conduit. In order to obtain proper strength while preventing settlement, it is necessary that the soil envelope around the structure be of good granular material, properly placed, and carefully compacted.

Pipe-arch and underpass shapes pose special installation problems not found in other shapes. These two shapes generate high corner bearing pressures against the side fill and foundation (see Page 57 for the corner bearing pressure). Therefore, special installation care must be implemented to achieve a composite soil structure.

A qualified Engineer should be engaged to design a proper foundation, adequate bedding, and backfill.

## Trench excavation

If the adjacent embankment material is structurally adequate, the trench requires only a bottom clear width of the structure's span plus sufficient room for compaction equipment.

## Bedding

Proper bedding preparation is critical to both structure performance and service life. The bed should be constructed to avoid distortions that may create undesirable stresses in the structure and/or rapid deterioration of the roadway. The bed should be free of rock formations, protruding stones and frozen matter that may cause unequal settlement.

It is recommended that the bedding be stable, well graded granular material. Placing the structure on the bedding surface is generally accomplished by one of the two following methods:

- Shaping the bedding surface to conform to the lower section of the structure
- Carefully tamping a granular or select material beneath the haunches to achieve a well-compacted condition

Using one of these two methods ensures satisfactory compaction beneath the haunches.

## Assembly

Assembly drawings and detailed assembly instructions are shipped with each order. Structures can be preassembled and lifted into place all at once or in sections, allowing for staged construction. If the site conditions allow, structures can be assembled in place. A qualified engineer should be engaged to determine the most appropriate site conditions. For additional information contact your local Contech representative.

## Backfill

Satisfactory backfill material, proper placement and compaction are key factors in obtaining maximum strength and stability.

The backfill material should be free of rocks, frozen lumps and foreign material that could cause hard spots or decompose to created voids. Backfill material should be well graded granular material that meets the requirements of AASHTO M 145 for soil classifications A-1, A-2, or A-3. Backfill must be placed symmetrically on each side of the structure in six-inch loose lifts. Each lift is to be compacted to a minimum of 90 percent density per AASHTO T 99.
A high percentage of silt or fine sand in the native soils suggests the need for a well graded granular backfill material to prevent soil migration.

During backfill, only small tracked vehicles (D-4 or smaller) should be near the structure as fill progresses above the crown and to the finished grade. The engineer and contractor are cautioned that the minimum cover may need to be increased to handle temporary construction vehicle loads (larger than D-4).

## Salt water installation

In salt water installations, the bedding and backfill around the structure must be clean granular material. If the backfill is subject to possible infiltration by the adjacent native soil, the clean granular backfill should be wrapped in a geotextile.

## Pavement

For minimum cover applications, Contech recommends that a properly designed flexible or rigid pavement be provided above the structure to distribute live loads and maintain cover.

## Precautions

During installation and prior to the construction of permanent erosion control and end treatment protection, special precautions may be necessary.

The structure must be protected from unbalanced loads from any structural loads or hydraulic forces that might bend or distort the unsupported ends of the structure.

Erosion or washout of previously placed soil support must be prevented to ensure that the structure maintains its load capacity.


MULTI-PLATE Conveyor Covers



Single Radius Arch for Residential Development

## Aluminum Box Culverts

## The Solution for Small Bridge Replacement: Aluminum Box Culverts

Contech Aluminum Box Culverts are a practical and costefficient solution for small bridge replacement. They have a lower installed cost because they are faster and easier to install than cast-in-place concrete structures. There are no forms to set and remove, no delays due to curing time, large installation crews are unnecessary and no special equipment is needed. Also, no heavy cranes are required as with precast concrete structures.

These wide-span, low-rise structures are available in a large range of standard sizes (from 8'-9" span x 2'-6" rise to 35'$3^{\prime \prime}$ span $\times 13^{\prime}-7^{\prime \prime}$ rise) that permit a minimum cover of only 17 inches for all spans, handling HS-20 or HS-25 live loads.

## Faster Installation Means Lower Installed Cost

Closing roads for bridge replacement causes extensive traffic detours, so minimizing installation time is critical. Aluminum Box Culverts may be quickly erected in place and are usually ready to be backfilled in a matter of hours. For faster installation, Aluminum Box Culverts can be completely assembled nearby while the site is being prepared. Light equipment can then be used to set them in place.

## National Specification

Contech Aluminum Box Culvert design and installation is covered by AASHTO Standard Specifications for Highway Bridges (Sec 12.8). The material is covered by AASHTO M 219 and ASTM B 864.


Lifting of Aluminum Box Culvert


Corrugated Aluminum Headwall Package


## Notes (refer to pages 66-67)

1. Structure 1 is a one-plate shell. Structures 2-26 are two plate shells. Structures 27-143 are three-plate shells.
2. In Shell Fill Height Table 48 \& 49 , the HG\CG designation indicates thickness or gage of haunch (HG) and crown (CG) plates as follows: $2=.125^{\prime \prime}, 3=.150^{\prime \prime}, 4=.175^{\prime \prime}, 5=.200^{\prime \prime}, 6=.225^{\prime \prime}, 7=.250^{\prime \prime}$. Example: $3 \backslash 6=.150^{\prime \prime}$ haunch and $.225^{\prime \prime}$ crown plate thickness. The HRS/CRS designation indicates the rib spacing on the haunch (HRS) and crown (CRS) plates. Example: $27 / 9=27^{\prime \prime}$ o.c. haunch and $9^{\prime \prime}$ o.c. crown.
3. Allowable cover (minimum and maximum) is measured from the outside valley of crown plate to bottom of flexible pavement or from the outside valley of crown plate to top of rigid pavement. Minimum cover is measured at the lowest fill area subjected to possible wheel loads (typically at the roadway shoulder). The roadway surface must be maintained to ensure minimum cover to prevent high-impact loads being imparted to the structure. Maximum cover is measured at highest fill and/ or pavement elevation.
4. Select the structure with the lowest alphabetical sub-designation and cover range that will include the actual minimum and maximum cover. Example: Structure 51-A6 is more economical than 51-B6 if the cover is between 3.0 and 4.5 feet.
5. Shell Wt ./Ft. shown is maximum handling weight and is based on heaviest component makeup for a specific span and rise combination. Weight per foot of shell includes plates, reinforcing ribs, rib splices, bolts, and nuts.
6. Total structure length can be any dimension, but whenever possible, it is recommended to work with a multiple of 4.5' (net plate width). This practice usually results in lower total structure cost. Example: 50' proposed structure $\div 4.5^{\prime}=11.1$, nearest whole number is 11 , therefore use $11 \times 4.5^{\prime}=49.5^{\prime}$ for total structure length. When ordering a structure with headwalls on each end, total structure length must be a multiple of 9 inches.
7. Shell data in Table 48A is designed for standard highway HS-20 wheel Loads. See Table 48B for HS-25 loading design information. Call a Contech representative for design information on other loadings.
8. Standard structure designs use Type VI ribs for most economical plate and rib combination. Plate and rib combinations using Type II and Type IV ribs are available for special designs.
9. The maximum cover for Aluminum Box Culverts with full inverts and footing pads should not exceed 4 feet. Special full invert and footing pad designs or slotted concrete footings can accommodate maximum covers to the limits shown in Tables 48A and 48B.

Box Culvert Shell-Plate and Rib Data (H-20, HS-20)

| TABLE 48A SHELL DATA - H-20, HS-20 LOADING PLATE AND RIB COMBINATIONS WITH ALLOWABLE HEIGHT OF COVER |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Structure <br> Number | $\begin{aligned} & \text { Span "A" } \\ & \text { (Ft.-In.) } \end{aligned}$ | Rise "B" (Ft.-In.) | $\begin{gathered} \text { Area } \\ \text { (Sq. Ft.) } \end{gathered}$ | $\begin{aligned} & \text { HGICG } \\ & \text { (Gage) } \end{aligned}$ | HRS/CRS (Inches) |  | Max. | $\begin{aligned} & \text { HGICG } \\ & \text { (Gage) } \end{aligned}$ | HRS/CRS (Inches) |  | Max. | $\begin{aligned} & \text { HGICG } \\ & \text { (Gage) } \end{aligned}$ | HRS/CRS (Inches) |  | Max. | Max. Shell Wt./Ft. (Lbs.) |
| STRUCTURES 1 THROUGH 26 HAVE TYPE II HAUNCH AND TYPE IV CROWN RIBS |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | 8-9 | 2-6 | 18.4 | 212 | 54/18 | 1.4 | 5.0 |  |  |  |  |  |  |  |  | 43 |
| 2 | 9-2 | 3-3 | 25.4 | 212 | 54/18 | 1.4 | 5.0 |  |  |  |  |  |  |  |  | 50 |
| 3 | 9-7 | 4-1 | 32.6 | 212 | 54/18 | 1.4 | 5.0 |  |  |  |  |  |  |  |  | 54 |
| 4 | 10-0 | 4-10 | 40.2 | 212 | 54/18 | 1.4 | 5.0 |  |  |  |  |  |  |  |  | 58 |
| 5 | 10-6 | 5-7 | 48.1 | 212 | 54/18 | 1.7 | 5.0 | 313 | 54/18 | 1.4 | 5.0 |  |  |  |  | 71 |
| 6 | 10-11 | 6-4 | 56.4 | 212 | 54/18 | 2.0 | 5.0 | 212 | 27/18 | 1.4 | 5.0 |  |  |  |  | 74 |
| 7 | 11-4 | 7-2 | 65.0 | 212 | 54/18 | 2.5 | 5.0 | 212 | 54/9 | 1.4 | 5.0 |  |  |  |  | 79 |
| 8 | 10-2 | 2-8 | 23.0 | 212 | 54/18 | 1.7 | 5.0 | 313 | 54/18 | 1.4 | 5.0 |  |  |  |  | 60 |
| 9 | 10-7 | 3-5 | 31.1 | 212 | 54/18 | 2.0 | 5.0 | 313 | 54/18 | 1.4 | 5.0 |  |  |  |  | 65 |
| 10 | 10-11 | 4-3 | 39.5 | 212 | 54/18 | 2.0 | 5.0 | 313 | 54/18 | 1.4 | 5.0 |  |  |  |  | 70 |
| 11 | 11-4 | 5-0 | 48.2 | 212 | 54/18 | 2.5 | 5.0 | 313 | 54/18 | 1.7 | 5.0 | 212 | 54/9 | 1.4 | 5.0 | 79 |
| 12 | 11-8 | 5-9 | 57.2 | 212 | 54/18 | 2.5 | 5.0 | 313 | 54/18 | 1.7 | 5.0 | 212 | 54/9 | 1.4 | 5.0 | 83 |
| 13 | 12-1 | 6-7 | 66.4 | 212 | 54/18 | 3.0 | 5.0 | 212 | 27/18 | 2.0 | 5.0 | 212 | 54/9 | 1.4 | 5.0 | 86 |
| 14 | 12-5 | 7-4 | 76.0 | 212 | 54/18 | 3.0 | 5.0 | 212 | $27 / 18$ | 2.5 | 5.0 | 212 | $27 / 9$ | 1.4 | 5.0 | 98 |
| 15 | 11-7 | 2-10 | 28.1 | 212 | 54/18 | 2.5 | 5.0 | 313 | 54/18 | 1.7 | 5.0 | 313 | 27/18 | 1.4 | 5.0 | 75 |
| 16 | 11-11 | 3-7 | 37.4 | 212 | 54/18 | 2.5 | 5.0 | 313 | 54/18 | 2.0 | 5.0 | 414 | 54/18 | 1.4 | 5.0 | 81 |
| 17 | 12-3 | 4-5 | 46.9 | 212 | 54/18 | 3.0 | 5.0 | 313 | 54/18 | 2.0 | 5.0 | 313 | 27/18 | 1.4 | 5.0 | 87 |
| 18 | 12-7 | 5-2 | 56.6 | 212 | 54/18 | 3.0 | 5.0 | 212 | 27/18 | 2.5 | 5.0 | 212 | 27/9 | 1.4 | 5.0 | 98 |
| 19 | 12-11 | 6-0 | 66.6 | 212 | 54/18 | 3.0 | 5.0 | 212 | 27/18 | 2.5 | 5.0 | 212 | $27 / 9$ | 1.4 | 5.0 | 102 |
| 20 | 13-3 | 6-9 | 76.9 | 313 | 54/18 | 2.5 | 5.0 | 313 | 27/18 | 2.0 | 5.0 | 212 | 27/9 | 1.4 | 5.0 | 105 |
| 21 | 13-0 | 3-0 | 33.8 | 313 | 54/18 | 2.5 | 5.0 | 414 | 54/18 | 2.0 | 5.0 | 414 | 27/18 | 1.4 | 5.0 | 91 |
| 22 | 13-4 | 3-10 | 44.2 | 313 | 54/18 | 3.0 | 5.0 | 313 | 27/18 | 2.0 | 5.0 | 313 | 54/9 | 1.4 | 5.0 | 102 |
| 23 | 13-7 | 4-7 | 54.8 | 313 | 54/18 | 3.0 | 5.0 | 313 | 27/18 | 2.5 | 5.0 | 313 | 54/9 | 1.4 | 5.0 | 107 |
| 24 | 13-10 | 5-5 | 65.6 | 212 | 27/18 | 3.0 | 5.0 | 313 | 27/18 | 2.5 | 5.0 | 313 | 54/9 | 1.4 | 5.0 | 112 |
| 25 | 14-1 | 6-2 | 76.6 | 313 | 54/18 | 3.0 | 5.0 | 313 | 27/18 | 2.5 | 5.0 | 212 | 18/9 | 1.4 | 5.0 | 121 |
| 26 | 14-5 | 3-3 | 40.0 | 313 | 27/18 | 3.0 | 5.0 | 414 | 27/18 | 2.5 | 5.0 | 515 | 18/18 | 1.4 | 5.0 | 114 |
| STRUCTURES 27 THROUGH 39 HAVE TYPE II HAUNCH AND TYPE VI CROWN RIBS ${ }^{(10)}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 27 | 14-8 | 4-1 | 51.5 | 212 | 27/18 | 1.4 | 5.0 |  |  |  |  |  |  |  |  | 100 |
| 28 | 14-10 | 4-10 | 63.2 | 212 | 27/18 | 1.4 | 5.0 |  |  |  |  |  |  |  |  | 112 |
| 29 | 15-1 | 5-8 | 75.1 | 312 | 27/18 | 1.4 | 5.0 |  |  |  |  |  |  |  |  | 117 |
| 30 | 15-4 | 6-5 | 87.2 | 312 | 27/18 | 1.4 | 5.0 |  |  |  |  |  |  |  |  | 121 |
| 31 | 15-6 | 7-3 | 99.4 | 312 | 27/18 | 1.4 | 5.0 |  |  |  |  |  |  |  |  | 125 |
| 32 | 15-9 | 8-0 | 111.8 | 212 | 27/18 | 2.0 | 5.0 | 312 | 18/18 | 1.4 | 5.0 |  |  |  |  | 138 |
| 33 | 15-10 | 3-6 | 46.8 | 212 | 27/18 | 2.1 | 5.0 | 312 | 18/18 | 1.4 | 5.0 |  |  |  |  | 115 |
| 34 | 16-0 | 4-3 | 59.5 | 212 | 27/18 | 2.3 | 5.0 | 312 | 18/18 | 1.4 | 5.0 |  |  |  |  | 122 |
| 35 | 16-2 | 5-1 | 72.3 | 212 | 27/18 | 2.4 | 4.9 | 312 | 18/18 | 1.4 | 5.0 |  |  |  |  | 129 |
| 36 | 16-4 | 5-11 | 85.2 | 212 | 27/18 | 2.6 | 4.5 | 312 | 18/18 | 1.4 | 5.0 |  |  |  |  | 133 |
| 37 | 16-6 | 6-8 | 98.3 | 312 | $27 / 18$ | 1.8 | 5.0 | 412 | 18/18 | 1.4 | 5.0 |  |  |  |  | 146 |
| 38 | 16-8 | 7-6 | 111.5 | 312 | 27/18 | 1.9 | 5.0 | 412 | 18/18 | 1.4 | 5.0 |  |  |  |  | 151 |
| 39 | 16-10 | 8-3 | 124.8 | 312 | 27/18 | 2.0 | 5.0 | 412 | 18/18 | 1.4 | 5.0 |  |  |  |  | 165 |
| STRUCTURES 40 THROUGH 87 USE ALL TYPE VIRIBS ${ }^{(0)}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 40 | 17-9 | 3-10 | 54.4 | 212 | 54/18 | 2.0 | 5.0 | 212 | 27/18 | 1.4 | 5.0 |  |  |  |  | 124 |
| 41 | 18-2 | 4-7 | 68.3 | 212 | 54/18 | 2.2 | 5.0 | 212 | 27/18 | 1.4 | 5.0 |  |  |  |  | 131 |
| 42 | 18-7 | 5-4 | 82.5 | 212 | 54/18 | 2.4 | 5.0 | 212 | 27/18 | 1.4 | 5.0 |  |  |  |  | 138 |
| 43 | 19-0 | 6-1 | 97.1 | 212 | 54/18 | 2.6 | 5.0 | 212 | 27/18 | 1.4 | 5.0 |  |  |  |  | 142 |
| 44 | 19-5 | 6-11 | 111.9 | 212 | 54/18 | 2.8 | 5.0 | 212 | 18/18 | 1.4 | 5.0 |  |  |  |  | 154 |
| 45 | 19-10 | 7-8 | 127.1 | 212 | 54/18 | 2.9 | 5.0 | 212 | 18/18 | 1.4 | 5.0 |  |  |  |  | 164 |
| 46 | 20-3 | 8-5 | 142.6 | 212 | 27/18 | 1.9 | 5.0 | 212 | 18/18 | 1.4 | 5.0 |  |  |  |  | 167 |
| 47 | 19-1 | 4-2 | 63.3 | 212 | 54/18 | 2.6 | 5.0 | 212 | 18/18 | 1.4 | 5.0 |  |  |  |  | 133 |
| 48 | 19-5 | 4-11 | 78.3 | 212 | 54/18 | 2.8 | 5.0 | 212 | 18/18 | 1.4 | 5.0 |  |  |  |  | 153 |
| 49 | 19-9 | 5-8 | 93.6 | 212 | 54/18 | 2.9 | 4.8 | 212 | 18/18 | 1.4 | 5.0 |  |  |  |  | 162 |
| 50 | 20-1 | 6-6 | 109.2 | 212 | 27/18 | 1.9 | 5.0 | 212 | 18/18 | 1.4 | 5.0 |  |  |  |  | 165 |
| 51 | 20-6 | 7-3 | 125 | 212 | 27/18 | 2.0 | 5.0 | 212 | 18/18 | 1.4 | 5.0 |  |  |  |  | 169 |
| 52 | 20-10 | 8-1 | 141.2 | 212 | 27/18 | 2.1 | 5.0 | 212 | 18/18 | 1.4 | 5.0 |  |  |  |  | 173 |
| 53 | 21-2 | 8-10 | 157.6 | 212 | 27/18 | 2.2 | 5.0 | 212 | 18/18 | 1.4 | 5.0 |  |  |  |  | 176 |
| 54 | 20-4 | 4-6 | 73.1 | 212 | 27/18 | 2.0 | 5.0 | 212 | 18/18 | 1.4 | 5.0 |  |  |  |  | 153 |
| 55 | 20-7 | 5-3 | 89.2 | 212 | 27/18 | 2.1 | 5.0 | 212 | 18/18 | 1.4 | 5.0 |  |  |  |  | 162 |
| 56 | 20-11 | 6-1 | 105.5 | 212 | 27/18 | 2.2 | 5.0 | 212 | 18/18 | 1.4 | 5.0 |  |  |  |  | 171 |
| 57 | 21-3 | 6-10 | 122.1 | 212 | 27/18 | 2.3 | 5.0 | 212 | 18/18 | 1.4 | 5.0 |  |  |  |  | 174 |
| 58 | 21-6 | 7-8 | 139.0 | 212 | 27/18 | 2.3 | 5.0 | 212 | 18/18 | 1.4 | 5.0 |  |  |  |  | 178 |
| 59 | 21-10 | 8-5 | 156.0 | 212 | 27/18 | 2.5 | 5.0 | 212 | 18/18 | 1.4 | 5.0 |  |  |  |  | 182 |
| 60 | 22-1 | 9-3 | 173.3 | 212 | 27/18 | 2.5 | 4.8 | 213 | 18/18 | 1.4 | 5.0 |  |  |  |  | 190 |
| 61 | 21-7 | 4-11 | 83.8 | 212 | 27/18 | 2.4 | 5.0 | 212 | 18/18 | 1.4 | 5.0 |  |  |  |  | 162 |
| 62 | 21-10 | 5-8 | 101 | 212 | 27/18 | 2.5 | 5.0 | 212 | 18/18 | 1.4 | 5.0 |  |  |  |  | 171 |
| 63 | 22-1 | 6-6 | 118.4 | 212 | 27/18 | 2.5 | 4.8 | 213 | 18/18 | 1.4 | 5.0 |  |  |  |  | 185 |
| 64 | 22-3 | 7-3 | 135.9 | 212 | 27/18 | 2.6 | 4.6 | 213 | 18/18 | 1.4 | 5.0 |  |  |  |  | 188 |
| 65 | 22-6 | 8-1 | 153.7 | 212 | 27/18 | 2.7 | 4.4 | 213 | 18/18 | 1.4 | 5.0 |  |  |  |  | 192 |
| 66 | 22-9 | 8-10 | 171.6 | 212 | 27/18 | 2.8 | 4.2 | 214 | 18/18 | 1.4 | 5.0 |  |  |  |  | 191 |
| 67 | 23-0 | 9-8 | 189.8 | 212 | 27/18 | 2.8 | 4.0 | 214 | 18/18 | 1.4 | 5.0 |  |  |  |  | 204 |
| 68 | 22-9 | 5-4 | 95.5 | 212 | 27/18 | 2.8 | 4.2 | 214 | 18/18 | 1.4 | 5.0 |  |  |  |  | 181 |
| 69 | 23-0 | 6-1 | 113.7 | 212 | 27/18 | 2.8 | 4.0 | 214 | 18/18 | 1.4 | 5.0 |  |  |  |  | 190 |
| 70 | 23-2 | 6-11 | 132.1 | 313 | 27/18 | 2.6 | 4.4 | 215 | 18/18 | 1.4 | 5.0 |  |  |  |  | 203 |
| 71 | 23-4 | 7-8 | 150.6 | 313 | 27/18 | 2.6 | 4.3 | 215 | 18/18 | 1.4 | 5.0 |  |  |  |  | 207 |
| 72 | 23-6 | 8-6 | 169.3 | 313 | 27/18 | 2.7 | 4.2 | 215 | 18/18 | 1.4 | 5.0 |  |  |  |  | 211 |
| 73 | 23-8 | 9-3 | 188.1 | 313 | 27/18 | 2.7 | 4.0 | 215 | 18/18 | 1.4 | 5.0 |  |  |  |  | 214 |
| 74 | 23-10 | 10-1 | 207.0 | 313 | 27/18 | 2.8 | 3.9 | 215 | 18/18 | 1.4 | 5.0 |  |  |  |  | 213 |
| 75 | 24-0 | 5-9 | 108.2 | 212 | 18/18 | 1.7 | 5.0 | 215 | 18/18 | 1.4 | 5.0 |  |  |  |  | 196 |
| 76 | 24-1 | 6-6 | 127.5 | 212 | 18/18 | 1.7 | 5.0 | 216 | 18/18 | 1.4 | 5.0 |  |  |  |  | 211 |
| 77 | 24-3 | 7-4 | 146.8 | 212 | 18/18 | 1.8 | 5.0 | 216 | 18/18 | 1.4 | 5.0 |  |  |  |  | 220 |
| 78 | 24-4 | 8-2 | 166.2 | 212 | 18/18 | 1.8 | 5.0 | 216 | 18/18 | 1.4 | 5.0 |  |  |  |  | 224 |
| 79 | 24-5 | 8-11 | 185.7 | 212 | 18/18 | 1.8 | 5.0 | 216 | 18/18 | 1.4 | 5.0 |  |  |  |  | 227 |
| 80 | 24-7 | 9-9 | 205.3 | 212 | 18/18 | 1.8 | 5.0 | 216 | 18/18 | 1.4 | 5.0 |  |  |  |  | 231 |
| 81 | 24-8 | 10-6 | 225 | 212 | 18/18 | 1.8 | 5.0 | 216 | 18/18 | 1.4 | 5.0 |  |  |  |  | 234 |
| 82 | 25-2 | 6-2 | 122.0 | 212 | 18/18 | 1.9 | 4.9 | 216 | 18/18 | 1.4 | 5.0 |  |  |  |  | 214 |
| 83 | 25-2 | 7-0 | 142.2 | 212 | 18/18 | 1.9 | 4.9 | 217 | 18/18 | 1.4 | 5.0 |  |  |  |  | 226 |
| 84 | 25-3 | 7-9 | 162.4 | 212 | 18/18 | 1.9 | 4.9 | 217 | 18/18 | 1.4 | 5.0 |  |  |  |  | 235 |
| 85 | 25-4 | 8-7 | 182.6 | 212 | 18/18 | 1.9 | 4.8 | 217 | 18/18 | 1.4 | 5.0 |  |  |  |  | 238 |
| 86 | 25-4 | 9-5 | 202.9 | 212 | 18/18 | 1.9 | 4.8 | 217 | 18/18 | 1.4 | 5.0 |  |  |  |  | 242 |
| 87 | 25-5 | 10-2 | 223.3 | 212 | 18/18 | 2.0 | 4.5 | 217 | 18/18 | 1.4 | 5.0 |  |  |  |  | 245 |

See Notes page 65

Box Culvert Shell-Plafe and Rib Dafa (H-25, HS-25)

| TABLE 48B. SHELL DATA - H-25, HS-25 LOADING PLATE AND RIB COMBINATIONS WITH ALLOWABLE HEIGHT OF COVER |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Structure Number | Span "A" <br> (Ft.-In.) | Rise "B" <br> (Ft.-In.) | Area (Sq. Ft.) | $\begin{gathered} \text { HGICG } \\ \text { (Gage) } \end{gathered}$ | HRS/CRS (Inches) |  |  | HGICG (Gage) | HRS/CRS (Inches) |  | Max. | $\begin{gathered} \text { HGICG } \\ \text { (Gage) } \end{gathered}$ | HRS/CRS (Inches) | Min. | ${ }_{(\text {Feet })^{(9)}}^{\text {Max. }}$ | Max. Shell Wt./Ft. <br> (Lbs.) |
| STRUCTURES 1 THROUGH 20 HAVE TYPE II HAUNCH AND TYPE IV CROWN RIBS |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | 8-9 | 2-6 | 18.4 | 212 | 54/18 | 1.7 | 5.0 | 313 | 54/18 | 1.4 | 5.0 |  |  |  |  | 49 |
| 2 | 9-2 | 3-3 | 25.4 | 212 | 54/18 | 2.0 | 5.0 | 313 | 54/18 | 1.4 | 5.0 |  |  |  |  | 57 |
| 3 | 9-7 | 4-1 | 32.6 | 212 | 54/18 | 2.0 | 5.0 | 313 | 54/18 | 1.4 | 5.0 |  |  |  |  | 62 |
| 4 | 10-0 | 4-10 | 40.2 | 212 | 54/18 | 2.5 | 5.0 | 212 | 54/9 | 1.4 | 5.0 |  |  |  |  | 67 |
| 5 | 10-6 | 5-7 | 48.1 | 212 | 54/18 | 2.5 | 5.0 | 212 | 54/9 | 1.4 | 5.0 |  |  |  |  | 71 |
| 6 | 10-11 | 6-4 | 56.4 | 212 | 54/18 | 3.0 | 5.0 | 212 | 54/9 | 2.0 | 5.0 | 313 | 54/9 | 1.4 | 5.0 | 85 |
| 7 | 11-4 | 7-2 | 65.0 | 212 | 54/18 | 3.0 | 5.0 | 212 | 27/18 | 2.5 | 5.0 | 313 | 54/9 | 1.4 | 5.0 | 90 |
| 8 | 10-2 | 2-8 | 23.0 | 212 | 54/18 | 2.5 | 5.0 | 313 | 54/18 | 1.7 | 5.0 | 414 | 54/18 | 1.4 | 5.0 | 66 |
| 9 | 10-7 | 3-5 | 31.1 | 212 | 54/18 | 3.0 | 5.0 | 313 | 54/18 | 2.0 | 5.0 | 313 | 27/18 | 1.4 | 5.0 | 73 |
| 10 | 10-11 | 4-3 | 39.5 | 212 | 54/18 | 3.0 | 5.0 | 313 | 54/18 | 2.5 | 5.0 | 313 | 54/9 | 1.4 | 5.0 | 84 |
| 11 | 11-4 | 5-0 | 48.2 | 212 | 54/18 | 3.0 | 5.0 | 313 | 54/18 | 2.5 | 5.0 | 313 | 54/9 | 1.4 | 5.0 | 88 |
| 12 | 11-8 | 5-9 | 57.2 | 212 | 54/18 | 3.0 | 5.0 | 313 | 54/18 | 2.5 | 5.0 | 313 | 54/9 | 1.4 | 5.0 | 93 |
| 13 | 12-1 | 6-7 | 66.4 | 313 | 54/18 | 3.0 | 5.0 | 313 | 27/18 | 2.5 | 5.0 | 313 | $27 / 9$ | 1.4 | 5.0 | 105 |
| 14 | 12-5 | 7-4 | 76.0 | 212 | $27 / 18$ | 3.0 | 5.0 | 212 | $27 / 9$ | 2.0 | 5.0 | 313 | $27 / 9$ | 1.4 | 5.0 | 110 |
| 15 | 11-7 | 2-10 | 28.1 | 212 | 54/18 | 3.0 | 5.0 | 313 | 54/18 | 2.5 | 5.0 | 313 | 54/9 | 1.4 | 5.0 | 85 |
| 16 | 11-11 | 3-7 | 37.4 | 313 | 54/18 | 3.0 | 5.0 | 313 | 27/18 | 2.5 | 5.0 | 313 | 54/9 | 1.4 | 5.0 | 90 |
| 17 | 12-3 | 4-5 | 46.9 | 313 | 54/18 | 3.0 | 5.0 | 414 | 54/18 | 2.5 | 5.0 | 414 | 54/9 | 1.4 | 5.0 | 104 |
| 18 | 12-7 | 5-2 | 56.6 | 313 | 54/18 | 3.0 | 5.0 | 313 | 27/18 | 2.5 | 5.0 | 414 | 54/9 | 1.4 | 5.0 | 109 |
| 19 | 12-11 | 6-0 | 66.6 | 313 | 27/18 | 3.0 | 5.0 | 212 | $27 / 9$ | 2.0 | 5.0 | 414 | $27 / 9$ | 1.4 | 5.0 | 123 |
| 20 | 13-3 | 6-9 | 76.9 | 212 | 18/18 | 3.0 | 5.0 | 212 | 27/9 | 2.5 | 5.0 | 313 | 18/9 | 1.4 | 5.0 | 125 |
| STRUCTURES 21 THROUGH 39 HAVE TYPE II HAUNCH AND TYPE VI CROWN RIBS ${ }^{(10)}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 | 13-0 | 3-0 | 33.8 | 313 | 54/18 | 2.3 | 5.0 | 212 | $27 / 18$ | 1.6 | 5.0 | 313 | 27/18 | 1.4 | 5.0 | 100 |
| 22 | 13-4 | 3-10 | 44.2 | 313 | 54/18 | 2.5 | 5.0 | 212 | 27/18 | 1.7 | 5.0 | 414 | 27/18 | 1.4 | 5.0 | 114 |
| 23 | 13-7 | 4-7 | 54.8 | 313 | 54/18 | 2.7 | 5.0 | 212 | 27/18 | 1.9 | 5.0 | 313 | 18/18 | 1.4 | 5.0 | 118 |
| 24 | 13-10 | 5-5 | 65.6 | 313 | 54/18 | 2.9 | 5.0 | 212 | 27/18 | 2.0 | 5.0 | 313 | 18/18 | 1.4 | 5.0 | 122 |
| 25 | 14-1 | 6-2 | 76.6 | 212 | $27 / 18$ | 2.3 | 5.0 | 212 | 18/18 | 1.7 | 5.0 | 313 | 18/18 | 1.4 | 5.0 | 126 |
| 26 | 14-5 | 3-3 | 40.0 | 212 | 27/18 | 2.5 | 5.0 | 212 | 18/18 | 1.8 | 5.0 | 414 | 18/18 | 1.4 | 5.0 | 121 |
| 27 | 14-8 | 4-1 | 51.5 | 212 | 27/18 | 2.8 | 5.0 | 212 | 18/18 | 2.0 | 5.0 | 415 | 18/18 | 1.4 | 5.0 | 140 |
| 28 | 14-10 | 4-10 | 63.2 | 212 | 27/18 | 2.8 | 5.0 | 212 | 18/18 | 2.0 | 5.0 | 416 | 18/18 | 1.4 | 5.0 | 137 |
| 29 | 15-1 | 5-8 | 75.1 | 212 | 27/18 | 3.0 | 5.0 | 212 | 18/18 | 2.1 | 5.0 | 417 | 18/18 | 1.4 | 5.0 | 145 |
| 30 | 15-4 | 6-5 | 87.2 | 313 | 27/18 | 2.6 | 5.0 | 212 | 18/18 | 2.3 | 5.0 | 517 | 18/18 | 1.4 | 5.0 | 157 |
| 31 | 15-6 | 7-3 | 99.4 | 313 | 27/18 | 2.6 | 5.0 | 212 | 18/18 | 2.3 | 5.0 | 517 | 18/18 | 1.4 | 5.0 | 163 |
| 32 | 15-9 | 8-0 | 111.8 | 313 | 27/18 | 2.6 | 5.0 | 212 | 18/18 | 2.5 | 5.0 | 517 | 18/18 | 1.4 | 5.0 | 169 |
| 33 | 15-10 | 3-6 | 46.8 | 212 | 18/18 | 2.4 | 5.0 | 612 | 18/18 | 1.7 | 5.0 | 715 | 18/18 | 1.4 | 5.0 | 149 |
| 34 | 16-0 | 4-3 | 59.5 | 212 | 18/18 | 2.5 | 5.0 | 612 | 18/18 | 1.8 | 5.0 | 716 | 18/18 | 1.4 | 5.0 | 159 |
| 35 | 16-2 | 5-1 | 72.3 | 212 | 18/18 | 2.5 | 5.0 | 612 | 18/18 | 1.8 | 5.0 | 717 | 18/18 | 1.4 | 5.0 | 170 |
| 36 | 16-4 | 5-11 | 85.2 | 212 | 18/18 | 2.6 | 5.0 | 612 | 18/18 | 1.9 | 5.0 | 717 | 18/18 | 1.4 | 5.0 | 176 |
| 37 | 16-6 | 6-8 | 98.3 | 212 | 18/18 | 2.6 | 5.0 | 612 | 18/18 | 2.0 | 5.0 | 415 | 9/18 | 1.4 | 5.0 | 178 |
| 38 | 16-8 | 7-6 | 111.5 | 212 | 18/18 | 2.7 | 5.0 | 612 | 18/18 | 2.0 | 5.0 | 417 | 9/18 | 1.4 | 5.0 | 197 |
| 39 | 16-10 | 8-3 | 124.8 | 212 | 18/18 | 2.8 | 5.0 | 612 | 18/18 | 2.1 | 5.0 | 417 | 9/18 | 1.4 | 5.0 | 202 |
| STRUCTURES 40 THROUGH 87 USE ALL TYPE VI RIBS ${ }^{(10)}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 40 | 17-9 | 3-10 | 54.4 | 212 | 54/18 | 2.8 | 5.0 | 212 | 27/18 | 2.0 | 5.0 | 212 | 18/18 | 1.4 | 5.0 | 135 |
| 41 | 18-2 | 4-7 | 68.3 | 212 | 27/18 | 2.2 | 5.0 | 212 | 18/18 | 1.5 | 5.0 | 213 | 18/18 | 1.4 | 5.0 | 147 |
| 42 | 18-7 | 5-4 | 82.5 | 212 | 27/18 | 2.3 | 5.0 | 212 | 18/18 | 1.6 | 5.0 | 215 | 18/18 | 1.4 | 5.0 | 163 |
| 43 | 19-0 | 6-1 | 97.1 | 212 | $27 / 18$ | 2.4 | 5.0 | 212 | 18/18 | 1.8 | 5.0 | 216 | 18/18 | 1.4 | 5.0 | 174 |
| 44 | 19-5 | 6-11 | 111.9 | 212 | 27/18 | 2.6 | 5.0 | 212 | 18/18 | 1.8 | 5.0 | 217 | 18/18 | 1.4 | 5.0 | 186 |
| 45 | 19-10 | 7-8 | 127.1 | 212 | $27 / 18$ | 2.7 | 5.0 | 212 | 18/18 | 1.9 | 5.0 | 217 | 18/18 | 1.4 | 5.0 | 181 |
| 46 | 20-3 | 8-5 | 142.6 | 212 | 27/18 | 2.9 | 5.0 | 212 | 18/18 | 2.0 | 5.0 | 212 | 18/9 | 1.4 | 5.0 | 214 |
| 47 | 19-1 | 4-2 | 63.3 | 212 | 27/18 | 2.6 | 5.0 | 212 | 18/18 | 1.8 | 5.0 | 212 | 18/9 | 1.4 | 5.0 | 194 |
| 48 | 19-5 | 4-11 | 78.3 | 212 | 27/18 | 2.6 | 5.0 | 212 | 18/18 | 1.8 | 5.0 | 212 | 18/9 | 1.4 | 5.0 | 203 |
| 49 | 19-9 | 5-8 | 93.6 | 212 | 27/18 | 2.7 | 5.0 | 212 | 18/18 | 1.9 | 5.0 | 212 | 18/9 | 1.4 | 5.0 | 211 |
| 50 | 20-1 | 6-6 | 109.2 | 212 | $27 / 18$ | 2.9 | 5.0 | 212 | 18/18 | 1.9 | 5.0 | 212 | 18/9 | 1.4 | 5.0 | 218 |
| 51 | 20-6 | 7-3 | 125 | 212 | $27 / 18$ | 3.0 | 5.0 | 212 | 18/18 | 2.0 | 5.0 | 212 | 18/9 | 1.4 | 5.0 | 222 |
| 52 | 20-10 | 8-1 | 141.2 | 212 | $27 / 18$ | 3.2 | 4.5 | 212 | 18/18 | 2.0 | 5.0 | 212 | 18/9 | 1.4 | 5.0 | 225 |
| 53 | 21-2 | 8-10 | 157.6 | 212 | 18/18 | 2.1 | 5.0 | 217 | 18/18 | 1.7 | 5.0 | 212 | 18/9 | 1.4 | 5.0 | 229 |
| 54 | 20-4 | 4-6 | 73.1 | 212 | 27/18 | 3.0 | 5.0 | 212 | 18/18 | 2.0 | 5.0 | 212 | 18/9 | 1.4 | 5.0 | 211 |
| 55 | 20-7 | 5-3 | 89.2 | 212 | 27/18 | 3.1 | 4.9 | 212 | 18/18 | 2.0 | 5.0 | 212 | 18/9 | 1.4 | 5.0 | 220 |
| 56 | 20-11 | 6-1 | 105.5 | 212 | 27/18 | 3.2 | 4.3 | 212 | 18/18 | 2.0 | 5.0 | 212 | 18/9 | 1.4 | 5.0 | 229 |
| 57 | 21-3 | 6-10 | 122.1 | 212 | 18/18 | 2.1 | 5.0 | 217 | 18/18 | 1.7 | 5.0 | 212 | 18/9 | 1.4 | 5.0 | 233 |
| 58 | 21-6 | 7-8 | 139.0 | 212 | 18/18 | 2.2 | 5.0 | 217 | 18/18 | 1.8 | 5.0 | 212 | 18/9 | 1.4 | 5.0 | 236 |
| 59 | 21-10 | 8-5 | 156.0 | 212 | 18/18 | 2.2 | 5.0 | 217 | 18/18 | 1.9 | 5.0 | 212 | 18/9 | 1.4 | 5.0 | 240 |
| 60 | 22-1 | 9-3 | 173.3 | 212 | 18/18 | 2.3 | 5.0 | 217 | 18/18 | 2.0 | 5.0 | 212 | 18/9 | 1.4 | 5.0 | 243 |
| 61 | 21-7 | 4-11 | 83.8 | 212 | 18/18 | 2.2 | 5.0 | 217 | 18/18 | 1.8 | 5.0 | 212 | 18/9 | 1.4 | 5.0 | 225 |
| 62 | 21-10 | 5-8 | 101 | 212 | 18/18 | 2.2 | 5.0 | 217 | 18/18 | 1.9 | 5.0 | 212 | 18/9 | 1.4 | 5.0 | 234 |
| 63 | 22-1 | 6-6 | 118.4 | 212 | 18/18 | 2.3 | 5.0 | 217 | 18/18 | 2.0 | 5.0 | 212 | 18/9 | 1.4 | 5.0 | 243 |
| 64 | 22-3 | 7-3 | 135.9 | 212 | 18/18 | 2.4 | 5.0 | 217 | 18/18 | 2.0 | 5.0 | 212 | 18/9 | 1.4 | 5.0 | 247 |
| 65 | 22-6 | 8-1 | 153.7 | 212 | 18/18 | 2.5 | 5.0 | 217 | 18/18 | 2.0 | 5.0 | 212 | 18/9 | 1.4 | 5.0 | 251 |
| 66 | 22-9 | 8-10 | 171.6 | 212 | 18/18 | 2.6 | 5.0 | 217 | 18/18 | 2.0 | 5.0 | 212 | 18/9 | 1.4 | 5.0 | 254 |
| 67 | 23-0 | 9-8 | 189.8 | 212 | 18/18 | 2.6 | 5.0 | 217 | 18/18 | 2.2 | 5.0 | 212 | 18/9 | 1.4 | 5.0 | 258 |
| 68 | 22-9 | 5-4 | 95.5 | 212 | 18/18 | 2.4 | 5.0 | 217 | 18/18 | 2.1 | 5.0 | 212 | 18/9 | 1.4 | 5.0 | 240 |
| 69 | 23-0 | 6-1 | 113.7 | 212 | 18/18 | 2.5 | 5.0 | 217 | 18/18 | 2.1 | 5.0 | 212 | 18/9 | 1.4 | 5.0 | 249 |
| 70 | 23-2 | 6-11 | 132.1 | 212 | 18/18 | 2.5 | 5.0 | 217 | 18/18 | 2.2 | 5.0 | 212 | 18/9 | 1.4 | 5.0 | 258 |
| 71 | 23-4 | 7-8 | 150.6 | 212 | 18/18 | 2.6 | 5.0 | 217 | 18/18 | 2.2 | 5.0 | 212 | 18/9 | 1.4 | 5.0 | 262 |
| 72 | 23-6 | 8-6 | 169.3 | 212 | 18/18 | 2.6 | 5.0 | 217 | 18/18 | 2.2 | 5.0 | 212 | 18/9 | 1.4 | 5.0 | 265 |
| 73 | 23-8 | 9-3 | 188.1 | 212 | 18/18 | 2.7 | 4.9 | 217 | 18/18 | 2.3 | 5.0 | 212 | 18/9 | 1.4 | 5.0 | 269 |
| 74 | 23-10 | 10-1 | 207.0 | 212 | 18/18 | 2.7 | 4.8 | 217 | 18/18 | 2.3 | 5.0 | 212 | 18/9 | 1.4 | 5.0 | 272 |
| 75 | 24-0 | 5-9 | 108.2 | 212 | 18/18 | 2.7 | 4.6 | 217 | 18/18 | 2.4 | 5.0 | 212 | 18/9 | 1.4 | 5.0 | 254 |
| 76 | 24-1 | 6-6 | 127.5 | 212 | 18/18 | 2.7 | 4.6 | 217 | 18/18 | 2.4 | 5.0 | 212 | 18/9 | 1.4 | 5.0 | 263 |
| 77 | 24-3 | 7-4 | 146.8 | 212 | 18/18 | 2.8 | 4.4 | 217 | 18/18 | 2.4 | 5.0 | 212 | 18/9 | 1.4 | 5.0 | 272 |
| 78 | 24-4 | 8-2 | 166.2 | 212 | 18/18 | 2.8 | 4.3 | 217 | 18/18 | 2.4 | 5.0 | 212 | 18/9 | 1.4 | 5.0 | 276 |
| 79 | 24-5 | 8-11 | 185.7 | 212 | 18/18 | 2.9 | 4.2 | 217 | 18/18 | 2.4 | 5.0 | 212 | 18/9 | 1.4 | 5.0 | 280 |
| 80 | 24-7 | 9-9 | 205.3 | 212 | 18/18 | 2.9 | 4.1 | 217 | 18/18 | 2.4 | 5.0 | 212 | 18/9 | 1.4 | 5.0 | 283 |
| 81 | 24-8 | 10-6 | 225 | 212 | 18/18 | 3.0 | 4.0 | 217 | 18/18 | 2.5 | 5.0 | 212 | 18/9 | 1.4 | 5.0 | 287 |
| 82 | 25-2 | 6-2 | 122.0 | 315 | 18/18 | 2.7 | 4.3 | 212 | 18/9 | 1.4 | 5.0 |  |  |  |  | 272 |
| 83 | 25-2 | 7-0 | 142.2 | 315 | 18/18 | 2.7 | 4.3 | 212 | 18/9 | 1.4 | 5.0 |  |  |  |  | 278 |
| 84 | 25-3 | 7-9 | 162.4 | 315 | 18/18 | 2.7 | 4.3 | 212 | 18/9 | 1.4 | 5.0 |  |  |  |  | 287 |
| 85 | 25-4 | 8-7 | 182.6 | 315 | 18/18 | 2.7 | 4.2 | 212 | 18/9 | 1.4 | 5.0 |  |  |  |  | 291 |
| 86 | 25-4 | 9-5 | 202.9 | 315 | 18/18 | 2.7 | 4.2 | 212 | 18/9 | 1.4 | 5.0 |  |  |  |  | 294 |
| 87 | 25-5 | 10-2 | 223.3 | 315 | 18/18 | 2.8 | 4.2 | 212 | 18/9 | 1.4 | 5.0 |  |  |  |  | 298 |

Box Culvert Shell-Plate and Rib Dafa (HL-93)

| TABLE 49A. ALBC SHELL DATA-LRFD HL-93 PLATE AND RIB COMBINATIONS WITH ALLOWABLE HEIGHT OF COVER |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | L1 |  |  |  |  |  |  |  |
| Number | $\begin{aligned} & \text { Span } \\ & \text { (Ft.-In.) } \end{aligned}$ | $\begin{gathered} \text { Rise } \\ \text { (Ft.-In.) } \end{gathered}$ | (Sq. Ft.) | $\begin{aligned} & \hline \text { HG\CG } \\ & \text { (Gage) } \end{aligned}$ | HRS/CRS <br> (Inches) | $\begin{aligned} & \text { Min } \\ & \text { (Feet) } \end{aligned}$ | $\begin{gathered} \hline \text { Max }{ }^{(3)} \\ \text { (Feet) } \end{gathered}$ | Shell Wt/Ft <br> (Lbs.) | $\begin{aligned} & \hline \text { HG\CG } \\ & \text { (Gage) } \\ & \hline \end{aligned}$ | HR/CRS (Inches) | Min. (Feet) | $\begin{gathered} \text { Max. }{ }^{(3)} \\ \text { (Feet) } \end{gathered}$ | Shell Wt/Ft (Lbs.) |
| STRUCTURES 1 THROUGH 20 HAVE TYPE II HAUNCH AND TYPE IV CROWN RIBS |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | 8-9 | 2-6 | 18.4 | 2\2 | 54/18 | 1.4 | 5.0 | 43 |  |  |  |  | 43 |
| 2 | 9-2 | 3-3 | 25.4 | 2\2 | 54/18 | 1.4 | 5.0 | 50 |  |  |  |  | 50 |
| 3 | 9-7 | 4-1 | 32.6 | 2\2 | 54/18 | 2.0 | 5.0 | 58 | $2 \backslash 2$ | 27/18 | 1.4 | 5.0 | 67 |
| 4 | 10-0 | 4-10 | 40.2 | 2\2 | 54/18 | 2.5 | 5.0 | 61 | $2 \backslash 2$ | 27/18 | 1.4 | 5.0 | 70 |
| 5 | 10-6 | 5-7 | 48.1 | 2\2 | 27/18 | 2.0 | 5.0 | 74 | $2 \backslash 2$ | 18/18 | 1.4 | 5.0 | 83 |
| 6 | 10-11 | 6-4 | 56.4 | 2\2 | 27/18 | 2.5 | 5.0 | 77 | $2 \backslash 2$ | 27/9 | 1.4 | 5.0 | 88 |
| 7 | 11-4 | 7-2 | 65.0 | 2\2 | 27/18 | 2.5 | 5.0 | 81 | 2\2 | 27/9 | 1.4 | 5.0 | 91 |
| 8 | 10-2 | 2-8 | 23.0 | 2\2 | 27/18 | 2.0 | 5.0 | 63 | $2 \backslash 2$ | 27/18 | 1.4 | 5.0 | 63 |
| 9 | 10-7 | 3-5 | 31.1 | 2\2 | 27/18 | 2.0 | 5.0 | 68 | $2 \backslash 2$ | 18/18 | 1.4 | 5.0 | 76 |
| 10 | 10-11 | 4-3 | 39.5 | $2 \backslash 2$ | 27/18 | 2.0 | 5.0 | 74 | $2 \backslash 2$ | 18/18 | 1.4 | 5.0 | 83 |
| 11 | 11-4 | 5-0 | 48.2 | 2\2 | 27/18 | 2.5 | 5.0 | 78 | $2 \backslash 2$ | 27/9 | 1.4 | 5.0 | 92 |
| 12 | 11-8 | 5-9 | 57.2 | 2\2 | 27/18 | 2.5 | 5.0 | 81 | $2 \backslash 2$ | 27/9 | 1.4 | 5.0 | 95 |
| 13 | 12-1 | 6-7 | 66.4 | 2\2 | 27/18 | 3.0 | 5.0 | 85 | $2 \backslash 2$ | 27/9 | 1.4 | 5.0 | 99 |
| 14 | 12-5 | 7-4 | 76.0 | 2\2 | 27/9 | 2.0 | 5.0 | 102 | $2 \backslash 2$ | 18/9 | 1.4 | 5.0 | 111 |
| 15 | 11-7 | 2-10 | 28.1 | 2\2 | 27/18 | 2.5 | 5.0 | 70 | $2 \backslash 2$ | 27/9 | 1.4 | 5.0 | 88 |
| 16 | 11-11 | 3-7 | 37.4 | $2 \backslash 2$ | 27/18 | 2.5 | 5.0 | 76 | $2 \backslash 2$ | 27/9 | 1.4 | 5.0 | 94 |
| 17 | 12-3 | 4-5 | 46.9 | $2 \backslash 2$ | 27/9 | 2.0 | 5.0 | 99 | $2 \backslash 2$ | 18/9 | 1.4 | 5.0 | 108 |
| 18 | 12-7 | 5-2 | 56.6 | 2\2 | 27/9 | 2.0 | 5.0 | 102 | 2\2 | 18/9 | 1.4 | 5.0 | 111 |
| 19 | 12-11 | 6-0 | 66.6 | 2\2 | 27/9 | 2.0 | 5.0 | 106 | $3 \backslash 3$ | 18/9 | 1.4 | 5.0 | 121 |
| 20 | 13-3 | 6-9 | 76.9 | 2\2 | 27/9 | 2.0 | 5.0 | 110 | $3 \backslash 3$ | 18/9 | 1.4 | 5.0 | 125 |
| STRUCTURES 21 THROUGH 39 HAVE TYPE II HAUNCH AND TYPE VI CROWN RIBS |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 | 13-0 | 3-0 | 33.8 | $2 \backslash 2$ | 54/18 | 3.0 | 5.0 | 71 | $2 \backslash 2$ | 27/18 | 1.4 | 5.0 | 78 |
| 22 | 13-4 | 3-10 | 44.2 | 2\2 | 27/18 | 2.0 | 5.0 | 83 | $2 \backslash 2$ | 18/18 | 1.4 | 5.0 | 91 |
| 23 | 13-7 | 4-7 | 54.8 | 2\2 | 27/18 | 2.0 | 5.0 | 89 | $2 \backslash 2$ | 18/18 | 1.4 | 5.0 | 98 |
| 24 | 13-10 | 5-5 | 65.6 | 2\2 | 27/18 | 2.5 | 5.0 | 92 | $3 \backslash 3$ | 18/18 | 1.4 | 5.0 | 122 |
| 25 | 14-1 | 6-2 | 76.6 | 2\2 | 27/18 | 2.5 | 5.0 | 96 | $3 \backslash 3$ | 18/18 | 1.4 | 5.0 | 126 |
| 26 | 14-5 | 3-3 | 40.0 | 2\2 | 27/18 | 3.0 | 5.0 | 85 | $3 \backslash 3$ | 18/9 | 1.4 | 5.0 | 125 |
| 27 | 14-8 | 4-1 | 51.5 | 2\2 | 27/18 | 3.0 | 5.0 | 91 | $3 \backslash 2$ | 18/9 | 1.4 | 5.0 | 129 |
| 28 | 14-10 | 4-10 | 63.2 | $2 \backslash 2$ | 27/18 | 3.5 | 5.0 | 106 | $3 \backslash 2$ | 18/9 | 1.4 | 5.0 | 137 |
| 29 | 15-1 | 5-8 | 75.1 | 2\2 | 18/18 | 2.5 | 5.0 | 116 | $3 \backslash 2$ | 18/9 | 1.4 | 5.0 | 141 |
| 30 | 15-4 | 6-5 | 87.2 | 2\2 | 18/18 | 2.5 | 5.0 | 119 | $3 \backslash 2$ | 18/9 | 1.4 | 5.0 | 145 |
| 31 | 15-6 | 7-3 | 99.4 | 2\2 | 18/18 | 2.5 | 5.0 | 123 | $3 \backslash 2$ | 18/9 | 1.4 | 5.0 | 149 |
| 32 | 15-9 | 8-0 | 111.8 | $3 \backslash 2$ | 18/18 | 2.5 | 5.0 | 136 | $3 \backslash 2$ | 18/9 | 1.4 | 5.0 | 153 |
| 33 | 15-10 | 3-6 | 46.8 | $3 \backslash 2$ | 18/18 | 2.5 | 5.0 | 114 | $3 \backslash 2$ | 18/9 | 1.4 | 5.0 | 156 |
| 34 | 16-0 | 4-3 | 59.5 | $3 \backslash 2$ | 18/18 | 2.5 | 5.0 | 121 | $3 \backslash 2$ | 18/9 | 1.4 | 5.0 | 163 |
| 35 | 16-2 | 5-1 | 72.3 | $3 \backslash 2$ | 18/18 | 2.5 | 5.0 | 128 | $4 \backslash 2$ | 18/9 | 1.4 | 5.0 | 177 |
| 36 | 16-4 | 5-11 | 85.2 | $3 \backslash 2$ | 18/9 | 2.0 | 5.0 | 174 | $4 \backslash 2$ | 18/9 | 1.4 | 5.0 | 182 |
| 37 | 16-6 | 6-8 | 98.3 | $3 \backslash 2$ | 18/9 | 2.0 | 5.0 | 179 | $4 \backslash 2$ | 18/9 | 1.4 | 5.0 | 187 |
| 38 | 16-8 | 7-6 | 111.5 | $3 \backslash 2$ | 18/9 | 2.0 | 5.0 | 183 | $4 \backslash 2$ | 18/9 | 1.4 | 5.0 | 192 |
| 39 | 16-10 | 8-3 | 124.8 | $3 \backslash 2$ | 18/9 | 2.5 | 5.0 | 187 | $4 \backslash 2$ | 18/9 | 1.4 | 5.0 | 197 |
| STRUCTURES 40 THROUGH 87 USE ALL TYPE VI RIBS |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 40 | 17-9 | 3-10 | 54.4 | 2\2 | 27/18 | 2.5 | 5.0 | 124 | 2\2 | 27/9 | 1.4 | 5.0 | 170 |
| 41 | 18-2 | 4-7 | 68.3 | $2 \backslash 2$ | 27/18 | 2.5 | 5.0 | 131 | $2 \backslash 2$ | 27/9 | 1.4 | 5.0 | 178 |
| 42 | 18-7 | 5-4 | 82.5 | 2\2 | 27/18 | 3.0 | 5.0 | 139 | $2 \backslash 2$ | 27/9 | 1.4 | 5.0 | 185 |
| 43 | 19-0 | 6-1 | 97.1 | 2\2 | 27/9 | 2.0 | 5.0 | 188 | $2 \backslash 2$ | 18/9 | 1.4 | 5.0 | 203 |
| 44 | 19-5 | 6-11 | 111.9 | 2\2 | 27/9 | 2.0 | 5.0 | 192 | $2 \backslash 2$ | 18/9 | 1.4 | 5.0 | 207 |
| 45 | 19-10 | 7-8 | 127.1 | 2\2 | 27/9 | 2.0 | 5.0 | 195 | 2\2 | 18/9 | 1.4 | 5.0 | 210 |
| 46 | 20-3 | 8-5 | 142.6 | 2\2 | 27/9 | 3.0 | 5.0 | 199 | 2\2 | 18/9 | 1.4 | 5.0 | 214 |
| 47 | 19-1 | 4-2 | 63.3 | $2 \backslash 2$ | 27/9 | 2.0 | 5.0 | 185 | $2 \backslash 2$ | 18/9 | 1.4 | 5.0 | 194 |
| 48 | 19-5 | 4-11 | 78.3 | $2 \backslash 2$ | 27/9 | 2.0 | 5.0 | 192 | $2 \backslash 2$ | 18/9 | 1.4 | 5.0 | 203 |
| 49 | 19-9 | 5-8 | 93.6 | $2 \backslash 2$ | 27/9 | 2.0 | 5.0 | 199 | $2 \backslash 2$ | 18/9 | 1.4 | 5.0 | 211 |
| 50 | 20-1 | 6-6 | 109.2 | $2 \backslash 2$ | 18/18 | 2.5 | 5.0 | 165 | $2 \backslash 2$ | 18/9 | 1.4 | 5.0 | 218 |
| 51 | 20-6 | 7-3 | 125.0 | $2 \backslash 2$ | 18/18 | 2.5 | 5.0 | 168 | $2 \backslash 2$ | 18/9 | 1.4 | 5.0 | 222 |
| 52 | 20-10 | 8-1 | 141.2 | $2 \backslash 2$ | 18/18 | 3.0 | 5.0 | 172 | $2 \backslash 2$ | 18/9 | 1.4 | 5.0 | 225 |
| 53 | 21-2 | 8-10 | 157.6 | $2 \backslash 2$ | 18/18 | 3.0 | 5.0 | 175 | $2 \backslash 2$ | 18/9 | 1.4 | 5.0 | 229 |
| 54 | 20-4 | 4-6 | 73.1 | $2 \backslash 2$ | 18/18 | 2.5 | 5.0 | 152 | $2 \backslash 2$ | 18/9 | 1.4 | 5.0 | 211 |
| 55 | 20-7 | 5-3 | 89.2 | 2\2 | 18/18 | 2.5 | 5.0 | 161 | 2\2 | 18/9 | 1.4 | 5.0 | 220 |
| 56 | 20-11 | 6-1 | 105.5 | 2\2 | 18/18 | 3.0 | 5.0 | 170 | 2\2 | 18/9 | 1.4 | 5.0 | 229 |
| 57 | 21-3 | 6-10 | 122.1 | 2\2 | 18/18 | 3.0 | 5.0 | 174 | 2\2 | 18/9 | 1.4 | 5.0 | 233 |
| 58 | 21-6 | 7-8 | 139.0 | 2\2 | 18/9 | 2.0 | 5.0 | 235 | $3 \backslash 3$ | 18/9 | 1.4 | 5.0 | 249 |
| 59 | 21-10 | 8-5 | 156.0 | 2\2 | 18/9 | 2.0 | 5.0 | 239 | $3 \backslash 3$ | 18/9 | 1.4 | 5.0 | 253 |
| 60 | 22-1 | 9-3 | 173.3 | 2\2 | 18/9 | 2.0 | 5.0 | 243 | $3 \backslash 3$ | 18/9 | 1.4 | 5.0 | 257 |
| 61 | 21-7 | 4-11 | 83.8 | $2 \backslash 2$ | 18/9 | 2.0 | 5.0 | 225 | $3 \backslash 3$ | 18/9 | 1.4 | 5.0 | 236 |
| 62 | 21-10 | 5-8 | 101.0 | 2\2 | 18/9 | 2.0 | 5.0 | 234 | $3 \backslash 3$ | 18/9 | 1.4 | 5.0 | 246 |
| 63 | 22-1 | 6-6 | 118.4 | $2 \backslash 2$ | 18/9 | 2.0 | 5.0 | 243 | $3 \backslash 3$ | 18/9 | 1.4 | 5.0 | 256 |
| 64 | 22-3 | 7-3 | 135.9 | $2 \backslash 2$ | 18/9 | 2.0 | 5.0 | 246 | 4\4 | 18/9 | 1.4 | 5.0 | 273 |
| 65 | 22-6 | 8-1 | 153.7 | $2 \backslash 2$ | 18/9 | 2.0 | 5.0 | 250 | 4\4 | 18/9 | 1.4 | 5.0 | 278 |
| 66 | 22-9 | 8-10 | 171.6 | $2 \backslash 2$ | 18/9 | 2.0 | 5.0 | 253 | $5 \backslash 5$ | 18/9 | 1.4 | 5.0 | 297 |
| 67 | 23-0 | 9-8 | 189.8 | $2 \backslash 2$ | 18/9 | 2.0 | 5.0 | 257 | $5 \backslash 5$ | 18/9 | 1.4 | 5.0 | 303 |
| 68 | 22-9 | 5-4 | 95.5 | 2\2 | 18/9 | 2.0 | 5.0 | 239 | 4\4 | 18/9 | 1.4 | 5.0 | 263 |
| 69 | 23-0 | 6-1 | 113.7 | $2 \backslash 2$ | 18/9 | 2.0 | 5.0 | 248 | $5 \backslash 5$ | 18/9 | 1.4 | 5.0 | 286 |
| 70 | 23-2 | 6-11 | 132.1 | 2\2 | 18/9 | 2.0 | 5.0 | 266 | 5\5 | 18/9 | 1.4 | 5.0 | 297 |
| 71 | 23-4 | 7-8 | 150.6 | 2\2 | 18/9 | 2.5 | 5.0 | 270 | 5\5 | 18/9 | 1.4 | 5.0 | 303 |
| 72 | 23-6 | 8-6 | 169.3 | $2 \backslash 2$ | 18/9 | 2.5 | 5.0 | 274 | 5\5 | 18/9 | 1.4 | 5.0 | 308 |
| 73 | 23-8 | 9-3 | 188.1 | $2 \backslash 2$ | 18/9 | 2.5 | 5.0 | 278 | 5\5 | 18/9 | 1.4 | 5.0 | 314 |
| 74 | 23-10 | 10-1 | 207.0 | 2\2 | 18/9 | 2.5 | 5.0 | 283 | $5 \backslash 5$ | 18/9 | 1.4 | 5.0 | 319 |
| 75 | 24-0 | 5-9 | 108.2 | 212 | 18/9 | 2.5 | 5.0 | 254 | $6 \backslash 6$ | 18/9 | 1.4 | 5.0 | 304 |
| 76 | 24-1 | 6-6 | 127.5 | 212 | 18/9 | 2.5 | 5.0 | 263 | $6 \backslash 6$ | 18/9 | 1.4 | 5.0 | 316 |
| 77 | 24-3 | 7-4 | 146.8 | $2 \backslash 2$ | 18/9 | 2.5 | 5.0 | 272 | $6 \backslash 6$ | 18/9 | 1.4 | 5.0 | 327 |
| 78 | 24-4 | 8-2 | 166.2 | 2\2 | 18/9 | 2.5 | 5.0 | 275 | $6 \backslash 6$ | 18/9 | 1.4 | 5.0 | 334 |
| 79 | 24-5 | 8-11 | 185.7 | 2\2 | 18/9 | 2.5 | 5.0 | 279 | $6 \backslash 6$ | 18/9 | 1.4 | 5.0 | 340 |
| 80 | 24-7 | 9-9 | 205.3 | 2\2 | 18/9 | 2.5 | 5.0 | 283 | $6 \backslash 6$ | 18/9 | 1.4 | 5.0 | 346 |
| 81 | 24-8 | 10-6 | 225.0 | $2 \backslash 2$ | 18/9 | 2.5 | 5.0 | 286 | $7 \backslash 7$ | 18/9 | 1.4 | 5.0 | 369 |
| 82 | 25-2 | 6-2 | 122.0 | 2\2 | 18/9 | 2.5 | 5.0 | 268 | $7 \backslash 7$ | 18/9 | 1.4 | 5.0 | 334 |
| 83 | 25-2 | 7-0 | 142.2 | 2\2 | 18/9 | 2.5 | 5.0 | 277 | $7 \backslash 7$ | 18/9 | 1.4 | 5.0 | 347 |
| 84 | 25-3 | 7-9 | 162.4 | 2\2 | 18/9 | 2.5 | 5.0 | 286 | $7 \backslash 7$ | 18/9 | 1.4 | 5.0 | 359 |
| 85 | 25-4 | 8-7 | 182.6 | $2 \backslash 2$ | 18/9 | 2.5 | 5.0 | 290 | 777 | 18/9 | 1.4 | 5.0 | 366 |
| 86 <br> 87 | $\begin{array}{r}25-4 \\ 25-5 \\ \hline\end{array}$ | 9-5 $10-2$ | $\begin{array}{r}202.9 \\ 223.3 \\ \hline\end{array}$ | 212 | 18/9 | 2.5 <br> 2.5 | 5.0 <br> 5.0 | 293 <br> 297 | 7\7 | 18/9 | 1.4 1.4 | 5.0 <br> 5.0 | 373 <br> 380 |

Box Culvert Shell-Plate and Rib Dafa (HL-93)

| TABLE 49B. ALBC SHELL DATA - LRFD HL93 PLATE AND RIB COMBINATIONS WITH ALLOWABLE HEIGHT OF COVER |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Structure <br> Number | $\begin{gathered} \text { Span } \\ \text { (Ft.-In.) } \end{gathered}$ | $\begin{gathered} \text { Rise } \\ \text { (Ft.-In.) } \end{gathered}$ | $\begin{gathered} \text { Area } \\ \text { (Sq. Ft.) } \end{gathered}$ | HG\CG <br> (Gage) | HRS/CRS (Inches) | L1 <br> Min. ${ }^{(3)}$ <br> (Feet) | Max. <br> (Feet) | Shell Wt/Ft <br> (Lbs.) | HG\CG (Gage) | HRS/CRS (Inches) | $\begin{gathered} \text { L2 } \\ \text { Min. }{ }^{(3)} \\ \text { (Feet) } \end{gathered}$ | Max. <br> (Feet) | Shell Wt/Ft <br> (Lbs.) |
| STRUCTURES 88 THROUGH 143 USE ALL TYPE VI RIBS |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 88 | 26-7 | 5-5 | 111.6 | $3 \backslash 3$ | 9\9 | 2.9 | 5.0 | 314 | 7\7 | 9\9 | 2.0 | 5.0 | 367 |
| 89 | 27-0 | 6-3 | 132.4 | $3 \backslash 3$ | $9 \backslash 9$ | 2.9 | 5.0 | 329 | $7 \backslash 7$ | $9 \backslash 9$ | 2.0 | 5.0 | 384 |
| 90 | 27-5 | 7-0 | 153.4 | $3 \backslash 3$ | $9 \backslash 9$ | 2.9 | 5.0 | 344 | $7 \backslash 7$ | $9 \backslash 9$ | 2.0 | 5.0 | 402 |
| 91 | 27-10 | 7-9 | 174.8 | $3 \backslash 3$ | $9 \backslash 9$ | 2.9 | 5.0 | 360 | $7 \backslash 7$ | 9 99 | 2.0 | 5.0 | 420 |
| 92 | 28-3 | 8-7 | 196.5 | $3 \backslash 3$ | $9 \backslash 9$ | 2.9 | 5.0 | 364 | $7 \backslash 7$ | $9 \backslash 9$ | 2.0 | 5.0 | 427 |
| 93 | 28-8 | 9-4 | 218.6 | $3 \backslash 3$ | $9 \backslash 9$ | 2.9 | 5.0 | 368 | $7 \backslash 7$ | $9 \backslash 9$ | 2.0 | 5.0 | 434 |
| 94 | 29-1 | 10-1 | 241.0 | $3 \backslash 3$ | $9 \backslash 9$ | 2.9 | 5.0 | 372 | $7 \backslash 7$ | $9 \backslash 9$ | 2.0 | 5.0 | 441 |
| 95 | 27-10 | 5-10 | 125.4 | $3 \backslash 3$ | 9\9 | 2.9 | 5.0 | 329 | $7 \backslash 7$ | $9 \backslash 9$ | 2.0 | 5.0 | 384 |
| 96 | 28-3 | 6-8 | 147.3 | $3 \backslash 3$ | $9 \backslash 9$ | 2.9 | 5.0 | 344 | $7 \backslash 7$ | $9 \backslash 9$ | 2.0 | 5.0 | 402 |
| 97 | 28-7 | 7-5 | 169.4 | $3 \backslash 3$ | $9 \backslash 9$ | 2.9 | 5.0 | 360 | $7 \backslash 7$ | 9 99 | 2.0 | 5.0 | 420 |
| 98 | 29-0 | 8-3 | 191.8 | $3 \backslash 3$ | $9 \backslash 9$ | 2.9 | 5.0 | 375 | $7 \backslash 7$ | $9 \backslash 9$ | 2.0 | 5.0 | 438 |
| 99 | 29-4 | 9-0 | 214.6 | $3 \backslash 3$ | $9 \backslash 9$ | 2.9 | 5.0 | 379 | $7 \backslash 7$ | $9 \backslash 9$ | 2.0 | 5.0 | 445 |
| 100 | 29-8 | 9-9 | 237.6 | $3 \backslash 3$ | $9 \backslash 9$ | 2.9 | 5.0 | 383 | $7 \backslash 7$ | $9 \backslash 9$ | 2.0 | 5.0 | 452 |
| 101 | 30-1 | 10-7 | 260.9 | $3 \backslash 3$ | $9 \backslash 9$ | 2.9 | 5.0 | 387 | 7\7 | $9 \backslash 9$ | 2.0 | 5.0 | 459 |
| 102 | 29-1 | 6-4 | 140.2 | $3 \backslash 3$ | $9 \backslash 9$ | 2.9 | 5.0 | 344 | 7\7 | $9 \backslash 9$ | 2.0 | 5.0 | 402 |
| 103 | 29-5 | 7-1 | 163.2 | $3 \backslash 3$ | $9 \backslash 9$ | 2.9 | 5.0 | 360 | $7 \backslash 7$ | $9 \backslash 9$ | 2.0 | 5.0 | 420 |
| 104 | 29-8 | 7-11 | 186.4 | $3 \backslash 3$ | $9 \backslash 9$ | 2.9 | 5.0 | 375 | 7\7 | $9 \backslash 9$ | 2.0 | 5.0 | 438 |
| 105 | 30-0 | 8-8 | 209.8 | $3 \backslash 3$ | $9 \backslash 9$ | 2.9 | 5.0 | 390 | $7 \backslash 7$ | $9 \backslash 9$ | 2.0 | 5.0 | 456 |
| 106 | 30-4 | 9-5 | 233.6 | $3 \backslash 3$ | $9 \backslash 9$ | 2.9 | 5.0 | 394 | $7 \backslash 7$ | $9 \backslash 9$ | 2.0 | 5.0 | 463 |
| 107 | 30-8 | 10-3 | 257.5 | $3 \backslash 3$ | 9\9 | 2.9 | 5.0 | 398 | 7\7 | 9\9 | 2.0 | 5.0 | 470 |
| 108 | 31-0 | 11-0 | 281.8 | $3 \backslash 3$ | 9\9 | 2.9 | 5.0 | 403 | 7\7 | $9 \backslash 9$ | 2.0 | 5.0 | 477 |
| 109 | 31-3 | 6-9 | 156.1 | $3 \backslash 3$ | $9 \backslash 9$ | 2.9 | 5.0 | 360 | $7 \backslash 7$ | $9 \backslash 9$ | 2.0 | 5.0 | 420 |
| 110 | 30-6 | 7-7 | 180.1 | $3 \backslash 3$ | 9\9 | 2.9 | 5.0 | 375 | 7\7 | 9\9 | 2.0 | 5.0 | 438 |
| 111 | 30-10 | 8-4 | 204.4 | $3 \backslash 3$ | $9 \backslash 9$ | 2.9 | 5.0 | 390 | $7 \backslash 7$ | $9 \backslash 9$ | 2.0 | 5.0 | 456 |
| 112 | 31-1 | 9-2 | 228.8 | $3 \backslash 3$ | $9 \backslash 9$ | 2.9 | 5.0 | 405 | $7 \backslash 7$ | $9 \backslash 9$ | 2.0 | 5.0 | 474 |
| 113 | 31-4 | 9-11 | 253.5 | $3 \backslash 3$ | 9\9 | 2.9 | 5.0 | 409 | 7\7 | 9\9 | 2.0 | 5.0 | 481 |
| 114 | 31-8 | 10-9 | 278.4 | $3 \backslash 3$ | 9\9 | 2.9 | 5.0 | 414 | $7 \backslash 7$ | $9 \backslash 9$ | 2.0 | 5.0 | 487 |
| 115 | 31-11 | 11-6 | 303.5 | $3 \backslash 3$ | $9 \backslash 9$ | 2.9 | 5.0 | 418 | $7 \backslash 7$ | $9 \backslash 9$ | 2.0 | 5.0 | 494 |
| 116 | 31-5 | 7-3 | 173.1 | $3 \backslash 3$ | 9\9 | 2.9 | 5.0 | 375 | 7\7 | 9\9 | 2.0 | 5.0 | 438 |
| 117 | 31-8 | 8-0 | 198.2 | $3 \backslash 3$ | 9\9 | 2.9 | 5.0 | 390 | $7 \backslash 7$ | $9 \backslash 9$ | 2.0 | 5.0 | 456 |
| 118 | 31-10 | 8-10 | 223.4 | $3 \backslash 3$ | 9\9 | 2.9 | 5.0 | 405 | $7 \backslash 7$ | $9 \backslash 9$ | 2.0 | 5.0 | 474 |
| 119 | 32-1 | 9-8 | 248.8 | $3 \backslash 3$ | $9 \backslash 9$ | 2.9 | 5.0 | 420 | $7 \backslash 7$ | $9 \backslash 9$ | 2.0 | 5.0 | 491 |
| 120 | 32-4 | 10-4 | 274.4 | $3 \backslash 3$ | 9\9 | 2.9 | 5.0 | 424 | 7\7 | 9\9 | 2.0 | 5.0 | 498 |
| 121 | 32-7 | 11-3 | 300.1 | $3 \backslash 3$ | 9\9 | 2.9 | 5.0 | 429 | 7\7 | $9 \backslash 9$ | 2.0 | 5.0 | 505 |
| 122 | 32-9 | 12-0 | 326.1 | $3 \backslash 3$ | $9 \backslash 9$ | 2.9 | 5.0 | 433 | $7 \backslash 7$ | $9 \backslash 9$ | 2.0 | 5.0 | 512 |
| 123 | 32-7 | 7-9 | 191.3 | $3 \backslash 3$ | $9 \backslash 9$ | 2.9 | 5.0 | 390 | $7 \backslash 7$ | $9 \backslash 9$ | 2.0 | 5.0 | 456 |
| 124 | 32-9 | 8-6 | 217.3 | $3 \backslash 3$ | 9\9 | 2.9 | 5.0 | 405 | $7 \backslash 7$ | $9 \backslash 9$ | 2.0 | 5.0 | 474 |
| 125 | 32-11 | 9-4 | 243.4 | $3 \backslash 3$ | $9 \backslash 9$ | 2.9 | 5.0 | 420 | $7 \backslash 7$ | $9 \backslash 9$ | 2.0 | 5.0 | 491 |
| 126 | 33-1 | 10-2 | 269.7 | $3 \backslash 3$ | $9 \backslash 9$ | 2.9 | 5.0 | 435 | $7 \backslash 7$ | $9 \backslash 9$ | 2.0 | 5.0 | 509 |
| 127 | 33-3 | 10-11 | 296.4 | $3 \backslash 3$ | 9\9 | 2.9 | 5.0 | 440 | 7\7 | 9\9 | 2.0 | 5.0 | 516 |
| 128 | 33-5 | 11-9 | 322.8 | $3 \backslash 3$ | $9 \backslash 9$ | 2.9 | 5.0 | 444 | $7 \backslash 7$ | $9 \backslash 9$ | 2.0 | 5.0 | 523 |
| 129 | 33-8 | 12-6 | 349.5 | $3 \backslash 3$ | $9 \backslash 9$ | 2.9 | 5.0 | 448 | $7 \backslash 7$ | $9 \backslash 9$ | 2.0 | 5.0 | 530 |
| 130 | 33-8 | 8-3 | 210.5 | $3 \backslash 3$ | 9\9 | 2.9 | 5.0 | 405 | 7\7 | 9\9 | 2.0 | 5.0 | 474 |
| 131 | 33-9 | 9-1 | 237.5 | $3 \backslash 3$ | $9 \backslash 9$ | 2.9 | 5.0 | 420 | 7\7 | $9 \backslash 9$ | 2.0 | 5.0 | 491 |
| 132 | 33-11 | 9-10 | 264.5 | $3 \backslash 3$ | $9 \backslash 9$ | 2.9 | 5.0 | 435 | $7 \backslash 7$ | $9 \backslash 9$ | 2.0 | 5.0 | 509 |
| 133 | 34-0 | 10-8 | 291.7 | $3 \backslash 3$ | 9\9 | 2.9 | 5.0 | 451 | 7\7 | 9\9 | 2.0 | 5.0 | 527 |
| 134 | 34-2 | 11-5 | 319.0 | $3 \backslash 3$ | $9 \backslash 9$ | 2.9 | 5.0 | 455 | 7\7 | $9 \backslash 9$ | 2.0 | 5.0 | 534 |
| 135 | 34-3 | 12-3 | 346.4 | $3 \backslash 3$ | $9 \backslash 9$ | 2.9 | 5.0 | 459 | $7 \backslash 7$ | $9 \backslash 9$ | 2.0 | 5.0 | 541 |
| 136 | 34-5 | 13-1 | 373.8 | $3 \backslash 3$ | 9\9 | 2.9 | 5.0 | 463 | 7\7 | 9\9 | 2.0 | 5.0 | 548 |
| 137 | 34-9 | 8-9 | 230.9 | $3 \backslash 3$ | 9\9 | 2.9 | 5.0 | 420 | 7\7 | 9\9 | 2.0 | 5.0 | 491 |
| 138 | 34-10 | 9-7 | 258.1 | $3 \backslash 3$ | $9 \backslash 9$ | 2.9 | 5.0 | 435 | 7\7 | $9 \backslash 9$ | 2.0 | 5.0 | 509 |
| 139 | 34-11 | 10-4 | 286.7 | $3 \backslash 3$ | 9\9 | 2.9 | 5.0 | 451 | 7\7 | 9\9 | 2.0 | 5.0 | 527 |
| 140 | 35-0 | 11-2 | 314.6 | $3 \backslash 3$ | 9\9 | 2.9 | 5.0 | 466 | 7\7 | $9 \backslash 9$ | 2.0 | 5.0 | 545 |
| 141 | 35-2 | 12-0 | 342.7 | $3 \backslash 3$ | $9 \backslash 9$ | 2.9 | 5.0 | 470 | $7 \backslash 7$ | $9 \backslash 9$ | 2.0 | 5.0 | 552 |
| 142 | 35-2 | 12-9 | 370.8 | $3 \backslash 3$ | $9 \backslash 9$ | 2.9 | 5.0 | 474 | 7\7 | 9\9 | 2.0 | 5.0 | 559 |
| 143 | 35-3 | 13-7 | 399.0 | $3 \backslash 3$ | 9\9 | 2.9 | 5.0 | 476 | $7 \backslash 7$ | 9\9 | 2.0 | 5.0 | 563 |

Notes

1. The cover height is measured from the outside valley crown plate corrugation to the bottom of a flexible pavement, or to the top of a rigid pavement.
2. Plate thickness designations: $2=.125^{\prime \prime}, 3=.150^{\prime \prime}, 4=.175^{\prime \prime}, 5=.200^{\prime \prime}, 6=.255^{\prime \prime}, 7=.250^{\prime \prime}$
3. The maximum cover for Aluminum Box Culverts with full inverts and footing pads should not exceed 4 feet. Special full invert and footing pad designs or slotted concrete footings can accommodate maximum covers to the limits shown in Tables 49A and 49B.
4. Check with your Contech representative to see if additional options are available.


Aluminum Box Culvert Pedestrian Underpass



Stream Crossing for Environmentally Sensitive Areas

Headwall and Wingwall Details


Panel Entrenchment
${ }^{(2)}$ (Approx. 2')

## Typical Headwall Elevation



1. All panels are fabricated from aluminum structural plate as specified in ASTM B 746.
2. Height of headwall listed in Table 50B permits approximately $24^{\prime \prime}$ entrenchment depth below the invert. All wingwall and headwall end panels must be trenched into existing ground.
3. Horizontal rotation on the wingwall should not exceed $90^{\circ}$.
4. The top of a headwall and its wingwall is always horizontal, unless beveled wingwalls are required.
5. Standard headwalls shown are for vertical orientation only.
6. If side slope is flatter than $2: 1$, a double tieback assembly is required for each deadman.
7. Standard headwalls are shown. HS-20 and HS-25 wheel loads must be kept a minimum distance of $36^{\prime \prime}$ from the wall face. Special headwall packages can be fabricated to meet other loading requirements.
8. For details on single and dual deadman anchors, refer to next page.
9. Structures on concrete footings with headwalls require field modification of the headwall plates to fit around the footings.
10. Aluminum headwalls may be used only on square-ended structures. Structure length must be an increment of 9 inches, if these headwalls are utilized at both ends.

| HEADWALL |  |  |  | WINGWALLS |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Wall Height | Center Panel <br> Thickness | End Panel Thickness | Wale Beam Distance from top of HW | Panel Thickness | e Anchor <br> Wale Beam Distance from top of HW | Panel Thickness | Anchors <br> Wale Beam - <br> Distance from top of HW "D" | 0.150 " thick Deadman Size | 3/4"dia Rod Length |
| $6^{\prime} 2^{\prime \prime}$ to $8^{\prime \prime} 7{ }^{\prime \prime}$ | $0.125^{\prime \prime}$ | 0.150 " | N/A | $0.125^{\prime \prime}$ | $3^{\prime \prime} 0^{\prime \prime}$ | $0.125^{\prime \prime}$ | 2'6" | $1^{\prime \prime} 8^{\prime \prime} \times 2^{\prime} 43 / 4^{\prime \prime}$ | $12^{\prime \prime} 6^{\prime \prime}$ |
| $9^{\prime} 4^{\prime \prime}$ to 11'9" | $0.125^{\prime \prime}$ | $0.150 \prime \prime$ | N/A | $0.15{ }^{\prime \prime}$ | 3'6" | $0.125^{\prime \prime}$ | $3^{\prime \prime} 0^{\prime \prime}$ | $1^{\prime \prime} 8^{\prime \prime} \times 2^{\prime} 43 / 4^{\prime \prime}$ | 12'6" |
| 12'7" to 14'2" | $0.125^{\prime \prime}$ | $0.150^{\prime \prime}$ | N/A | N/A | N/A | 0.150 " | $3^{\prime \prime} 6^{\prime \prime}$ | $1^{\prime \prime} 8^{\prime \prime} \times 2^{\prime} 43 / 4^{\prime \prime}$ | 12'6" |

ANYTHING GREATER THAN 14'2": INQUIRE


Headwall Dimensions for H-20, HS-20, H-25, HS-25 Loading

| TABLE 50B. HEADWALL |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| No. | Width | Height | No. of Anchor Rods | No. | Width | Height | No. of Anchor Rods |
| 1 | 13'-6" | 6'-2' | 3 | 88 | 33'-0" | 9'-4" | 7 |
| 2 | 13'-6" | 6'11" | 3 | 89 | 33'-0" | 10'-2" | 7 |
| 3 | 13'-6" | 7'-9" | 3 | 90 | 33'-0" | 10'-11" | 7 |
| 4 | 13'-6" | 8'6" | 3 | 91 | 33'-0" | 11-9" | 7 |
| 5 | 13'-6" | 9'-4" | 3 | 92 | 33'-0" | 12'-7" | 7 |
| 6 | 13'-6" | 10'-2" | 3 | 93 | 33'-0" | 13'-4" | 7 |
| 7 | 13'-6" | 10'11" | 3 | 94 | 33'-0" | 14'-2" | 7 |
| 8 | 15'-0" | $6{ }^{\prime \prime} 1$ | 3 | 95 | 34'-6" | 10'-2" | 8 |
| 9 | 15'-0" | 7'-9" | 3 | 96 | 34'-6" | 10'-11" | 8 |
| 10 | 15'-0" | 8'6" | 3 | 97 | 34'-6" | 11'-9" | 8 |
| 11 | 15'-0" | 9'-4" | 3 | 98 | 34'-6" | 12'-7" | 8 |
| 12 | 15'-0" | 10'-2" | 3 | 99 | 34'-6" | 13'-4" | 8 |
| 13 | 15'-0" | 10'11" | 3 | 100 | 34'-6" | 14'-2" | 8 |
| 14 | 15'-0" | 11'-9" | 3 | 101 | 34'-6" | 15'1" | 8 |
| 15 | 16'-6" | 6'11" | 4 | 102 | 36'-0" | 10'-2" | 8 |
| 16 | 16'-6" | 7'-9" | 4 | 103 | 36'-0" | 10'-11 | 8 |
| 17 | 16'-6" | 8'6" | 4 | 104 | 36'-0" | 11'-9" | 8 |
| 18 | 16'-6" | $9^{\prime}-4{ }^{\prime \prime}$ | 4 | 105 | 36'-0" | 12'-7" | 8 |
| 19 | 16'-6" | 10'-2" | 4 | 106 | 36'-0" | 13'-4" | 8 |
| 20 | 16'-6" | 10'11" | 4 | 107 | 36'-0" | 14'-2" | 8 |
| 21 | 18'-0" | 6'11" | 4 | 108 | 36'-0" | 15'1" | 8 |
| 22 | 18'-0" | 7'-9" | 4 | 109 | 37'-6" | 10-11" | 8 |
| 23 | 18'-0" | 8'6" | 4 | 110 | 37'-6" | 11'-9" | 8 |
| 24 | 18'-0" | 9'-4" | 4 | 111 | 37'-6" | 12'-7" | 8 |
| 25 | 18'-0" | 10'-2" | 4 | 112 | 37'-6" | 13'-4" | 8 |
| 26 | 19'-6" | $6^{\prime \prime 11}$ | 4 | 113 | 37'-6" | 14'-2" | 8 |
| 27 | 19'-6" | 7'-9" | 4 | 114 | 37'-6" | 15'1" | 8 |
| 28 | 19'-6" | 8'6" | 4 | 115 | 37'-6" | 15'1" | 8 |
| 29 | 19'-6" | 9'-4" | 4 | 116 | 37'-6" | 11'-9" | 8 |
| 30 | 19'-6" | 10'-2" | 4 | 117 | 37'-6" | 12'-7" | 8 |
| 31 | 19'-6" | 10'11" | 4 | 118 | 37'-6" | 13'-4" | 8 |
| 32 | 19'-6" | 11'-9" | 4 | 119 | $37{ }^{\prime}-6{ }^{\prime \prime}$ | 14'-2" | 8 |
| 33 | 21'-0" | 7'-9" | 5 | 120 | 37'-6" | 15'1" | 8 |
| 34 | 21'-0" | 8'6" | 5 | 121 | 37'-6" | 15'1" | 8 |
| 35 | 21 '-0" | $9^{\prime}-4^{\prime \prime}$ | 5 | 122 | $37^{\prime}-6{ }^{\prime \prime}$ | 16'-8" | 8 |
| 36 | 21 -0" | 10'-2" | 5 | 123 | 37'-6" | 11'-9" | 8 |
| 37 | 21'-0" | 10'11" | 5 | 124 | 37'-6" | 12'-7" | 8 |
| 38 | 21'-0" | 11'-9" | 5 | 125 | 37'-6" | 13'-4" | 8 |
| 39 | 21'-0" | 12'-7" | 5 | 126 | 37'-6" | 14'-2" | 8 |
| 40 | 22'-6" | 7'-9" | 5 | 127 | 37'-6" | 15'1" | 8 |
| 41 | 22'-6" | 8'6" | 5 | 128 | $37{ }^{\prime}-6{ }^{\prime \prime}$ | 15'11" | 8 |
| 42 | 22'-6" | 9'-4" | 5 | 129 | 37'-6" | 16'-8" | 8 |
| 43 | 22'-6" | 10'-2" | 5 | 130 | 40'-6" | 12'-7" | 9 |
| 44 | 22'-6" | 10'11" | 5 | 131 | 40'-6" | 13'-4" | 9 |
| 45 | 22'-6" | 11-9" | 5 | 132 | 40'-6" | 14'-2" | 9 |
| 46 | 22'-6" | 12'-7" | 5 | 133 | 40'-6" | 15'1" | 9 |
| 47 | 24'-0" | 8'6" | 5 | 134 | 40'-6" | 15'11" | 9 |
| 48 | 24'-0" | 9'-4" | 5 | 135 | 40'-6" | 16'-8" | 9 |
| 49 | 24'-0" | 10'-2" | 5 | 136 | 40'-6" | 17'-5" | 9 |
| 50 | 24'-0" | 10'11" | 5 | 137 | 42'-0" | 13'-4" | 9 |
| 51 | 24'-0" | 11'-9" | 5 | 138 | 42'-0" | 14'-2" | 9 |
| 52 | 24'-0" | 12'-7" | 5 | 139 | 42'-0" | 15'1" | 9 |
| 53 | 24'-0" | 13'-4" | 5 | 140 | 42'-0" | 15'11" | 9 |
| 54 | 25'-6" | 8'6" | 6 | 141 | 42'-0" | 16'-8" | 9 |
| 55 | 25'-6" | $9{ }^{\prime}-4$ | 6 | 142 | $42^{\prime}-0^{\prime \prime}$ | 17'-5" | 9 |
| 56 | 25'-6" | 10'-2" | 6 | 143 | 42'-0" | 17'-5" | 9 |
| 57 | 25'-6" | 10'11" | 6 |  |  |  |  |
| 58 | 25'-6" | 11'-9" | 6 |  |  |  |  |
| 59 | 25'-6" | 12'-7" | 6 |  |  |  |  |
| 60 | 25'-6" | 13'-4" | 6 |  |  |  |  |
| 61 | 27'-0" | $9{ }^{\prime \prime} 4^{\prime \prime}$ | 6 |  |  |  |  |
| 62 | 27'-0" | 10'-2" | 6 |  |  |  |  |
| 63 | 27'-0" | 10'11" | 6 |  |  |  |  |
| 64 | 27'-0" | 11'-9" | 6 |  |  |  |  |
| 65 | 27'-0" | 12'-7" | 6 |  |  |  |  |
| 66 | 27'-0" | 13'-4" | 6 |  |  |  |  |
| 67 | 27-0" | 14'-2" | 6 |  |  |  |  |
| 68 | 28'-6" | $9{ }^{\prime}-4$ " | 6 |  |  |  |  |
| 69 | 28'-6" | 10'-2" | 6 |  |  |  |  |
| 70 | 28'-6" | 10'11 | 6 |  |  |  |  |
| 71 | 28'-6" | 11'-9" | 6 |  |  |  |  |
| 72 | 28'-6" | 12'-7" | 6 |  |  |  |  |
| 73 | 28'-6" | 13'-4" | 6 |  |  |  |  |
| 74 | 28'-6" | 14'-2" | 6 |  |  |  |  |
| 75 | 30'-0" | 9'-4" | 7 |  |  |  |  |
| 76 | 30'-0" | 10'-2" | 7 |  |  |  |  |
| 77 | 30'-0" | 10'11" | 7 |  |  |  |  |
| 78 | 30'-0" | 11'-9" | 7 |  |  |  |  |
| 79 | $30^{\prime}-0 \mid$ | 12'-7" | 7 |  |  |  |  |
| 80 | 30'-0" | 13'-4" | 7 |  |  |  |  |
| 81 | 30'-0" | 14'-2" | 7 |  |  |  |  |
| 82 | 31'-6" | 10'-2" | 7 |  |  |  |  |
| 83 | 31'-6" | 10'10 | 7 |  |  |  |  |
| 84 | 31'-6" | 11-9" | 7 |  |  |  |  |
| 85 | 31 -6" | 12'-7" | 7 |  |  |  |  |
| 86 | 31'-6" | 13'-4" | 7 |  |  |  |  |
| 87 | 31'-6" | 14'-2" | 7 |  |  |  |  |



Aluminum Full Invert Option ${ }^{(2,3,5,6)}$


Aluminum Bent Sheet Toewall Detail


Installation of Aluminum Box Culvert Toewall

Note: Flat sheet toewalls are available only for structures having a full corrugated aluminum invert.

## Notes

1. $\mathrm{N}=9.625^{\prime \prime}$ or $9^{5} / 8^{\prime \prime}$. Use N as a conversion factor. For example, for Structure No. 1, Width "F" is $13 \times \mathrm{N}$, or 125.13 ".
2. Minimum allowable soil-bearing pressure is $4,000 \mathrm{Lbs} . / \mathrm{Sq}$. Ft. for structures and details shown in this catalog. This applies specifically for width " G " below the receiving channel. Other conditions can be accommodated. Contact a Contech Representative for more information.
3. The maximum cover for Aluminum Box Culverts with full inverts and footing pads should not exceed 4 feet. Special full invert and footing pad designs or slotted concrete footings can accommodate maximum covers to the limits shown in Table 48 or Table 49.
4. Weight per foot of full invert includes receiving channels, scallop plates, nuts, bolts and all plates.
5. Full invert plates thickness are as shown. When reactions to the invert require additional thickness, supplemental plates of the thickness and width listed in Table 51 are furnished to bolt between the full invert and the receiving channel.
6. Invert widths 21 N and greater are two-pieces.
7. Invert plates must not be overlapped on adjacent structures unless appropriate design modifications are incorporated.


## Aluminum Scallop Plate <br> (Full Invert Only)

Invert Details

| TABLE 51A |  |  |  |  | TABLE 51B |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| FULL INVERT (H-20, HS-20) |  |  |  |  | FULL INVERT (H-25, HS-25, HL-93) |  |  |  |  |  |
| Structure Number | Width " ${ }^{\prime \prime}$ (N) | Supplemental Plate Thickness Width (inches) "G" (N) | Weight/Ft. (Lbs.) | Bolts/Ft. (Each) | Structure Number | Width $" F "(N)$ | Supplemental Plate Thickness (in) | $\begin{aligned} & \text { Width } \\ & \text { "G" (N) } \end{aligned}$ | Weight/Ft. (Lbs.) | Bolts/Ft. <br> (Each) |
| 1 | 13 | 2 | 26.1 | 5.78 | 1 | 13 |  | 2 | 26.1 | 5.78 |
| 2 | 14 | 2 | 27.6 | 6.00 | 2 | 14 |  | 2 | 27.6 | 6.00 |
| 3 | 14 | 2 | 27.6 | 6.00 | 3 | 14 |  | 2 | 27.6 | 6.00 |
| 4 | 15 | 2 | 29.1 | 6.22 | 4 | 15 |  | 2 | 29.1 | 6.22 |
| 5 | 16 | 2 | 30.5 | 6.44 | 5 | 16 | $\stackrel{\square}{0}$ | 2 | 30.5 | 6.44 |
| 6 | 16 | 2 | 30.5 | 6.44 | 6 | 16 | , | 2 | 30.5 | 6.44 |
| 7 | 17 | 2 | 32.0 | 6.67 | 7 | 17 | $\stackrel{\text { O}}{0}$ | 2 | 33.0 | 6.67 |
| 8 | 15 | 2 | 29.1 | 6.22 | 8 | 15 | ¢ | 2 | 29.8 | 6.23 |
| 9 | 16 | 2 | 30.5 | 6.44 | 9 | 16 | $\stackrel{\square}{\circ}$ | 2 | 30.5 | 6.44 |
| 10 | 16 | - 2 | 30.5 | 6.44 | 10 | 16 |  | 2 | 33.0 | 6.67 |
| 11 | 17 | - | 32.0 | 6.67 | 11 | 17 |  | 2 | 33.0 | 6.67 |
| 12 | 17 | - | 32.0 | 6.67 | 12 | 17 |  | 2 | 33.0 | 6.67 |
| 13 | 18 | $\stackrel{2}{\square}$ | 33.5 | 6.89 | 13 | 18 | . 100 | 2 | 38.8 | 6.67 |
| 14 | 18 | $\stackrel{\square}{\square}$ | 33.5 | 6.89 | 14 | 18 | . 100 | 2 | 38.8 | 6.67 |
| 15 | 17 | 2 | 32.0 | 6.67 | 15 | 17 | . 100 | 2 | 38.8 | 6.67 |
| 16 | 17 | 2 | 32.0 | 6.67 | 16 | 17 | . 100 | 2 | 38.8 | 6.67 |
| 17 | 18 | 2 | 33.5 | 6.89 | 17 | 18 | . 100 | 2 | 38.8 | 6.67 |
| 18 | 18 | 2 | 33.5 | 6.89 | 18 | 18 | . 100 | 2 | 42.0 | 7.11 |
| 19 | 19 | 2 | 35.0 | 7.11 | 19 | 19 | . 100 | 2 | 42.0 | 7.11 |
| 20 | 19 | 2 | 35.0 | 7.11 | 20 | 19 | . 100 | 2 | 42.0 | 7.11 |
| 21 | 19 | 2 | 35.0 | 7.11 | 21 | 19 | . 100 | 2 | 42.0 | 7.11 |
| 22 | 19 | 2 | 35.0 | 7.11 | 22 | 19 | . 100 | 2 | 42.0 | 7.11 |
| 23 | 19 | 2 | 35.0 | 7.11 | 23 | 19 | . 100 | 2 | 42.0 | 7.11 |
| 24 | 20 | 2 | 37.9 | 10.00 | 24 | 20 | . 100 | 2 | 46.3 | 12.45 |
| 25 | 20 | 2 | 37.9 | 10.00 | 25 | 20 | . 100 | 2 | 46.3 | 12.45 |
| 26 | 20 | . 1002 | 43.7 | 10.22 | 26 | 20 | . 100 | 2 | 46.3 | 12.45 |
| 27 | 21 | . 1002 | 45.2 | 10.22 | 27 | 21 | . 100 | 2 | 47.9 | 12.67 |
| 28 | 21 | . 1002 | 45.2 | 10.22 | 28 | 21 | . 100 | 2 | 47.9 | 12.67 |
| 29 | 21 | . 1002 | 45.2 | 10.22 | 29 | 21 | . 100 | 2 | 47.9 | 12.67 |
| 30 | 22 | . 1002 | 46.7 | 10.44 | 30 | 22 | . 100 | 2 | 47.9 | 12.67 |
| 31 | 22 | . 1002 | 46.7 | 10.44 | 31 | 22 | . 100 | 2 | 49.5 | 12.89 |
| 32 | 22 | . 1002 | 46.7 | 10.44 | 32 | 22 | . 100 | 2 | 49.5 | 12.89 |
| 33 | 22 | . 1002 | 46.7 | 10.44 | 33 | 22 | . 100 | 2 | 49.5 | 12.89 |
| 34 | 22 | . 1002 | 46.7 | 10.44 | 34 | 22 | . 100 | 2 | 49.5 | 12.89 |
| 35 | 23 | . 1002 | 48.2 | 10.67 | 35 | 23 | . 100 | 2 | 51.1 | 13.11 |
| 36 | 23 | . 1002 | 48.2 | 10.67 | 36 | 23 | . 100 | 2 | 51.1 | 13.11 |
| 37 | 23 | . 1002 | 48.2 | 10.67 | 37 | 23 | . 100 | 2 | 51.1 | 13.11 |
| 38 | 23 | . 1002 | 48.2 | 10.67 | 38 | 23 | . 100 | 2 | 51.1 | 13.11 |
| 39 | 24 | . 1002 | 49.7 | 10.67 | 39 | 24 | . 100 | 3 | 55.6 | 13.34 |
| 40 | 26 | . 1003 | 55.2 | 11.33 | 40 | 26 | . 150 | 3 | 61.5 | 13.56 |
| 41 | 26 | . 1003 | 55.2 | 11.33 | 41 | 26 | . 150 | 3 | 61.5 | 13.56 |
| 42 | 27 | . 1003 | 56.6 | 11.56 | 42 | 27 | . 150 | 3 | 63.0 | 13.78 |
| 43 | 27 | . 1003 | 56.6 | 11.56 | 43 | 27 | . 150 | 3 | 63.0 | 13.78 |
| 44 | 28 | . 1003 | 58.1 | 11.78 | 44 | 28 | . 150 | 3 | 64.9 | 14.00 |
| 45 | 28 | . 1003 | 58.1 | 11.78 | 45 | 28 | . 150 | 3 | 64.9 | 14.00 |
| 46 | 29 | . 1003 | 59.6 | 12.00 | 46 | 29 | . 150 | 3 | 66.5 | 14.23 |
| 47 | 27 | . 1003 | 56.6 | 11.56 | 47 | 27 | . 150 | 3 | 63.0 | 13.78 |
| 48 | 28 | . 1003 | 58.1 | 11.78 | 48 | 28 | . 150 | 3 | 64.9 | 14.00 |
| 49 | 28 | . 1003 | 58.1 | 11.78 | 49 | 28 | . 150 | 3 | 64.9 | 14.00 |
| 50 | 29 | . 1003 | 59.6 | 12.00 | 50 | 29 | . 150 | 3 | 68.0 | 14.45 |
| 51 | 29 | . 1003 | 59.6 | 12.00 | 51 | 29 | . 150 | 3 | 68.0 | 14.45 |
| 52 | 29 | 125 <br> 125 | 61.5 | 12.00 | 52 | 29 | . 150 | 3 | 68.0 | 14.45 |
| 53 | 30 | . 125 3 | 63.0 | 12.22 | 53 | 30 | . 175 | 3 | 70.0 | 14.45 |
| 54 | 29 | . 125 3 | 61.5 | 12.00 | 54 | 29 | . 175 | 3 | 68.0 | 14.45 |
| 55 | 29 | . 125 3 | 61.5 | 12.00 | 55 | 29 | . 175 | 3 | 70.0 | 14.45 |
| 56 | 30 | . 125 3 | 63.0 | 12.22 | 56 | 30 | . 175 | 3 | 71.9 | 14.67 |
| 57 | 30 | . 125 3 | 63.0 | 12.22 | 57 | 30 | . 175 | 3 | 71.9 | 14.67 |
| 58 | 30 | . 125 3 | 63.0 | 12.22 | 58 | 30 | . 175 | 3 | 71.9 | 14.67 |
| 59 | 31 | . 125 3 | 64.5 | 12.44 | 59 | 31 | . 175 | 3 | 73.4 | 14.89 |
| 60 | 31 | . 125 3 | 64.5 | 12.44 | 60 | 31 | . 175 | 3 | 73.4 | 14.89 |
| 61 | 30 | . 125 3 | 63.0 | 12.22 | 61 | 30 | . 175 | 3 | 71.9 | 14.67 |
| 62 | 31 | . 125 3 | 64.5 | 12.44 | 62 | 31 | . 175 | 3 | 73.4 | 14.89 |
| 63 | 31 | . 150 3 | 66.4 | 12.44 | 63 | 31 | . 175 | 3 | 73.4 | 14.89 |
| 64 | 31 | . 150 3 | 66.4 | 12.44 | 64 | 31 | . 175 | 3 | 73.4 | 14.89 |
| 65 | 32 | . 150 3 | 67.9 | 12.67 | 65 | 32 | . 175 | 3 | 75.0 | 15.11 |
| 66 | 32 | . 150 3 | 67.9 | 12.67 | 66 | 32 | . 175 | 3 | 75.0 | 15.11 |
| 67 | 32 | . 150 3 | 67.9 | 12.67 | 67 | 32 | . 175 | 3 | 75.0 | 15.11 |
| 68 | 32 | . 150 3 | 67.9 | 12.67 | 68 | 32 | . 175 | 3 | 75.0 | 15.11 |
| 69 | 32 | . 150 3 | 67.9 | 12.67 | 69 | 32 | . 175 | 3 | 75.0 | 15.11 |
| 70 | 32 | . 150 3 | 67.9 | 12.67 | 70 | 32 | . 175 | 3 | 75.0 | 15.11 |
| 71 | 33 | . 150 3 | 69.4 | 12.89 | 71 | 33 | . 175 | 3 | 76.6 | 15.34 |
| 72 | 33 | . 150 3 | 69.4 | 12.89 | 72 | 33 | . 175 | 3 | 76.6 | 15.34 |
| 73 | 33 | . 150 3 | 69.4 | 12.89 | 73 | 33 | . 175 | 3 | 76.6 | 15.34 |
| 74 | 33 | . 150 3 | 69.4 | 12.89 | 74 | 33 | . 175 | 3 | 76.6 | 15.34 |
| 75 | 33 | . 150 3 | 71.3 | 12.89 | 75 | 33 | . 200 | 3 | 78.7 | 15.34 |
| 76 | 34 | . 175 3 | 72.8 | 13.11 | 76 | 34 | . 200 | 3 | 80.2 | 15.56 |
| 77 | 34 | . 175 3 | 72.8 | 13.11 | 77 | 34 | . 200 | 3 | 80.2 | 15.56 |
| 78 | 34 | . 175 3 | 72.8 | 13.11 | 78 | 34 | . 200 | 3 | 80.2 | 15.56 |
| 79 | 34 | 175 .175 | 72.8 | 13.11 | 79 | 34 | . 200 | 3 | 80.2 | 15.56 |
| 80 | 34 | 175 .175 | 72.8 | 13.11 | 80 | 34 | . 200 | 3 | 80.2 | 15.56 |
| 81 | 34 | . 175 3 | 72.8 | 13.11 | 81 | 34 | . 200 | 3 | 80.2 | 15.56 |
| 82 | 35 | . 200 3.5 | 78.8 | 13.33 | 82 | 35 | . 250 | 3.5 | 88.5 | 15.78 |
| 83 | 35 | . 200 3.5 | 78.8 | 13.33 | 83 | 35 | . 250 | 3.5 | 88.5 | 15.78 |
| 84 | 35 | . 200 3.5 | 78.8 | 13.33 | 84 | 35 | . 250 | 3.5 | 88.5 | 15.78 |
| 85 | 36 | . 200 3.5 | 80.3 | 13.56 | 85 | 36 | . 250 | 3.5 | 88.5 | 15.78 |
| 86 | 36 | . 200 3.5 | 80.3 | 13.56 | 86 | 36 | . 250 | 3.5 | 88.5 | 15.78 |
| 87 | 36 | . 200 3.5 | 80.3 | 13.56 | 87 | 36 | . 250 | 3.5 | 88.5 | 15.78 |

Notes

1) For structures 1-87, invert plates are $0.100^{\prime \prime}$ thick.





Aluminum Footing Pad Option

## Scour Discussion

In most cases, using a full aluminum invert with toe plate extensions at the inlet and outlet ends will eliminate the potential for scour through the structure. If, however, it is desirable to span the stream crossing, scour should be investigated. The most efficient counter measure, as listed below, should be chosen based on site specific conditions. The chosen alternative should be designed by a competent professional experienced in the chosen field.

These counter measures include:

- Rip rap protection
- Concrete paving
- Lower footings below anticipated scour depth
- Bearing foundation on competent rock
- Undercut erodible soils and replace with nonerodible material
- Construction of guide banks including sheet piling
- Implementation of permanent erosion control mats where vegetation can be established, such as Pyramat ${ }^{\oplus}$
- Implementation of hard armor interlocking blocks where vegetation cannot be established, such as Petraflex ${ }^{\circledR}$, or Geolink ${ }^{\circledR}$, or A-Jacks ${ }^{\circledR}$

Please contact your Contech representative for more details and design guidance.


## Slotted Concrete Footing Option

*See note above


Aluminum Receiving Channel


Typical Projecting End ${ }^{(6)}$

## Notes - Installation

1. If less than $3^{\prime}$ of space is available, concrete grout may be required.
2. Backfill to be well graded granular, $\mathrm{A}-1, \mathrm{~A}-3, \mathrm{~A}-2-4$, or A-2-5, per AASHTO M145, placed in six- to eight-inch lifts symmetrically on each side compacted to minimum $90 \%$ density per AASHTO T180. D-4 dozer or smaller to operate near and above structure during backfilling to finish grade. Refer to AASHTO Sec. 26 installation specification.
3. Fill in these zones, must be placed in 8 " maximum lifts and compacted to minimum $90 \%$ density per AASHTO T180.
4. Minimum cover may need to be increased to handle temporary construction vehicle loads (larger than D4) but not to exceed maximum allowable cover for the specific box culvert design.
5. When using a full invert or footing pads, the foundation shall have a minimum of 4,000 psf bearing capacity and include a $6^{\prime \prime}$ stable well-graded granular
bed. Lower bearing capacities can be accommodated through special design or the use of concrete footings.
6. Standard headwalls shown are for vertical orientation only. Any design, other than vertical orientation, must be reviewed by the design engineer.
7. The type and extent of end treatment on the box culvert should be chosen and designed so as to prevent the loss of backfill due to high flow conditions.
8. Bolt torque requirements - plate lap must be properly mated in a tangent fashion using proper alignment techniques and adequate bolt torque to seat the corrugation. The recommended installation bolt torque for aluminum box culverts is $90-115 \mathrm{ft}$-lbs for full inverts and 115-135 ft-lbs for all other components. When seam sealant tape is used, bolts shall be installed and retightened to these torque levels after 24 hours. Torque levels are for installation, not residual, in-service requirements.
9. For assembly information, see the manufacturer's detailed assembly drawings and instructions.

## Aluminum Box Culvert Specification

## Scope

This specification covers the manufacture and installation of the aluminum box culvert structure detailed in the plans.

## Material

The aluminum box culvert shall consist of plates, ribs, and appurtenant items as shown on the plans and shall conform to the requirements of ASTM B 864 and AASHTO M219. Plate thicknesses, rib spacings, end treatment, and type of invert and foundation shall be as indicated on the plans.

Bolts and nuts shall conform to the requirements of ASTM A 307 or ASTM A 449 and shall be galvanized in accordance with ASTM A 153.

## Assembly

The box culvert shall be assembled in accordance with the shop drawings provided by the manufacturer and per the manufacturer's recommendations. Bolts shall be tightened using an applied torque of between 90 and 135 ft -lbs.

## Installation

The box culvert shall be installed in accordance with the plans and specifications, the manufacturer's recommendations and the AASHTO Standard Specification for Highway Bridges, Section 26 (Division II).

## Bedding

The bedding should be constructed to a uniform line and grade using material outlined in the backfill section. The foundation must be capable of providing a bearing capacity of at least two tons per square foot.

## Backfill

The structure shall be backfilled using clean, well graded granular material that meets the requirements of AASHTO M145 for soil classifications A-1, A-3, A-2-4, or A-2-5. Backfill must be placed symmetrically on each side of the structure in 6 -inch to 8 -inch lifts. Each lift shall be compacted to a minimum of 90 percent density per AASHTO T180.

Assembly




## SUPER-SPAN" and SUPER-PLATE ${ }^{\circledR}$

## Over 4000 SUPER-SPANS in Place

Since 1967, more than 4,000 structures have been built on five continents. That makes SUPER-SPAN the most widely accepted, long-span, corrugated steel design in the world.

SUPER-SPAN structures with individual spans up to 50 feet are serving as bridges, railroad overpasses, stream enclosures, vehicular tunnels, culverts, and conveyor conduits. Installations have involved almost every job condition possible, including severe weather and unusual construction time constraints.

## National specification

SUPER-SPAN's popularity has resulted in a national specification written for long-span, corrugated metal structures by the American Association of State Highway and Transportation Officials. AASHTO Standard Specifications (Section 12.7) for Highway Bridges provide for the selection of acceptable combinations of plate thickness, minimum cover requirements, plate radius and other design factors. Material is covered by AASHTO M 167 AND ASTM A 761. Installation is covered by AASHTO standard specification for highway bridges (Sec. 12) and ASTM A 761.

## Acceptance

Many state and federal agencies recognize the excellent performance and economy of SUPER-SPAN corrugated structures. In a 1979 memorandum, the chief of FHWA's Bridge Division noted that in the previous 15 years, several hundred Contech SUPER-SPAN Culverts had been erected in the United States and Canada and their performance had been excellent.

In a 1983 report to the Secretary of Transportation, the General Accounting Office stated, "Some innovations, such as using certain long-span culverts rather than building conventional bridges, have substantially lowered bridge costs."

## Aluminum Long-Span structures (SUPER-PLATE)

SUPER-PLATE structures add both longitudinal stiffeners (thrust beams) and circumferential stiffeners (reinforcing ribs) to conventional Aluminum Structural Plate to achieve larger sizes. Clear spans in excess of 30 feet and clear areas over 435 square feet are achievable with SUPER-PLATE.
Available shapes include low-profile and high-profile arch (as seen below) and horizontal ellipse. Consult a Contech representative for additional information.


High-profile arch SUPER-SPAN (43'-3" span, 27' rise) in Hamilton, Ohio to span a wetland and to provide a wildlife crossing.


Pear-Arch
Standard Shapes

## General design and installation characteristics

As conventional round structures increase in diameter beyond 16-18 feet, they become more difficult to install. It becomes increasingly difficult to both control the shape and to achieve good backfill support. Contech's SUPER-SPAN and SUPER-PLATE help overcome these problems through the use of both special shapes and concrete thrust beams.

## SUPER-SPAN/SUPER-PLATE solves the problem

The horizontal ellipse, low-profile and high-profile arch shapes are wide-span, reduced-rise structures. They provide large open areas with less rise than comparable circular shapes. Sidewalls are compact with a modest radius to provide a more rigid pipe wall to compact against. At the same time, the large radius top arc of these structures is flatter and, therefore, has less tendency to peak as it supports the sides (see Figure 9).


Figure 9

By contrast, Pear and Pear-Arch shapes provide relatively high-rise structures. These shapes orient their sides at the derivable angle to the soil pressures (see Figure 10). Their smaller radius crowns are typically heavy gage to provide the necessary restraint at the top.

The thrust beam is the key element to SUPER-SPAN and SUPER-PLATE success. Besides providing perfect backfill in the important area above the spring line, it acts as a floating footing for the critical large radius top arch of the structure. It fixes the end of the arch, stiffening it and reducing deflection as backfill goes over the top.

The thrust beam also provides a solid vertical surface that is easy to backfill against to obtain excellent compaction*. After installation, the beam effectively controls possible horizontal spreading of the top arch.


With the shape on the left, it is difficult to obtain adequate compaction of the backfill at the critical $3 / 4$ rise point.

Compare it to the SUPER-SPAN on the right. Excellent compaction* and a high restraining force $(R)$ is readily obtained against the vertical surface of the thrust beam. Force $(R)$ acts on the vertical surface to prevent significant horizontal movement on the pipe wall at the $3 / 4$ rise point under dead and live loads.
*See Backfilling and Backfill material on Design Details on page 85.

SUPER-SPAN and SUPER-PLATE structures, by means of their shape and thrust beams (which reduce the central angle of the effective top arch to 80 degrees) have added stability against deflection and snap-through buckling. They can be economically designed and installed within recognized AASHTO /AISI critical stresses and seam strength limits.


Figure 10


Standard Shapes

## Structural Design

| TABLE 53MINIMUM THICKNESS — MININUM COVER TABLE, FT. H-20, HS-20, H-25, HS-25 LIVE LOAD |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Wall Thickness, Inches |  |  |  |  |  |  |
| Top Radius $\mathbf{R}_{\mathbf{T}^{\prime}} \mathbf{F t} .$ | $\begin{gathered} 0.111^{\prime \prime} \\ \text { (12 Ga.) } \end{gathered}$ | $\begin{gathered} 0.140^{\prime \prime} \\ (10 \mathrm{Ga} .) \end{gathered}$ | $0.170^{\prime \prime}$ or $0.188^{\prime \prime}$ ( 8 or 7 Ga.) | $0.218^{\prime \prime}$ <br> (5 Ga.) | $\begin{aligned} & 0.249^{\prime \prime} \\ & \text { (3 Ga.) } \end{aligned}$ | $\begin{aligned} & 0.280^{\prime \prime} \\ & \text { (1 Ga.) } \end{aligned}$ |
| 15' | 2.5' | $2.5{ }^{\prime}$ | $2.5{ }^{\prime}$ | $2.0{ }^{\prime}$ | $2.0{ }^{\prime}$ | $2.0{ }^{\prime}$ |
| 15'-17' |  | $3.0{ }^{\prime}$ | $3.0{ }^{\prime}$ | $2.5{ }^{\prime}$ | $2.0^{\prime}$ | $2.0{ }^{\prime}$ |
| $17^{\prime}-20^{\prime}$ |  |  | $3.0{ }^{\prime}$ | $2.5{ }^{\prime}$ | $2.5{ }^{\prime}$ | $2.5{ }^{\prime}$ |
| 20'-23' |  |  |  | $3.0{ }^{\prime}$ | $3.0{ }^{\prime}$ | $3.0{ }^{\prime}$ |
| 23'-25' |  |  |  |  | $4.0{ }^{\prime}$ | $4.0{ }^{\prime}$ |

## Notes

1. Designs listed are for steel $6^{\prime \prime} \times 2^{\prime \prime}$ corrugation only. For aluminum $9^{\prime \prime} \times 2^{1 /} 2^{\prime \prime}$ corrugation design, please contact your local Contech representative.
2. Heights of cover for highway live loads given are to top of concrete pavement or bottom of flexible pavement.
3. Minimum covers for E 80 live loads are approximately twice those for HS 20. However, E 80 minimums must be established for individual applications.
4. Minimum covers for construction loads and similar heavy wheel loads must be established for individual applications.
5. The table assumes a granular backfill over the crown of the structure to the full minimum cover depth (height) compacted to not less than 90 percent AASHTO T180 density.
6. Call a Contech representative for Pear and Pear-Arch shape gages.

A SUPER-SPAN or SUPER-PLATE structure is essentially an engineering combination of steel and soil. Maximum fill heights are calculated on the basis of AASHTO/AISI design methods using top radius to calculate ring compression (thrust= pressure $\times R_{\mathrm{T}}$ ) with allowable wall stress of 16,500 psi. In the design method, AISI requires a seam strength safety factor of two, while AASHTO requires a seam strength safety factor of three.

In accordance with AASHTO, buckling and flexibility factors are not calculated. These factors are covered by the minimum thickness/minimum cover table on this page and special geometry limitations spelled out by AASHTO.

## Shallow fill

Minimum designs are shown in Table 53. Ordinarily, shallow cover structures will be at the minimum (shown in the tables) thickness required for installation and to prevent against buckling. Wall stresses can be checked in deep cover applications by adding the soil load to the appropriate live load.

When adding the total live load over the structure, it is necessary to distribute it over an appropriate area of the structure which varies with the fill height.

## Special designs

Structure sizes shown in Tables 54 through 60 are standard shapes. Intermediate or larger sizes are available. These special sizes also are designed in accordance with the AASHTO design method.

Minimum covers shown in Table 53 are based on standard construction. Somewhat lower covers are possible with special measures such as using concrete relieving slabs. Special designs are also available for fill heights exceeding
the normal limitations of standard structures. Your Contech representative can provide information on special requirements.

## Foundation

The foundation under the structure and sidefill zones must be evaluated by the design engineer to ensure adequate bearing capacity. Differential settlement between the structure and side fill must be minimal.

## Hydraulic design

The most commonly used SUPER-SPAN and SUPER-PLATE hydraulic shapes are the horizontal ellipse, the low-profile arch, and the high-profile arch. Hydraulic data for these shapes are presented in tabular and graphical form in the current edition of the NCSPA CSP Design Manual. Standard procedures are presented in the Hydraulics chapter of the handbook to determine the headwater depth required for a given flow through these structures under both inlet and outlet control conditions.

In addition, the hydraulic design series of publications from FHWA offers guidance regarding hydraulic capacity of these structures.

## Installation precautions

During the installation and prior to the construction of permanent erosion control and end-treatment protection, special precautions may be necessary. The structure must be protected from unbalanced loads and from any structural loads or hydraulic forces that might bend or distort the unsupported ends of the structure. Erosion wash out of previously placed soil support must be prevented to ensure that the structure maintains its load capacity.

Contech SUPER-SPAN structures have proven both practical and economical to construct in a wide range of applications and conditions. Nevertheless, there are basic rules of installation that must be obeyed to ensure acceptable performance.

Comprehensive installation and inspection standards are furnished with every SUPER-SPAN purchase. These documents should be studied thoroughly by the contractor and engineer. The following material highlights the key elements involved in the proper construction of a Contech SUPER-SPAN.

## Excavation, foundation and bedding

There must be adequate distance between the SUPER-SPAN and questionable native soils. Bedding must be preshaped for structures with inverts. A loose soil cushion should be provided for the bottom plates. Base channels for arches must be square to the centerline on arch structures.

## Erection

Plates can be placed either one at a time or in preassembled units of two or more plates in a ring.

All bolts in a newly hung plate or assembly should be tightened before adding the next unit above it. This should be done only with the plates in proper relation to each other for correct curvature and alignment in the structure. It may be necessary to use cables, props, or jigs to keep the plates in position during tightening.

The structure cross-section must be checked regularly during assembly. Its shape must be symmetrical, with the plates forming smooth, continuous curves. Longitudinal seams should be tight and plate ends should be parallel to each other.

## Backfilling

SUPER-SPANs are flexible structures, therefore care is required during the placement and compaction of backfill. An effective system to monitor the structure during the backfilling process must be established.

Select an approved structure backfill material for the zone around the SUPER-SPAN. Establish soil density curves and determine proper frequencies and procedures for testing. The equipment used to place and compact fill around and over the structure should be selected based on the quality of the backfill and the shape of the SUPER-SPAN. Such plans should be verified in the initial backfilling stages.

Use only backfilling methods and equipment that obtain specified density without excessive movement or deformation of the structure.

## Backfill material

Contech's specification for backfill material contains the following as listed in the AASHTO Bridge Specification:

1. Granular type soils shall be used as structure backfill (the envelope next to the metal structure). Well-graded sand and gravel that is sharp, rough, and angular is preferred.
Approved stabilized soil shall be used only under direct supervision of a competent, experienced soils engineer. Plastic or cohesive soils should not be used.
2. The structure backfill material shall conform to one of the following soil classifications from AASHTO Specification M145, Table 2; for height of fill less than 12 feet, A-1, A-2-4 and A-2-5; for height of fill of 12 feet and more and all pear or pear-arch structures, A-1. Structure backfill shall be placed and compacted to not less than 90 percent density, per AASHTO T 180.
3. The extent of the select structural backfill outside the maximum span is dependent on the quality of the adjacent embankment, loading and shape of the structure. It may be necessary to excavate native soil at the sides to provide an adequate width needed for compaction. For ordinary installations with a good quality, well-compacted embankment or in situ soil adjacent to the structure backfill, a minimum width of structural backfill six feet beyond the structure is usually required. The engineer must evaluate the in situ conditions to ensure adequate bearing capacity. The structure backfill shall extend to the minimum cover elevation (Table 53-page 83) above the structure.

## Monitoring Backfill

Regular monitoring is required during backfilling to ensure a structure with a proper shape and that compaction levels are achieved. A Contech technician will confirm the structure's shape before backfilling, then monitor the shape and verify compaction readings until the backfill reaches the minimum cover level.

## Special requirements

Very large or high structures sometimes call for additional special provisions for shape control during backfilling.

The minimum stiffness requirements for some structures shown in Table 53 on Page 83 may need to be augmented by increased design stiffness or mandatory top loading. Top loading requires the placement of a modest blanket of soil on the crown when backfill is approximately at the springline height.

## Conceptual drawings'



Note:

1. Many of the details shown are conceptual. The designer should work with the Contech representative on each particular application.

| TABLE 54. TYPICAL LOW PROFILE ARCH SHAPES (ALL DIMENSIONS TO INSIDE CRESTS) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Structure <br> Number | Maximum Span | Bottom Span | Total Rise | Top <br> Rise | Top Radius $\mathbf{R}_{\mathrm{T}}$ | Side Radius $R_{s}$ | Angle Below Horizontal $\Delta$ | Approx. Area (Sq. Ft.) | Shape <br> Factor $\mathbf{R}_{\mathrm{T}} / \mathbf{R}_{\mathrm{s}}$ |
| 69 Al 5 | 19'-5" | 19'-2" | 6'-9" | 5'-10" | 13'-1" | $3^{\prime}-7{ }^{\prime \prime}$ | $15^{\circ}-36^{\prime}$ | 105 | 3.60 |
| 69A18 | 20'-1" | 19'-10" | 7'-6" | $6^{\prime}-6^{\prime \prime}$ | 13'-1" | $4^{\prime}-6^{\prime \prime}$ | $12^{\circ}-28^{\prime}$ | 120 | 2.91 |
| 75A18 | 21'-6" | $21^{\prime}-4{ }^{\prime \prime}$ | 7'-9" | $6^{\prime}-9^{\prime \prime}$ | $14^{\prime}-3^{\prime \prime}$ | $4^{\prime}-6^{\prime \prime}$ | $12^{\circ}-28^{\prime}$ | 133 | 3.13 |
| 78A18 | 22'-3" | 22'-1" | 7'11' | $6^{\prime}-11^{\prime \prime}$ | 14'-10" | $4^{\prime}-6^{\prime \prime}$ | $12^{\circ}-28^{\prime}$ | 140 | 3.25 |
| 81A18 | $23^{\prime}-0^{\prime \prime}$ | 22'-9" | 8'-1" | 7'-1' | 15'-5" | $4^{\prime}-6^{\prime \prime}$ | $12^{\circ}-28^{\prime}$ | 147 | 3.38 |
| 84A18 | 23'-9" | $23^{\prime}-6^{\prime \prime}$ | $8^{\prime}-2^{\prime \prime}$ | $7^{\prime}-2 \prime$ | $16^{\prime}-0^{\prime \prime}$ | $4^{\prime}-6^{\prime \prime}$ | $12^{\circ}-28^{\prime}$ | 154 | 3.50 |
| 87A18 | $24^{\prime}-6^{\prime \prime}$ | $24^{\prime}-3^{\prime \prime}$ | $8^{\prime}-3^{\prime \prime}$ | $7^{\prime}-4^{\prime \prime}$ | 16'-6" | $4^{\prime}-6^{\prime \prime}$ | $12^{\circ}-28^{\prime}$ | 161 | 3.63 |
| 90A18 | 25'-2" | $25^{\prime}-0^{\prime \prime}$ | $8^{\prime}-5^{\prime \prime}$ | $7^{\prime}-5^{\prime \prime}$ | 17'-1" | $4^{\prime}-6^{\prime \prime}$ | $12^{\circ}-28^{\prime}$ | 168 | 3.75 |
| $93 \mathrm{Al8}$ | 25'-11" | 25'-9" | 8'-7" | $7{ }^{\prime}-7{ }^{\prime \prime}$ | 17'-8" | $4^{\prime}-6^{\prime \prime}$ | $12^{\circ}-28^{\prime}$ | 176 | 3.88 |
| 93A24 | 27'-3" | 27'-1' | $10^{\prime}-0^{\prime \prime}$ | $9^{\prime}-0^{\prime \prime}$ | $17^{\prime}-8 \prime \prime$ | $6^{\prime}-4^{\prime \prime}$ | $8^{\circ}-55^{\prime}$ | 217 | 2.77 |
| 99A2 1 | 28'-1" | 27'-11" | 9'-6" | 8'-7" | $18^{\prime} 10^{\prime \prime}$ | $5^{\prime}-5^{\prime \prime}$ | $10^{\circ}-24^{\prime}$ | 212 | 3.48 |
| 99A24 | 28'-9" | 28'-7" | $10^{\prime}-3^{\prime \prime}$ | $9^{\prime}-3^{\prime \prime}$ | 18'-10" | $6^{\prime}-4 \prime$ | $8^{\circ}-55^{\prime}$ | 234 | 2.95 |
| 102A21 | 28'-10" | 28'-8" | $9^{\prime}-8$ " | 8'-8" | 19'-5" | $5^{\prime}-5^{\prime \prime}$ | $10^{\circ}-24^{\prime}$ | 220 | 3.54 |
| 108A21 | $30^{\prime}-3^{\prime \prime}$ | 30'-1" | 9'-11" | 8'-11" | 20'-7" | $5^{\prime}-5^{\prime \prime}$ | $10^{\circ}-24^{\prime}$ | 237 | 3.76 |
| 108A24 | $30^{\prime}-1{ }^{\prime \prime}$ | $30^{\prime}-9^{\prime \prime}$ | 10'-8" | $9^{\prime}-8^{\prime \prime}$ | $20^{\prime}-7{ }^{\prime \prime}$ | $6^{\prime}-4^{\prime \prime}$ | $8^{\circ}-55^{\prime}$ | 261 | 3.22 |
| 108A30 | $31^{\prime}-7{ }^{\prime \prime}$ | 31'-2" | 12'-1" | $10^{\prime}-4 \prime$ | 20'-7" | 7'-3" | $14^{\circ}-03^{\prime}$ | 309 | 2.82 |
| 111A21 | $31^{\prime}-0^{\prime \prime}$ | $30^{\prime} 10^{\prime \prime}$ | 10'-1" | $9^{\prime \prime}-1$ " | 21'-1" | $5^{\prime}-5^{\prime \prime}$ | $10^{\circ}-24^{\prime}$ | 246 | 3.85 |
| 111 A 30 | 32'-4" | 31'-11' | 12'-3" | 10'-6" | 21'-1" | $7^{\prime}-3^{\prime \prime}$ | $14^{\circ}-03^{\prime}$ | 319 | 2.89 |
| 114A21 | 31'-9" | $31^{\prime}-7{ }^{\prime \prime}$ | 10'-2" | $9^{\prime}-3^{\prime \prime}$ | 21'-8" | $5^{\prime}-5^{\prime \prime}$ | $10^{\circ}-24^{\prime}$ | 255 | 3.96 |
| 114A30 | 33'-1" | 32'-7" | 12'-5" | $10^{\prime}-8^{\prime \prime}$ | 21'-8" | $7^{\prime}-3^{\prime \prime}$ | $14^{\circ}-03^{\prime}$ | 330 | 2.97 |
| 117A24 | $33^{\prime}-2^{\prime \prime}$ | $33^{\prime}-0^{\prime \prime}$ | 11'-1" | 10'-1" | 22'-3" | $6^{\prime}-4 \prime$ | $8^{\circ}-55^{\prime}$ | 289 | 3.49 |
| 117A33 | $34^{\prime}-5^{\prime \prime}$ | $34^{\prime}-1{ }^{\prime \prime}$ | 13'-3" | 11'-6" | $22^{\prime}-3^{\prime \prime}$ | $8^{\prime}-2^{\prime \prime}$ | $12^{\circ}-29^{\prime}$ | 367 | 2.71 |
| 123A24 | $34^{\prime}-7^{\prime \prime}$ | $34^{\prime}-6^{\prime \prime}$ | 11'-4" | $10^{\prime}-4^{\prime \prime}$ | 23'-5" | $6^{\prime}-4^{\prime \prime}$ | $8^{\circ}-55^{\prime}$ | 308 | 3.67 |
| $123 A 42$ | 37'-11" | 37'-7" | 15'-7" | 13'-10" | 23'-5" | 10'-11" | $9^{\circ}-22^{\prime}$ | 477 | 2.14 |
| 126A24 | $35^{\prime}-4^{\prime \prime}$ | 35'-2" | 11'-5" | 10'-6" | $24^{\prime}-0^{\prime \prime}$ | $6^{\prime}-4^{\prime \prime}$ | $8^{\circ}-55^{\prime}$ | 318 | 3.76 |
| $126 A 42$ | 38'-8" | 38'-4" | 15'-9" | $14^{\prime}-0^{\prime \prime}$ | $24^{\prime}-0^{\prime \prime}$ | 10'-11' | $9^{\circ}-22^{\prime}$ | 490 | 2.28 |
| 129 A 30 | 37'-10" | 37'-9" | 12'-11" | $12^{\prime}-5^{\prime \prime}$ | $24^{\prime}-7^{\prime \prime}$ | $8^{\prime}-9^{\prime \prime}$ | $3^{\circ}-10^{\prime}$ | 383 | 2.81 |
| 129A36 | $39^{\prime}-4^{\prime \prime}$ | 39'-4" | 14'-4" | $14^{\prime}-1{ }^{\prime \prime}$ | $24^{\prime}-7^{\prime \prime}$ | 10'-10" | $1^{\circ}-25^{\prime}$ | 441 | 2.27 |
| *138A30 | *39'-8" | 39'-7" | 13'-5" | 12'-6" | $26^{\prime}-3^{\prime \prime}$ | $8^{\prime}-3^{\prime \prime}$ | $6^{\circ}-22^{\prime}$ | 417 | 3.18 |
| *138A39 | * 42 '-3" | $42^{\prime}-3^{\prime \prime}$ | $15^{\prime}-5^{\prime \prime}$ | $15^{\prime}-3^{\prime \prime}$ | $26^{\prime}-3^{\prime \prime}$ | 11'-11" | $0^{\circ}-36^{\prime}$ | 510 | 2.20 |
| *144A51 | * $45{ }^{\prime}-0^{\prime \prime}$ | 44'-9" | $18^{\prime}-8^{\prime \prime}$ | 16'-11' | 27'-5" | $13^{\prime}-8^{\prime \prime}$ | $7^{\circ}-30^{\prime}$ | 675 | 2.00 |

## Notes:

Other sizes are available for special designs.

* Structures require ring beams on the crown plates per AASHTO Section 12


| TABLE 55. SPECIAL LOW-RISE SHAPES ${ }^{1}$ (ALL DIMENSIONS TO INSIDE CRESTS) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Structure Number | Maximum Span | Bottom Span | Total Rise | Top Rise | Top Radius $R_{T}$ | Side Radius $\mathbf{R}_{\mathrm{s}}$ | Angle Below Horizontal | Approx. Area (Sq. Ft.) | Shape Factor $\mathbf{R}_{\mathrm{T}} / \mathbf{R}_{\mathrm{s}}$ |
| 69A15-NS | $20^{\prime}-8{ }^{\prime \prime}$ | $20^{\prime}-8{ }^{\prime \prime}$ | $6^{\prime}-3^{\prime \prime}$ | 6'-1.5" | 14'-10" | $4^{\prime}-2^{\prime \prime}$ | $1^{\circ}-56{ }^{\prime}$ | 101 | 3.56 |
| 78A15-NS | 22'-8" | $22^{\prime}-8^{\prime \prime}$ | $6^{\prime}-8{ }^{\prime \prime}$ | $6^{\prime}-3.5 \prime \prime$ | $16^{\prime}-8^{\prime \prime}$ | $3^{\prime}-11^{\prime \prime}$ | $5^{\circ}-43^{\prime}$ | 119 | 4.26 |
| 84A15-NS | $24^{\prime}-5^{\prime \prime}$ | $24^{\prime}-5^{\prime \prime}$ | $6^{\prime}-11^{\prime \prime}$ | 6'-9" | 18'-0" | $4^{\prime}-2^{\prime \prime}$ | $2^{\circ}-05^{\prime}$ | 130 | 4.32 |
| 87A15-S | 24'-6" | $24^{\prime}-6^{\prime \prime}$ | 7'-6" | 7'-4.5" | 16'-6" | $4^{\prime}-7{ }^{\prime \prime}$ | $1^{\circ}-32^{\prime}$ | 142 | 3.61 |
| 93A15-S | $26^{\prime}-0^{\prime \prime}$ | $26^{\prime}-0^{\prime \prime}$ | 7'-9" | 7'-7.5" | $17^{\prime}-8^{\prime \prime}$ | $4^{\prime}-7{ }^{\prime \prime}$ | $1^{\circ}-32^{\prime}$ | 155 | 3.86 |
| 99A15-S | $27^{\prime}-6^{\prime \prime}$ | $27^{\prime}-6 \prime \prime$ | $8^{\prime}-0^{\prime \prime}$ | 7'11" | 18'-10" | $4^{\prime}-7{ }^{\prime \prime}$ | $1^{\circ}-32^{\prime}$ | 169 | 4.11 |
| 108A15-S | 29'-9" | 29'-9" | 8'-5" | $8^{\prime}-4 \prime$ | 20'-7" | $4^{\prime}-8^{\prime \prime}$ | $0^{\circ}-38^{\prime}$ | 191 | 4.40 |
| 105A21-NS | 30'-9" | 30'-9" | $9{ }^{\prime}-1$ " | 8'-7" | 22'-9" | $5^{\prime}-5^{\prime \prime}$ | $5^{\circ}-32^{\prime}$ | 220 | 4.20 |
| 111A18-S | 31'-1" | 31'-1" | 9'-3" | $9^{\prime}-1.5^{\prime \prime}$ | 21'-1" | $5^{\prime}-6^{\prime \prime}$ | $1^{\circ}-17^{\prime}$ | 221 | 3.84 |
| 117A18-S | 32'-7" | $32^{\prime}-7{ }^{\prime \prime}$ | $9^{\prime}-7{ }^{\prime \prime}$ | 9'-5" | 22'-3" | $5^{\prime}-6^{\prime \prime}$ | $1^{\circ}-17^{\prime}$ | 238 | 4.05 |
| 123A18-S | $34^{\prime}-0^{\prime \prime}$ | $34^{\prime}-0^{\prime \prime}$ | 9'-10" | $9^{\prime}-8 \prime \prime$ | 23'-5" | $5^{\prime}-6^{\prime \prime}$ | $1^{\circ}-17^{\prime}$ | 255 | 4.26 |
| 129A18-S | 35'-7" | 35'-7" | 10'-1" | $10^{\prime}-0^{\prime \prime}$ | $24^{\prime}-7{ }^{\prime \prime}$ | 5'-7" | $0^{\circ}-32^{\prime}$ | 273 | 4.40 |
| 129A21S | $36^{\prime}-2^{\prime \prime}$ | $36^{\prime}-2^{\prime \prime}$ | 10'-9' ${ }^{\prime \prime}$ | 10'-8" | 24'-7" | $6^{\prime}-5^{\prime \prime}$ | $1^{\circ}-07^{\prime}$ | 299 | 3.83 |

'Due to their high shape factor, cover heights are generally limited to 8' or less. Backfill material typically must meet AASHTO M145 requirements for A- 1 materials or consist of cementitious grout, CLSM, or cement stabilized sand. Other backfill materials may be acceptable, depending upon the structure selected and the actual cover height.

Notes:
Other sizes are available for special designs.


| TABLE 56. TYPICAL HIGH PROFILE ARCH SHAPES (ALL DIMENSIONS TO INSIDE CRESTS) |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Structure <br> Number | Maximum Span | Bottom Span | Total Rise | Top Rise | Top Radius $\mathbf{R}_{\mathrm{T}}$ | Upper Side Radius $\mathbf{R}_{\mathrm{c}}$ | Lower Side Radius $R_{s}$ | Angle Below Horizontal $\Delta$ | Approx. Area (Sq. Ft.) | Shape <br> Factor $\mathbf{R}_{\mathrm{T}} / \mathbf{R}_{\mathrm{C}}$ |
| 69A15-9 | 20'-1" | 19'-7" | 9'-1" | 6'-6" | 13'-1" | $4^{\prime}-6^{\prime \prime}$ | 13'1" | $11^{\circ}-18^{\prime}$ | 152 | 2.91 |
| 69A18-18 | 20'8" | 18'-10" | 12'-1" | $7^{\prime}-3^{\prime \prime}$ | 13'-1" | $5^{\prime}-5^{\prime \prime}$ | 13'1" | $21^{\circ}-44^{\prime}$ | 214 | 2.40 |
| 75A15-18 | 21'-6" | 19'-10" | 11'-8" | $6^{\prime}-9^{\prime \prime}$ | $14^{\prime}-3^{\prime \prime}$ | $4^{\prime}-6^{\prime \prime}$ | $14^{\prime}-3^{\prime \prime}$ | $20^{\circ}-0^{\prime}$ | 215 | 3.13 |
| 75A21-24 | 22'-10" | $19^{\prime} 10^{\prime \prime}$ | $14^{\prime}-6{ }^{\prime \prime}$ | $8^{\prime}-2^{\prime \prime}$ | $14^{\prime}-3^{\prime \prime}$ | $6^{\prime}-4 \prime \prime$ | $14^{\prime}-3^{\prime \prime}$ | $26^{\circ}-24^{\prime}$ | 284 | 2.24 |
| 78A15-18 | $22^{\prime}-3^{\prime \prime}$ | 20'-7" | 11'-10" | $6^{\prime}-11^{\prime \prime}$ | 14'-10" | $4^{\prime}-6^{\prime \prime}$ | 14' $10^{\prime \prime}$ | $19^{\circ}-13^{\prime}$ | 224 | 3.25 |
| 78A18-15 | 22'-11" | 21'-9" | 11'-9" | $7^{\prime}-8{ }^{\prime \prime}$ | 14'-10" | $5^{\prime}-5^{\prime \prime}$ | 14' $-10^{\prime \prime}$ | $16^{\circ}-.09^{\prime}$ | 228 | 2.73 |
| 78A18-24 | 22'-11" | 20'-1" | $14^{\prime}-0^{\prime \prime}$ | 7'-7" | 14'-10" | $5^{\prime}-5^{\prime \prime}$ | 14'-10" | $25^{\circ}-23^{\prime}$ | 275 | 2.71 |
| 81A15-18 | $23^{\prime}-0^{\prime \prime}$ | 21'-5" | 11'-11" | 7'-1" | $15^{\prime}-5^{\prime \prime}$ | $4^{\prime}-6^{\prime \prime}$ | $15^{\prime}-5^{\prime \prime}$ | $18^{\circ}-31^{\prime}$ | 234 | 3.38 |
| 81A18-15 | $23^{\prime}-8^{\prime \prime}$ | 22'-6" | 11'-10" | 7'-9" | $15^{\prime}-5^{\prime \prime}$ | $5^{\prime}-5^{\prime \prime}$ | $15^{\prime}-5^{\prime \prime}$ | $15^{\circ}-33^{\prime}$ | 238 | 2.84 |
| 81A21-24 | $24^{\prime}-4^{\prime \prime}$ | 21'-7" | 14'-10" | 8'-5" | $15^{\prime}-5^{\prime \prime}$ | $6^{\prime}-4^{\prime \prime}$ | $15^{\prime}-5^{\prime \prime}$ | $24^{\circ}-26^{\prime}$ | 309 | 2.41 |
| 84A15-18 | 23'-9" | 22'-2" | 12'-1" | 7'-2" | $16^{\prime}-0^{\prime \prime}$ | $4^{\prime}-6^{\prime \prime}$ | $16^{\prime}-0^{\prime \prime}$ | $17^{\circ}-51^{\prime}$ | 244 | 3.50 |
| 84A18-15 | $24^{\prime}-5^{\prime \prime}$ | 23'-4" | 12'-0" | 7'-11' | $16^{\prime}-0^{\prime \prime}$ | $5^{\prime}-5^{\prime \prime}$ | $16^{\prime}-0^{\prime \prime}$ | $14^{\circ}-57^{\prime}$ | 248 | 2.95 |
| 87A15-24 | 24'-6" | 21'-11" | 13'-9" | 7'-4" | 16'-6" | $4^{\prime}-6^{\prime \prime}$ | $16^{\prime}-6^{\prime \prime}$ | $22^{\circ}-45^{\prime}$ | 288 | 3.63 |
| 87A21-15 | 25'-9" | 24'-9" | 12'-10" | 8'-9" | $16^{\prime}-6^{\prime \prime}$ | $6^{\prime}-4 \prime \prime$ | $16^{\prime}-6^{\prime \prime}$ | $14^{\circ}-29^{\prime}$ | 280 | 2.61 |
| 87A21-24 | 25'-9" | 23'-2" | 15'-1" | 8'-9" | $16^{\prime}-6^{\prime \prime}$ | $6^{\prime}-4 \prime$ | $16^{\prime}-6^{\prime \prime}$ | $22^{\circ}-45^{\prime}$ | 334 | 2.59 |
| 90A15-21 | 25'-2" | 23'-3" | 13'1" | 7'-5" | 17'-1" | $4^{\prime}-6^{\prime \prime}$ | 17'-1" | $19^{\circ}-20^{\prime}$ | 283 | 3.75 |
| 90A21-15 | $26^{\prime}-6^{\prime \prime}$ | 25'-6" | $13^{\prime}-0^{\prime \prime}$ | $8^{\prime}-10^{\prime \prime}$ | 17'-1" | $6^{\prime}-4 \prime \prime$ | 17'-1" | $13^{\circ}-59^{\prime}$ | 290 | 2.70 |
| 90A21-24 | 26'-6" | $24^{\prime}-0^{\prime \prime}$ | 15'-3" | 8'-10" | 17'-1" | $6^{\prime}-4 \prime$ | 17'-1" | $22^{\circ}-0^{\prime}$ | 347 | 2.68 |
| 93A15-21 | 25'-11" | 24'-1" | $13^{\prime}-3^{\prime \prime}$ | 7'-7" | $17^{\prime}-8{ }^{\prime \prime}$ | $4^{\prime}-6^{\prime \prime}$ | $17^{\prime}-8^{\prime \prime}$ | $18^{\circ}-42^{\prime}$ | 294 | 3.88 |
| 93A21-15 | 27'-3" | $26^{\prime}-3^{\prime \prime}$ | $13^{\prime}-2^{\prime \prime}$ | $9^{\prime}-0^{\prime \prime}$ | $17^{\prime}-8{ }^{\prime \prime}$ | $6^{\prime}-4^{\prime \prime}$ | $17^{\prime}-8{ }^{\prime \prime}$ | $13^{\circ}-32^{\prime}$ | 301 | 2.79 |
| 93A21-24 | $27^{\prime}-3^{\prime \prime}$ | $24^{\prime}-10^{\prime \prime}$ | $15^{\prime}-5^{\prime \prime}$ | $9^{\prime}-0^{\prime \prime}$ | $17^{\prime}-8^{\prime \prime}$ | $6^{\prime}-4^{\prime \prime}$ | $17^{\prime}-8^{\prime \prime}$ | $21^{\circ}-17^{\prime}$ | 360 | 2.77 |
| 99A15-21 | 27'-5" | $25^{\prime}-8^{\prime \prime}$ | 13'-6" | $7^{\prime}-10^{\prime \prime}$ | 18'-10" | $4^{\prime}-6^{\prime \prime}$ | 18'-10" | $17^{\circ}-34^{\prime}$ | 317 | 4.13 |
| 99A21-15 | 28'-9" | 27'-10" | $13^{\prime}-5^{\prime \prime}$ | $9{ }^{\prime}-3^{\prime \prime}$ | 18'-10" | $6^{\prime}-4^{\prime \prime}$ | 18'-10" | $12^{\circ}-43^{\prime}$ | 323 | 2.97 |
| 99A24-24 | 29'-5" | 27'-1" | $16^{\prime}-5^{\prime \prime}$ | 9'-11' | 18'-10" | $7^{\prime}-3^{\prime \prime}$ | 18'-10" | $20^{\circ}-0^{\prime}$ | 412 | 2.58 |

Notes:
Other sizes are available for special designs.


| TABLE 57. TYPICAL HIGH PROFILE ARCH SHAPES (ALL DIMENSIONS TO INSIDE CRESTS) |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Structure Number | Maximum Span | Bottom Span | Total Rise | Top <br> Rise | Top Radius $\mathbf{R}_{\mathrm{T}}$ | Upper Side Radius $\mathbf{R}_{\mathrm{c}}$ | Lower Side Radius $\mathbf{R}_{\mathrm{s}}$ | Angle Below Horizontal | Approx. Area (Sq. Ft.) $\Delta$ | Shape <br> Factor $\mathbf{R}_{\mathrm{T}} / \mathbf{R}_{\mathrm{C}}$ |
| 102A15-24 | 28'-2" | 25'-11' | 14'-5" | $8^{\prime}-0^{\prime \prime}$ | 19'-5" | $4^{\prime}-6$ " | 19'-5" | $19^{\circ}-24^{\prime}$ | 348 | 4.25 |
| 102A24-15 | 30'-1" | 29'-3" | $14^{\prime}-3^{\prime \prime}$ | 10'-1" | 19'-5" | $7^{\prime}-3^{\prime \prime}$ | 19'-5" | $12^{\circ}-21^{\prime}$ | 360 | 2.68 |
| 102A24-30 | 30'-1" | 26'-9" | 18'-0" | 10'-1" | 19'-5" | $7^{\prime}-3^{\prime \prime}$ | $19^{\prime}-5^{\prime \prime}$ | $24^{\circ}-07^{\prime}$ | 466 | 2.66 |
| 108A18-24 | $30^{\prime}-3^{\prime \prime}$ | 28'-2" | 15'-5" | 8'-11" | 20'-7" | 5'-5" | 20'-7" | $18^{\circ}-20^{\prime}$ | 399 | 3.75 |
| 108A24-18 | 31'-7" | 30'-5" | $15^{\prime}-3^{\prime \prime}$ | 10'-4" | 20'-7" | 7'-3" | 20'-7" | $13^{\circ}-51^{\prime}$ | 408 | 2.83 |
| 108A24-30 | 31'-7" | 28'-5" | 18'-4" | 10'-4" | 20'-7" | $7^{\prime}-3^{\prime \prime}$ | 20'-7" | $22^{\circ}-46^{\prime}$ | 496 | 2.82 |
| 111A18-24 | $31^{\prime}-0^{\prime \prime}$ | $29^{\prime}-0^{\prime \prime}$ | 15'-7" | 9'-1" | 21'-1" | $5^{\prime}-5^{\prime \prime}$ | 21'-1" | $17^{\circ}-50^{\prime}$ | 412 | 3.85 |
| 111A21-30 | $31^{\prime}-8^{\prime \prime}$ | 28'-7" | 17'-9" | $9^{\prime}-10^{\prime \prime}$ | 21'-1" | $6^{\prime}-4^{\prime \prime}$ | 21'-1" | $22^{\circ}-09^{\prime}$ | 483 | 3.31 |
| 111A24-18 | $32^{\prime}-4^{\prime \prime}$ | $31^{\prime}-2^{\prime \prime}$ | 15'-5" | 10'-6" | 21'-1" | $7^{\prime}-3^{\prime \prime}$ | 21'-1" | $13^{\circ}-31^{\prime}$ | 420 | 2.91 |
| $\dagger 111$ 24-36 | 32'-4" | 27'-11' | 19'-11" | 10'-6" | 21'-1" | $7^{\prime}-3^{\prime \prime}$ | 21'-1" | $26^{\circ}-29^{\prime}$ | 553 | 2.89 |
| 114A18-30 | 31'-9" | 28'-8" | 17'-2" | $9^{\prime}-3^{\prime \prime}$ | 21'-8" | $5^{\prime}-5^{\prime \prime}$ | 21'-8" | $21^{\circ}-34^{\prime}$ | 469 | 3.96 |
| 114A30-18 | $34^{\prime}-4^{\prime \prime}$ | $33^{\prime}-3^{\prime \prime}$ | $17^{\prime}-0^{\prime \prime}$ | $12^{\prime}-0^{\prime \prime}$ | 21'-8" | 9'-1" | 21'-8" | $13^{\circ}-09^{\prime}$ | 490 | 2.39 |
| $\dagger 114 \mathrm{~A} 24-36$ | 33'-1" | 28'-9" | 20'-1" | 10'-8" | 21'-8" | $7^{\prime}-3^{\prime \prime}$ | 21'-8" | $25^{\circ}-47^{\prime}$ | 570 | 2.97 |
| 117A18-30 | 32'-6" | 29'-6" | 17'-4" | $9^{\prime}-4^{\prime \prime}$ | 22'-3" | $5^{\prime}-5^{\prime \prime}$ | $22^{\prime}-3^{\prime \prime}$ | $21^{\circ}-01^{\prime}$ | 484 | 4.06 |
| 117A30-18 | 35'-1" | $34^{\prime}-0^{\prime \prime}$ | 17'-1" | 12'-2" | 22'-3" | 9'-1" | $22^{\prime}-3^{\prime \prime}$ | $12^{\circ}-49^{\prime}$ | 504 | 2.45 |
| $\dagger 117 A 24-36$ | 33'-10" | 29'-7" | $20^{\prime}-3^{\prime \prime}$ | 10'-9" | 22'-3" | $7^{\prime}-3^{\prime \prime}$ | $22^{\prime}-3^{\prime \prime}$ | $25^{\circ}-07^{\prime}$ | 587 | 3.05 |
| 123A18-30 | $34^{\prime}-0^{\prime \prime}$ | $31^{\prime}-2^{\prime \prime}$ | 17'-8" | $9^{\prime}-8 \prime \prime$ | 23'-5" | $5^{\prime}-5^{\prime \prime}$ | $23^{\prime}-5^{\prime \prime}$ | $20^{\circ}-0^{\prime}$ | 513 | 4.27 |
| 123A30-18 | $36^{\prime}-7{ }^{\prime \prime}$ | 35'-6" | $17^{\prime}-4^{\prime \prime}$ | 12'-5" | 23'-5" | 9'-1" | $23^{\prime}-5^{\prime \prime}$ | $12^{\circ}-11^{\prime}$ | 533 | 2.58 |
| $\dagger$ 123A21-36 | $34^{\prime}-7^{\prime \prime}$ | $30^{\prime}-7{ }^{\prime \prime}$ | 19'-10" | 10'-4" | $23^{\prime}-5^{\prime \prime}$ | $6^{\prime}-4 \prime$ | 23'-5" | $23^{\circ}-54^{\prime}$ | 590 | 3.67 |
| 126A18-30 | $34^{\prime}-8^{\prime \prime}$ | $31^{\prime}-1{ }^{\prime \prime}$ | 17'-9" | 9'-9" | $24^{\prime}-0^{\prime \prime}$ | $5^{\prime}-5^{\prime \prime}$ | $24^{\prime}-0^{\prime \prime}$ | $19^{\circ}-31^{\prime}$ | 528 | 4.38 |
| 126A30-18 | $37^{\prime}-4^{\prime \prime}$ | $36^{\prime}-3^{\prime \prime}$ | 17'-6" | 12'-7" | $24^{\prime}-0^{\prime \prime}$ | 9'-1" | $24^{\prime}-0^{\prime \prime}$ | $11^{\circ}-54^{\prime}$ | 547 | 2.64 |
| $\dagger 126 A 21-36$ | $35^{\prime}-4{ }^{\prime \prime}$ | $31^{\prime}-5^{\prime \prime}$ | 20'-0" | 10'-6" | $24^{\prime}-0^{\prime \prime}$ | $6^{\prime}-4^{\prime \prime}$ | $24^{\prime}-0^{\prime \prime}$ | $23^{\circ}-20^{\prime}$ | 607 | 3.76 |

$\dagger$ Very large or high structures sometimes call for additional special provisions for shape control during backfill.
Note: Other sizes are available for special designs.


Galvanized Steel 6" $\times \mathbf{2}^{\prime \prime}$ Corrugation
SUPER-SPAN

| TABLE 58. TYPICAL HORIZONTAL ELLIPSE SHAPES <br> (ALL DIMENSIONS TO INSIDE CRESTS) |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Structure <br> Number | Maximum Span | Total Rise | Top Radius $R_{T}$ | Side Radius $\mathbf{R}_{\mathrm{s}}$ | Approx. Area (Sq. Ft.) | Shape <br> Factor $\mathbf{R}_{\mathrm{T}} \mathbf{R}_{\mathrm{S}}$ |
| 66 E 30 | 19'-4" | 12'-9" | 12'-6" | $4^{\prime}-6^{\prime \prime}$ | 191 | 2.78 |
| 69 E 30 | 20'-1" | $13^{\prime}-0^{\prime \prime}$ | 13'-1" | $4^{\prime}-6^{\prime \prime}$ | 202 | 2.90 |
| 72E24 | 20'-2" | 11'-11' | $13^{\prime}-8^{\prime \prime}$ | $3^{\prime}-7{ }^{\prime \prime}$ | 183 | 3.81 |
| 75E24 | $20^{\prime}-10^{\prime \prime}$ | 12'-2" | $14^{\prime}-3^{\prime \prime}$ | $3^{\prime}-7{ }^{\prime \prime}$ | 194 | 3.97 |
| 69 E39 | $21^{\prime}-0^{\prime \prime}$ | 15'-2" | 13'-1" | 5'-11" | 248 | 2.21 |
| 78 E 27 | 21'-11" | 13'-1" | 14'-10" | $4^{\prime}-1$ " | 221 | 3.63 |
| 75 E 39 | 22'-6" | 15'-8" | 14'-3" | 5'-11" | 274 | 2.40 |
| 81 E30 | $23^{\prime}-0^{\prime \prime}$ | 14'-1" | 15'-5" | $4^{\prime}-6^{\prime \prime}$ | 249 | 3.42 |
| 78 E 39 | 23'-3" | 15'-11" | 14'-10" | 5'-11" | 288 | 2.50 |
| 81 E42 | $24^{\prime}-4^{\prime \prime}$ | 16'-11" | 15'-5" | $6^{\prime}-4^{\prime \prime}$ | 320 | 2.43 |
| 87 E30 | 24'-6" | $14^{\prime}-8{ }^{\prime \prime}$ | $16^{\prime}-6^{\prime \prime}$ | $4^{\prime}-6^{\prime \prime}$ | 274 | 3.66 |
| 90E30 | $25^{\prime}-2^{\prime \prime}$ | 14'-11" | 17'-1" | $4^{\prime}-6^{\prime \prime}$ | 287 | 3.79 |
| 87 E 39 | 25'-5" | $16^{\prime}-9^{\prime \prime}$ | $16^{\prime}-6^{\prime \prime}$ | $5^{\prime}-11^{\prime \prime}$ | 330 | 2.79 |
| 87E45 | 26'-1" | 18'-2" | $16^{\prime}-6^{\prime \prime}$ | $6^{\prime}-10^{\prime \prime}$ | 369 | 2.42 |
| 93 E 33 | $26^{\prime}-3^{\prime \prime}$ | 15'-10" | $17^{\prime}-8^{\prime \prime}$ | $5^{\prime}-0^{\prime \prime}$ | 320 | 3.53 |
| 96 E 33 | $27^{\prime}-0^{\prime \prime}$ | $16^{\prime}-2^{\prime \prime}$ | $18^{\prime}-3^{\prime \prime}$ | $5^{\prime}-0^{\prime \prime}$ | 334 | 3.65 |
| 90E48 | 27'-2" | 19'-1" | $17^{\prime}-1$ " | 7'-3" | 405 | 2.35 |
| 93 E 48 | 27'-11" | 19'-5" | 17'-8" | 7'-3" | 421 | 2.43 |
| 99 E 36 | 28'-1" | 17'-1" | 18'-10" | 5'-5" | 369 | 3.47 |
| 102 E 36 | 28'-10" | 17'-5" | 19'-5" | 5'-5" | 384 | 3.58 |
| 99 E 48 | 29'-5" | 19'11" | 18'-10" | $7^{\prime}-3^{\prime \prime}$ | 455 | 2.59 |
| 102 E 48 | 30'-1" | 20'-2" | $19^{\prime}-5^{\prime \prime}$ | $7^{\prime}-3^{\prime \prime}$ | 472 | 2.67 |
| 108 E 36 | 30'-3" | 17'11" | $20^{\prime}-7{ }^{\prime \prime}$ | 5'-5" | 415 | 3.75 |
| 105E51 | 31'-2" | $21^{\prime}-2^{\prime \prime}$ | $20^{\prime}-0^{\prime \prime}$ | 7'-9" | 513 | 2.58 |
| 111 E39 | $31^{\prime}-4 \prime$ | 18'11" | 21'-1" | 5'-11" | 454 | 3.56 |
| 114 E 39 | 32'-1" | $19^{\prime}-2^{\prime \prime}$ | $21^{\prime}-8^{\prime \prime}$ | 5'-11" | 471 | 3.66 |
| 108 E 54 | 32'-3" | $22^{\prime}-2^{\prime \prime}$ | 20'-7" | $8^{\prime}-2^{\prime \prime}$ | 555 | 2.52 |
| 111 E54 | $33^{\prime}-0^{\prime \prime}$ | $22^{\prime}-5^{\prime \prime}$ | 21'-1" | $8^{\prime}-2^{\prime \prime}$ | 574 | 2.58 |
| $117 E 42$ | 33'-2" | 20'-1" | $22^{\prime}-3^{\prime \prime}$ | $6^{\prime}-4^{\prime \prime}$ | 512 | 3.51 |
| 114 E 57 | 34'-1" | $23^{\prime}-4^{\prime \prime}$ | $21^{\prime}-8^{\prime \prime}$ | $8^{\prime}-8^{\prime \prime}$ | 619 | 2.50 |
| $123 E 42$ | 34'-7" | $20^{\prime}-8^{\prime \prime}$ | 23'-5" | $6^{\prime}-4 \prime$ | 548 | 3.69 |
| 123 E 45 | 34'-11" | $21^{\prime}-4^{\prime \prime}$ | $23^{\prime}-5^{\prime \prime}$ | 6'-10" | 574 | 3.42 |
| $\dagger 117 \mathrm{E} 60$ | 35'-1" | $24^{\prime}-4^{\prime \prime}$ | $22^{\prime}-3^{\prime \prime}$ | 9'-1" | 665 | 2.44 |
| 126 E48 | $36^{\prime}-0^{\prime \prime}$ | $22^{\prime}-4^{\prime \prime}$ | $24^{\prime}-0^{\prime \prime}$ | $7{ }^{\prime}-3^{\prime \prime}$ | 619 | 3.31 |
| $\dagger 132 \mathrm{E} 45$ | $37^{\prime}-2^{\prime \prime}$ | $22^{\prime}-2^{\prime \prime}$ | $25^{\prime}-2^{\prime \prime}$ | $6^{\prime}-10^{\prime \prime}$ | 631 | 3.68 |

$\dagger$ Very large or high structures sometimes call for additional special provisions for shape control during backfill.
Note:
Other sizes are available for special designs.

| TABLE 59. TYPICAL PEAR SHAPES (ALL DIMENSIONS TO INSIDE CRESTS) |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Structure Number | Maximum Span | Total Rise | Bottom Rise | Top Radius $\mathrm{R}_{\mathrm{T}}$ | $\Delta$ | Corner <br> Radius $\mathbf{R}_{\mathrm{c}}$ | $\Delta_{\text {c }}$ | Side Radius $\mathbf{R}_{\mathrm{s}}$ | $\Delta_{\text {s }}$ | Bottom Radius $\mathbf{R}_{\mathrm{B}}$ | $\Delta_{\text {b }}$ | Approx. Area (Sq. Ft.) |
| 75P15-72-45 | $23^{\prime}-8^{\prime \prime}$ | $25^{\prime}-5^{\prime \prime}$ | 14'-10" | 14'-11" | $38^{\circ}-25^{\prime}$ | $6^{\prime}-1^{\prime \prime}$ | $37^{\circ}-10^{\prime}$ | $16^{\prime}-6^{\prime \prime}$ | $66^{\circ}-23^{\prime}$ | $9{ }^{\prime}-0^{\prime \prime}$ | $38^{\circ}-02^{\prime}$ | 477 |
| 66P21-66-60 | $24^{\prime}-0^{\prime \prime}$ | 25'-10" | 15'-1" | $16^{\prime}-2^{\prime \prime}$ | $31^{\circ}-02^{\prime}$ | $7^{\prime}-0^{\prime \prime}$ | $45^{\circ}-18^{\prime}$ | $17^{\prime}-4^{\prime \prime}$ | $57^{\circ}-49^{\prime}$ | $9^{\prime \prime} 1{ }^{\prime \prime}$ | $45^{\circ}-51^{\prime}$ | 497 |
| 81P21-60-63 | 25'-2" | 26'-1" | 16'-1" | 15'-10" | $38^{\circ}-16^{\prime}$ | $6^{\prime}-11^{\prime \prime}$ | $45^{\circ}-50^{\prime}$ | 18'-9" | $48^{\circ}-38^{\prime}$ | $10^{\prime}-3^{\prime \prime}$ | $46^{\circ}-39^{\prime}$ | 517 |
| 81P15-75-54 | $24^{\prime}-10^{\prime \prime}$ | 27'-8" | 16'-9" | 15'-11" | $38^{\circ}-41^{\prime}$ | 5'-9" | $39^{\circ}-17^{\prime}$ | 19'-9" | $57^{\circ}-45^{\prime}$ | $9^{\prime}-3^{\prime \prime}$ | $44^{\circ}-17^{\prime}$ | 544 |
| *84P15-90-36 | 26'-7" | $28^{\prime}-4^{\prime \prime}$ | 18'-1" | 20'-11" | $30^{\circ}-34^{\prime}$ | $4^{\prime}-9^{\prime \prime}$ | $47^{\circ}-25^{\prime}$ | $20^{\prime}-2^{\prime \prime}$ | $67^{\circ}-46^{\prime}$ | 7'-11" | $34^{\circ}-15^{\prime}$ | 593 |
| 90P18-78-48 | 27'-6" | $27^{\prime}-8^{\prime \prime}$ | $18^{\prime}-0^{\prime \prime}$ | 19'-11" | $34^{\circ}-22^{\prime}$ | $5^{\prime}-6^{\prime \prime}$ | $49^{\circ}-16^{\prime}$ | $20^{\prime}-3^{\prime \prime}$ | $58^{\circ}-32^{\prime}$ | $9^{\prime}-7{ }^{\prime \prime}$ | $37^{\circ}-00^{\prime}$ | 596 |
| 81P24-66-75 | 28'-1" | 27'-10" | 16'-9" | 20'-5" | $30^{\circ}-11^{\prime}$ | $7^{\prime}-3^{\prime \prime}$ | $50^{\circ}-0^{\prime}$ | 18'-10" | $53^{\circ}-16^{\prime}$ | 12'-3" | $46^{\circ}-33^{\prime}$ | 624 |
| 96P21-72-72 | 28'-6" | 30'-8" | 19'-8" | 18'-2" | $40^{\circ}-11^{\prime}$ | $7^{\prime}-0^{\prime \prime}$ | $45^{\circ}-18^{\prime}$ | $24^{\prime}-3^{\prime \prime}$ | $45^{\circ}-13^{\prime}$ | 11'-1" | $49^{\circ}-18^{\prime}$ | 689 |
| 96P24-69-75 | $30^{\prime}-0^{\prime \prime}$ | 29'-8" | 20'-1" | 21'-10" | $33^{\circ}-28^{\prime}$ | $6^{\prime}-7{ }^{\prime \prime}$ | $55^{\circ}-0^{\prime}$ | $24^{\prime}-2^{\prime \prime}$ | $43^{\circ}-29^{\prime}$ | 11'-10" | $48^{\circ}-03^{\prime}$ | 698 |
| ${ }^{* * 102 P 21-72-78 ~}$ | 29'-11" | 31'-3" | $20^{\prime}-0^{\prime \prime}$ | 19'-3" | $40^{\circ}-18^{\prime}$ | $7^{\prime}-0^{\prime \prime}$ | $45^{\circ}-18^{\prime}$ | 24'-4" | 45 ${ }^{\circ}-05^{\prime}$ | 12'-0" | $49^{\circ}-19^{\prime}$ | 738 |

*Meets AREMA clearances for bridges and turntables.
${ }^{* *}$ Meets AREMA clearances for single track tunnel.
Note

1. Other sizes are available for special designs.


End View - Pear

Galvanized Steel 6" $\times \mathbf{2}^{\prime \prime}$ Corrugation

| Galvanized Steel $\mathbf{6}^{\prime \prime} \mathbf{x} \mathbf{2}^{\prime \prime \prime}$ Corrugation |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |

${ }^{*}$ Meets AREMA clearances for bridges and turntables.
${ }^{* *}$ Meets AREMA clearances for single track tunnel.
Note:

1. Other sizes are available for special designs.


## Conceptual drawings'



Section A-A (see elev. p. 83)


## Section B-B

Typical Slope Collar ${ }^{1}$ (see elev. p. 83)

## Notes

1. Many of the details are conceptual. The designer should work with the Contech representative on each particular application.
2. Top and bottom steps are the same for ellipse shapes.
 as shown

- 

$\left.\begin{array}{c}\text { TABLE 61. TYPICAL TOP STEP DIMENSIONS } \\ \begin{array}{c}\text { Top or } \\ \text { Bottom } \\ \text { Arc. in Pi }\end{array} \\ \hline 60\end{array} \begin{array}{c}\text { Step or } \\ \text { Mid- } \\ \text { Ordinate }\end{array}\right]$
(applies only to structures with $80^{\circ}$ top arc)

## SUPER-SPAN

## Galvanized Steel Long Span Structures - <br> $6^{\prime \prime} \times 2^{\prime \prime}$ Corrugation Specification <br> General Description

The long span steel structural plate structure, conforming to the dimensions shown on the plans and specifications, shall be installed at the location designated. The design and installation shall conform to AASHTO Standard Specifications for Highway Bridges, Division I, "Soil-Corrugated Metal Structure Interaction Systems", Section 12.7, "Long Span Structural Plate Structures", and Division II, Section 26, "Metal Culverts" and Division II, Section 8, "Concrete Structures."

## Materials

The galvanized steel structural plate shall have $6^{\prime \prime} \times 2^{\prime \prime}$ corrugations and shall be of the gage as shown on the plans. The plates shall be manufactured in conformance with AASHTO Specification M 167. Bolts and nuts shall meet the provisions of ASTM A 449, Type 1 and ASTM A 563, Grade C, respectively. The steel anchor bolts shall conform to ASTM A-307, Grade A.

## Longitudinal Structural Stiffeners (Thrust Beams)

Longitudinal stiffeners shall be located at the radius transition at the ends of the top arc. The thrust beams shall consist of reinforced concrete conforming to Division II, Section 8, Class B of the AASHTO Standard Specifications for Highway Bridges having a minimum compression strength of 2400 psi. Reinforcing steel shall conform to ASTM A 615, Grade 40, having a minimum yield strength of 40,000 psi. Thrust beams shall be formed and poured conforming to the plan dimensions when the backfill reaches the bottom elevation of the thrust beams.

## Design

The long span structure shall be designed in accordance with the latest AASHTO design criteria and shall be required to incorporate the use of continuous longitudinal structural stiffeners (concrete thrust beams).

## Structure Assembly

The structure shall be assembled in strict accordance with the manufacturer's instructions and to the design shape shown on the plans. Plates shall be assembled according to plate assembly drawings supplied by the manufacturer.

## Structural Backfill

## Material

A granular type of material shall be used around and over the structure. This select structural backfill material shall conform to one of the following classifications of soil from AASHTO Specification M-145, as modified in the following table for A-1, A-2-4 or A-2-5.
GROUP CLASSIFICATION A-1-a A-1 $\quad$ A-1-b $\quad$ A-2-4 $\quad$ A-2-5

|  | alysis, P | nt Pas |  |  |
| :---: | :---: | :---: | :---: | :---: |
| No. 10 (2.00 mm) | 50 Max. |  |  |  |
| No. 40 (0.425 mm) | 30 Max. | 50 Max. |  |  |
| No. 100 (0.150 mm) |  |  | 50 Max. | 50 Max. |
| No. 200 (0.075 mm) | 15 Max. | 25 Max. | 20 Max. | 20 Max. |
| Characteristics of Fraction Passing No. 40 (0.425 mm) |  |  |  |  |
| Liquid Limit | 6 Max. |  | 40 Max. | 41 Min. |
| Plasticity Index |  |  | 10 Max. | 10 Max. |
| Usual Types of Significant | Stone Fragments |  | Silty or Clayey |  |
| Constituent Materials | Gravel and Sand |  | Gravel and Sand |  |

* Modified to be more select than M-145.


## Additional Requirements

1. Materials must be dense graded (open graded or gap graded materials are not allowed).
2. Fine beach sands, windblown sands, and stream deposited sands all of which exhibit fine, rounded particles and typically are classified by AASHTO M-145 as A-3 materials are not allowed.
3. On site mixing or blending to achieve specified gradation is not allowed.

Maximum particle size shall not exceed 3 inches. For the A-2 materials, moisture content must be between $-3 \%$ and $+2 \%$ optimum as defined by AASHTO T-180. All soil classifications are limited to the following height of cover limits and structure shape applications:

- A-1-a material is suitable for all long span shapes, sizes and fill heights.
- A-1-b material is suitable only for use with high profile arch and pear shape structures to a 12' maximum fill height and for use with elliptical and low profile arch structures to a $20^{\prime}$ maximum fill height.
- A-2-4 and A-2-5 materials are restricted to maximum heights of cover of $12^{\prime}$. These materials are not allowed for use with pear, pear arch or high profile arches with more than 30 Pi in the side arc.

Other backfill materials which provide equivalent structural properties, longterm, in the environmental conditions expected (saturation, freeze-thaw, etc.) may be used. Such materials shall be approved only after thorough investigation and testing by a soils engineer familiar with the requirements for structural backfill of long span structures.

## Backfill Envelope Limits

The backfill envelope limits are as detailed on the plans.

## Backfill Placement

Before backfilling, the erected structure shall meet the tolerance and symmetry requirements of AASHTO and the manufacturer.

Approved backfill material shall be placed in horizontal, uniform layers not exceeding $8^{\prime \prime}$ in thickness, before compaction, and shall be brought up uniformly on both sides of the structure. Each layer of backfill shall be compacted to a relative density of not less than $90 \%$, modified proctor per AASHTO Test Method No. T-180. Field density tests of compacted backfill will be made at regular intervals during backfill.
Long span structures, due to their size and shape, are sensitive to the types and weights of equipment used to place and compact the select backfill material. This is especially critical in the areas immediately adjacent to and above the structure. Therefore, equipment types will be restricted in those critical zones. Compaction equipment or methods that produce horizontal or vertical earth pressures which cause excessive distortion or damage to structures shall not be used. Contractors should plan to have a D4 (approximately 20,000 lbs.) or similar weight tracked dozer to place and grade backfill immediately alongside and above the structure until minimum cover level is reached. Lightweight vibratory plate or roller type compaction equipment must be used to compact the backfill in these zones. Use of heavier equipment and/or rubber tired equipment such as scrapers, graders, and front end loaders will likely be prohibited inside the select fill envelope zone until appropriate minimum cover height has been obtained.

## Shape Control Monitoring

Contech shall provide a Shape Control Technician who is a qualified representative of a professional soils engineering firm, or other qualified organization, to ensure a properly shaped structure. The Shape Control Technician shall take initial measurements of the erected structure before backfilling, observe all backfill materials and their placement, and record compaction densities. The Technician shall record all density readings and ensure they meet the requirements of the plans and specifications. However, in no case shall the relative densities be less than 90\% per AASHTO T-180. The Shape Control Technician shall monitor the structure shape during the placement of structural backfill to the minimum cover height over the structure. No structural backfill shall be placed without the Shape Control Technician on site.

## The Shape Control Technician shall:

- Monitor the structure's shape throughout the backfilling operation and report shape change rates to the contractor.
- Contact the Contech representative immediately if there are problems in meeting the established tolerances.
- Have full authority to stop backfill work if necessary.


## Preconstruction Conference

Prior to construction, a meeting will be held to review the construction procedures. A qualified representative of the manufacturer of the structure will be present to discuss methods and responsibility for shape monitoring and control, backfill material selection, testing and placement, and compaction methods and testing. A representative of the Engineer, Prime Contractor, and any involved sub-contractors must be present.

## Alternate Structures

The Contractor may furnish an alternate structure to the long span shown on the plans and these specifications but the following conditions must be met:

1. The structure must be designed using the AASHTO Long Span criteria and these plans and specifications. Steel structural plate shall conform to the requirements of AASHTO M167. Aluminum alloy structural plate shall conform to the requirements of AASHTO M219.
2. The corrugated metal plate thickness specified is considered the minimum acceptable for the structure(s) on this project based on structural and durability requirements. Any other structure, regardless of "special features", must be of the same thickness or greater.
3. "Special Features", such as hot rolled structural steel ribs, shall be hot-dip galvanized after fabrication per ASTM A 123. Ribs shall be placed across the top $180^{\circ}$, i.e., to the springline of all structures. Maximum rib spacing shall be two (2) feet. Ribs shall be placed over the same length of structure that the thrust beams would apply. No allowance for composite action between the rib and plate will be allowed. The combined moment of inertia of both plate and rib must satisfy the normal flexibility factor as shown in AASHTO Division I, Section 12.6.1.4. The span in the formula for the flexibility factor shall be replaced by twice the top arc radius.
4. Alternate structures meeting the above criteria will only be considered for use if pre-approved in writing by the Engineer prior to the bid date. To qualify for pre-approval, an alternate submittal package must be submitted to the Engineer a minimum of 15 days prior to the bid date.
5. The material supplier shall be a qualified manufacturer of steel structural plate and long span structures with a minimum of 50 successful installations. The foundation, structural backfill and end treatment shall be as required herein and detailed on the plans.

| TABLE 63. TYPICAL LOW PROFILE ARCH SHAPES (ALL DIMENSIONS TO INSIDE CRESTS) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Structure <br> Number | Maximum Span | Bottom Span | Total Rise | Top Rise | Top Radius $\mathbf{R}_{\mathbf{T}}$ | Side Radius $\mathbf{R}_{\mathbf{S}}$ | Angle Below Horizontal $\Delta$ | Approx. Area (Sq. Ft.) | Shape <br> Factor $R_{T} / R_{S}$ |
| 23A5 | 19'-5" | 19'-2" | $6^{\prime}-9^{\prime \prime}$ | $5^{\prime}-10^{\prime \prime}$ | 13'-1" | $3^{\prime}-7{ }^{\prime \prime}$ | $15^{\circ}-23^{\prime}$ | 105 | 3.66 |
| 23A6 | 20'-1" | 19'-10" | 7'-6" | $6^{\prime}-6^{\prime \prime}$ | 13'-1" | $4^{\prime}-6^{\prime \prime}$ | $12^{\circ}-21^{\prime}$ | 120 | 2.91 |
| 25A6 | 21'-7" | 21'-4" | 7'-9" | $6^{\prime}-9^{\prime \prime}$ | $14^{\prime}-3^{\prime \prime}$ | $4^{\prime}-6^{\prime \prime}$ | $12^{\circ}-21^{\prime}$ | 133 | 3.17 |
| 26A6 | 22'-3" | 22'-1" | 7'-1" | $6^{\prime}-11^{\prime \prime}$ | 14'-10" | $4^{\prime}-6^{\prime \prime}$ | $12^{\circ}-21^{\prime}$ | 140 | 3.30 |
| 27A6 | 23'-0" | 22'-10" | $8^{\prime}-0^{\prime \prime}$ | 7'-1" | 15'-5" | $4^{\prime}-6^{\prime \prime}$ | $12^{\circ}-21^{\prime}$ | 147 | 3.42 |
| 28A6 | 23'-9" | 23'-7" | $8^{\prime}-2^{\prime \prime}$ | 7'-2" | $16^{\prime}-0^{\prime \prime}$ | $4^{\prime}-6^{\prime \prime}$ | $12^{\circ}-21^{\prime}$ | 154 | 3.55 |
| 29 A 6 | 24'-6" | $24^{\prime}-3^{\prime \prime}$ | $8^{\prime}-3^{\prime \prime}$ | 7'-4" | $16^{\prime}-7^{\prime \prime}$ | $4^{\prime}-6^{\prime \prime}$ | $12^{\circ}-21^{\prime}$ | 161 | 3.68 |
| 30A6 | $25^{\prime}-3^{\prime \prime}$ | $25^{\prime}-0^{\prime \prime}$ | $8^{\prime}-5^{\prime \prime}$ | 7'-5" | 17'-2" | $4^{\prime}-6^{\prime \prime}$ | $12^{\circ}-21^{\prime}$ | 168 | 3.81 |
| 31 A 6 | $26^{\prime}-0^{\prime \prime}$ | 25'-9" | 8'-7" | $7{ }^{\prime}-7{ }^{\prime \prime}$ | 17'-8" | $4^{\prime}-6^{\prime \prime}$ | $12^{\circ}-21^{\prime}$ | 176 | 3.93 |
| $31 \mathrm{A8}$ | 27'-3" | 27'-2" | 10'-0" | $9^{\prime}-0^{\prime \prime}$ | $17^{\prime}-8^{\prime \prime}$ | $6^{\prime}-4^{\prime \prime}$ | $8^{\circ}-52^{\prime}$ | 217 | 2.80 |
| 33A7 | 28'-1" | 27'-11" | 9'-6" | $8^{\prime}-7{ }^{\prime \prime}$ | $18^{\prime} 10^{\prime \prime}$ | $5^{\prime}-5^{\prime \prime}$ | $10^{\circ}-19^{\prime}$ | 212 | 3.48 |
| 33A8 | 28'-9" | 28'-7" | $10^{\prime}-3^{\prime \prime}$ | 9'-3" | 18'-10" | $6^{\prime}-4 \prime \prime$ | $8^{\circ}-52^{\prime}$ | 234 | 2.98 |
| 34A7 | 28'-10" | 28'-8" | 9'-8" | 8'-8" | 19'-5" | $5^{\prime}-5^{\prime \prime}$ | $10^{\circ}-19^{\prime}$ | 220 | 3.59 |
| 36A7 | $30^{\prime}-4 \prime$ | $30^{\prime}-2^{\prime \prime}$ | $9^{\prime}-11^{\prime \prime}$ | $9^{\prime}-0^{\prime \prime}$ | $20^{\prime}-7^{\prime \prime}$ | $5^{\prime}-5^{\prime \prime}$ | $10^{\circ}-19^{\prime}$ | 237 | 3.80 |
| 36A8 | $31^{\prime}-0^{\prime \prime}$ | 30'-10" | 10'-8" | $9^{\prime}-8{ }^{\prime \prime}$ | 20'-7" | $6^{\prime}-4^{\prime \prime}$ | $8^{\circ}-52^{\prime}$ | 261 | 3.25 |
| 36A10 | 31'-8" | $31^{\prime}-2^{\prime \prime}$ | 12'-2" | $10^{\prime}-4^{\prime \prime}$ | $20^{\prime}-7^{\prime \prime}$ | 7'-3" | $14^{\circ}-02^{\prime}$ | 309 | 2.84 |
| 37A7 | 31'-1" | $30^{\prime \prime 1} 1{ }^{\prime \prime}$ | 10'-1" | 9'-1" | 21'-2" | 5'-5" | $10^{\circ}-19^{\prime}$ | 246 | 3.90 |
| 37A10 | $32^{\prime}-4^{\prime \prime}$ | 31'-11" | 12'-3" | 10'-6" | 21'-2" | $7^{\prime}-3^{\prime \prime}$ | $14^{\circ}-02^{\prime}$ | 320 | 2.92 |
| 38A7 | 31'-10" | 31'-7" | 10'-2" | $9^{\prime}-3^{\prime \prime}$ | 21'-9" | 5'-5" | $10^{\circ}-19^{\prime}$ | 255 | 4.01 |
| 38A10 | 33'-1" | 32'-8" | 12'-5" | $10^{\prime}-8^{\prime \prime}$ | 21'-9" | $7^{\prime}-3^{\prime \prime}$ | $14^{\circ}-02^{\prime}$ | 330 | 3.00 |
| 39A8 | 33'-2" | $33^{\prime}-0^{\prime \prime}$ | 11'-1" | 10'-1" | 22'-4" | $6^{\prime}-4^{\prime \prime}$ | $8^{\circ}-52^{\prime}$ | 289 | 3.52 |
| 39A11 | 34'-6" | 34'-1" | $13^{\prime}-3^{\prime \prime}$ | 11'-6" | $22^{\prime}-4^{\prime \prime}$ | $8^{\prime}-2^{\prime \prime}$ | $12^{\circ}-29^{\prime}$ | 368 | 2.73 |
| 41A8 | $34^{\prime}-8^{\prime \prime}$ | $34^{\prime}-6^{\prime \prime}$ | 11'-4" | $10^{\prime}-4^{\prime \prime}$ | $23^{\prime}-5^{\prime \prime}$ | $6^{\prime}-4^{\prime \prime}$ | $8^{\circ}-52^{\prime}$ | 308 | 3.70 |
| 41A14 | 37'-11" | 37'-8" | 15'-8" | 13'-10" | $23^{\prime}-5^{\prime \prime}$ | 10'-11" | $9^{\circ}-24^{\prime}$ | 478 | 2.15 |
| 42A8 | $35^{\prime}-5^{\prime \prime}$ | $35^{\prime}-3^{\prime \prime}$ | 11'-5" | 10'-6" | $24^{\prime}-0^{\prime \prime}$ | $6^{\prime}-4^{\prime \prime}$ | $8^{\circ}-52^{\prime}$ | 318 | 3.79 |
| 42A14 | 38'-8" | 38'-5" | 15'-9" | $14^{\prime}-0^{\prime \prime}$ | $24^{\prime}-0^{\prime \prime}$ | 10'-11" | $9^{\circ}-24^{\prime}$ | 491 | 2.20 |

Note: Other sizes are available for special designs.
1 The design table on page 83 of the catalog is for steel $6^{\prime \prime} \times 2^{\prime \prime}$ corrugation only, for aluminum $9^{\prime \prime} \times 2-1 / 2^{\prime \prime}$ corrugation design, please call your local Contech representative.
Reinforcing ribs may be required. Rib length will be determined.


| TABLE 64. TYPICAL HIGH PROFILE ARCH SHAPES (ALL DIMENSIONS TO INSIDE CRESTS) |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Structure <br> Number | Maximum Span | Bottom Span | Total Rise | Top Rise | Top Radius $\mathbf{R}_{\mathrm{T}}$ | Upper Side <br> Radius $\mathbf{R}_{\mathrm{c}}$ | Lower Side Radius $\mathbf{R}_{\mathrm{s}}$ | Angle Below Horizontal $\Delta$ | Approx. Area (Sq. Ft.) | Shape <br> Factor $R_{T} / R_{c}$ |
| 23A5-3 | 20'-1" | 19'-7" | 9'-1" | $6^{\prime}-6^{\prime \prime}$ | 13'-1" | 4'-6" | 13'-1" | $11^{\circ}-18^{\prime}$ | 152 | 2.91 |
| 23A6-6 | 20'9" | 18'-10" | 12'-1" | $7^{\prime}-3^{\prime \prime}$ | 13'-1" | $5^{\prime}-5^{\prime \prime}$ | 13'-1" | $21^{\circ}-44^{\prime}$ | 214 | 2.42 |
| 25A5-6 | 21'-6" | 19'-10" | 11'-8" | $6^{\prime}-9{ }^{\prime \prime}$ | $14^{\prime}-3^{\prime \prime}$ | $4^{\prime}-6^{\prime \prime}$ | $14^{\prime}-3^{\prime \prime}$ | $20^{\circ}-0^{\prime}$ | 215 | 3.17 |
| 25A7-8 | 22'-10" | $19^{\prime} 10^{\prime \prime}$ | 14'-6" | 8'-2" | $14^{\prime}-3^{\prime \prime}$ | $6^{\prime}-4^{\prime \prime}$ | $14^{\prime}-3^{\prime \prime}$ | $26^{\circ}-23^{\prime}$ | 285 | 2.25 |
| 26A5-6 | 22'-3" | 20'-7" | 11'-10" | $6^{\prime}-11^{\prime \prime}$ | 14'-10" | $4^{\prime}-6^{\prime \prime}$ | 14'-10" | $19^{\circ}-13^{\prime}$ | 225 | 3.30 |
| 26A6-8 | 22'-11" | 20'-1" | 14'-0" | 7'-7" | 14'-10" | $5^{\prime}-5^{\prime \prime}$ | 14'-10" | $25^{\circ}--22^{\prime}$ | 275 | 2.74 |
| 27A5-6 | $23^{\prime}-0^{\prime \prime}$ | 21'-5" | 11'-11" | $7{ }^{\prime \prime}-1$ | $15^{\prime}-5^{\prime \prime}$ | $4^{\prime}-6^{\prime \prime}$ | $15^{\prime}-5^{\prime \prime}$ | $18^{\circ}-31^{\prime}$ | 235 | 3.43 |
| 27A7-8 | $24^{\prime}-4^{\prime \prime}$ | 21'-7" | 14'-10" | 8'-5" | 15'-5" | $6^{\prime}-4^{\prime \prime}$ | 15'-5" | $24^{\circ}-27^{\prime}$ | 309 | 2.43 |
| 28A5-6 | 23'-9" | $22^{\prime}-3^{\prime \prime}$ | 12'-1" | $7^{\prime}-2 \prime \prime$ | 16'-0" | $4^{\prime}-6^{\prime \prime}$ | 16'-0" | $17^{\circ}-51^{\prime}$ | 245 | 3.56 |
| 29A5-8 | $24^{\prime}$-6" | 21'-11' | 13'-9" | $7^{\prime}-4^{\prime \prime}$ | 16'-7" | $4^{\prime}-6^{\prime \prime}$ | 16'-7" | $22^{\circ}-45^{\prime}$ | 289 | 3.69 |
| 29A7-8 | 25'-10" | 23'-3" | 15'-1" | 8'-9" | 16'-7" | $6^{\prime}-4^{\prime \prime}$ | 16'-7" | $22^{\circ}-45^{\prime}$ | 335 | 2.62 |
| 30A5-7 | $25^{\prime}-3^{\prime \prime}$ | 23'-4" | 13'-1" | 7'-5" | 17'-2" | $4^{\prime}-6^{\prime \prime}$ | 17'-2" | $19^{\circ}-20^{\prime}$ | 283 | 3.81 |
| 30A7-8 | 26'-7" | 24'-1" | 15'-3" | 8'-10" | 17'-2" | $6^{\prime}-4^{\prime \prime}$ | 17'-2" | $22^{\circ}-0^{\prime}$ | 347 | 2.71 |
| 31A5-7 | $26^{\prime}-0^{\prime \prime}$ | 24'-1" | $13^{\prime}-3^{\prime \prime}$ | 7'-7" | 17'-8" | $4^{\prime}-6^{\prime \prime}$ | 17'-8" | $18^{\circ}-43^{\prime}$ | 294 | 3.94 |
| 31A7-8 | 27'-3" | 24'-10" | 15'-5" | $99^{\prime}-0^{\prime \prime}$ | 17'-8" | $6^{\prime}-4^{\prime \prime}$ | $17^{\prime}-8^{\prime \prime}$ | $21^{\circ}-17^{\prime}$ | 360 | 2.80 |
| 33A5-7 | 27'-5" | $25^{\prime}-8^{\prime \prime}$ | 13'-7" | $7^{\prime}-10^{\prime \prime}$ | 18'-10" | $4^{\prime}-6^{\prime \prime}$ | 18'-10" | $17^{\circ}-35^{\prime}$ | 317 | 4.20 |
| 33A8-8 | 29'-5" | 27'-2" | 16'-5" | 10'-0" | 18'-10" | 7'-3" | 18'-10" | $20^{\circ}-0^{\prime}$ | 412 | 2.60 |
| 34A5-8 | 28'-2" | 25'-11" | 14'-5" | $8^{\prime}-0^{\prime \prime}$ | 19'-5" | $4^{\prime}-6^{\prime \prime}$ | 19'-5" | $19^{\circ}-25^{\prime}$ | 348 | 4.33 |
| 34A8-10 | $30^{\prime}-2^{\prime \prime}$ | 26'-9" | $18^{\prime}-0^{\prime \prime}$ | 10'-1" | 19'-5" | $7^{\prime}-3^{\prime \prime}$ | 19'-5" | $24^{\circ}-07^{\prime}$ | 466 | 2.68 |
| 36A6-8 | $30^{\prime}-4^{\prime \prime}$ | $28^{\prime}-3^{\prime \prime}$ | $15^{\prime}-5^{\prime \prime}$ | $9^{\prime}-0^{\prime \prime}$ | $20^{\prime}-7^{\prime \prime}$ | 5'-5" | $20^{\prime}-7^{\prime \prime}$ | $18^{\circ}-20^{\prime}$ | 400 | 3.80 |
| 36A8-10 | $31^{\prime}-8^{\prime \prime}$ | 28'-5" | 18'-4" | $10^{\prime}-4^{\prime \prime}$ | 20'-7" | $7^{\prime}-3^{\prime \prime}$ | 20'-7" | $22^{\circ}-47^{\prime}$ | 497 | 2.84 |
| 37A6-8 | $31^{\prime \prime} \mathbf{1}^{\prime \prime}$ | $29^{\prime}-0^{\prime \prime}$ | 15'-7" | 9'-1" | 21'-2" | 5'-5" | 21'-2" | $17^{\circ}-50^{\prime}$ | 413 | 3.91 |
| 37A7-10 | 31'-9" | 28'-7" | 17'-9" | $9^{\prime}-10^{\prime \prime}$ | 21'-2" | $6^{\prime}-4^{\prime \prime}$ | 21'-2" | $22^{\circ}-10^{\prime}$ | 484 | 3.34 |
| $\dagger 37 \mathrm{~A}$-12 | 32'-4" | 27'-11" | 19'-11" | 10'-6" | 21'-2" | $7{ }^{\prime}-3^{\prime \prime}$ | 21'-2" | $26^{\circ}-29^{\prime}$ | 555 | 2.92 |
| 38A6-10 | 31'-10" | 28'-9" | 17'-3" | $9^{\prime}-3^{\prime \prime}$ | 21'-9" | $5^{\prime}-5^{\prime \prime}$ | 21'-9" | $21^{\circ}-35^{\prime}$ | 470 | 4.02 |
| $\dagger 3848-12$ | 33'-1" | 28'-9" | 20'-1" | $10^{\prime}-8^{\prime \prime}$ | 21'-9" | $7^{\prime}-3^{\prime \prime}$ | 21'-9" | $25^{\circ}-47^{\prime}$ | 572 | 3.00 |
| 39A6-10 | 32'-6" | 29'-7" | 17'-4" | $9^{\prime}-4 \prime$ | 22'-4" | 5'-5" | 22'-4" | $21^{\circ}-02^{\prime}$ | 485 | 4.12 |
| $\dagger$ †9A8-12 | 33'-10" | 29'-8" | $20^{\prime}-3^{\prime \prime}$ | 10'-9" | $22^{\prime}-4^{\prime \prime}$ | $7^{\prime}-3^{\prime \prime}$ | 22'-4" | $25^{\circ}-08^{\prime}$ | 589 | 3.08 |
| 41A6-10 | $34^{\prime}-0^{\prime \prime}$ | 31'-2" | 17'-8" | $9^{\prime}-8{ }^{\prime \prime}$ | $23^{\prime}-5^{\prime \prime}$ | 5'-5" | 23'-5" | $20^{\circ}-0^{\prime}$ | 514 | 4.33 |
| $\dagger 41 A 7-12$ | $34^{\prime}-8^{\prime \prime}$ | 30'-8" | 19'-10" | $10^{\prime}-4^{\prime \prime}$ | $23^{\prime}-5^{\prime \prime}$ | $6^{\prime}-4^{\prime \prime}$ | 23'-5" | $23^{\circ}-54^{\prime}$ | 591 | 3.70 |
| 42A6-10 | $34^{\prime}-9^{\prime \prime}$ | $32^{\prime}-0^{\prime \prime}$ | 17'-9" | 9'-9" | $24^{\prime}-0^{\prime \prime}$ | 5'-5" | $24^{\prime}-0^{\prime \prime}$ | $19^{\circ}-32^{\prime}$ | 529 | 4.44 |
| $\dagger 42 \mathrm{~A}-12$ | 35'-5" | $31^{\prime}-6{ }^{\prime \prime}$ | 20'-0" | 10'-6" | $24^{\prime}-0^{\prime \prime}$ | $6^{\prime}-4 \prime$ | $24^{\prime}-0^{\prime \prime}$ | $23^{\circ}-20^{\prime}$ | 608 | 3.80 |

$\dagger$ Very large or high structures sometimes call for additional special provisions for shape control during backfill.

## Notes:

1. Other sizes are available for special designs.

2 The design table on page 83 of the catalog is for steel $6^{\prime \prime} \times 2^{\prime \prime}$ corrugation only. For aluminum
$9^{\prime \prime} \times 2-1 / 2^{\prime \prime}$ corrugation design, please call your local Contech representative.
Reinforcing ribs may be required. Rib length will be determined.


End View - High Profile Arch

Aluminum 9" $\times 2$ 2-1/2" Corrugation
SUPER-PLATE

| TABLE 65. TYPICAL HORIZONTAL ELLIPSE SHAPES' (ALL DIMENSIONS TO INSIDE CRESTS) |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Structure <br> Number | Maximum Span | Total Rise | Top <br> Radius $\mathbf{R}_{\mathrm{T}}$ | Side <br> Radius $\mathbf{R}_{\mathrm{s}}$ | Approx. <br> Area (Sq. Ft.) | Shape <br> Factor $\mathbf{R}_{\mathrm{T}} \mathbf{R}_{\mathrm{S}}$ |
| 22E10 | 19'-4" | 12'-9" | 12'-6" | $4^{\prime}-6^{\prime \prime}$ | 191 | 2.79 |
| 23E10 | 20'-1" | $13^{\prime}-0^{\prime \prime}$ | 13'-1" | $4^{\prime}-6^{\prime \prime}$ | 202 | 2.92 |
| 24E8 | 20'-2" | 11'-11" | 13'-8" | $3^{\prime}-7$ " | 183 | 3.83 |
| 25E8 | 20'-11" | 12'-2" | $14^{\prime}-3^{\prime \prime}$ | $3^{\prime}-7{ }^{\prime \prime}$ | 194 | 3.99 |
| 23E13 | 21-1' | 15'-2" | 13'-1" | $5^{\prime}-10^{\prime \prime}$ | 248 | 2.23 |
| 26E9 | 21'-11" | 13'-1" | 14'-10" | $4^{\prime}-0^{\prime \prime}$ | 221 | 3.68 |
| 25E13 | $22^{\prime}-6^{\prime \prime}$ | 15'-8" | $14^{\prime}-3^{\prime \prime}$ | $5^{\prime}-10^{\prime \prime}$ | 275 | 2.43 |
| 27E10 | $23^{\prime}-0^{\prime \prime}$ | 14'-1" | 15'-5" | $4^{\prime}-6$ " | 249 | 3.43 |
| 26E13 | 23'-3" | 15'-11" | 14'-10" | $5^{\prime}-10^{\prime \prime}$ | 288 | 2.53 |
| 27E14 | 24'-4" | 16'-11" | 15'-5" | $6^{\prime}-4 \prime$ | 320 | 2.43 |
| 29E10 | 24'-6" | 14'-8" | 16'-7" | $4^{\prime}-6^{\prime \prime}$ | 275 | 3.69 |
| 30E10 | 25'-3" | 14'-11" | 17'-2" | $4^{\prime}-6^{\prime \prime}$ | 288 | 3.81 |
| 29E13 | 25'-6" | 16'-9" | 16'-7" | $5^{\prime}-10^{\prime \prime}$ | 330 | 2.82 |
| 29E15 | $26^{\prime}-2^{\prime \prime}$ | 18'-2" | 16'-7" | $6^{\prime}-9^{\prime \prime}$ | 369 | 2.44 |
| $31 \mathrm{El1}$ | 26'-4" | 15'-10" | 17'-8" | $4^{\prime}-11^{\prime \prime}$ | 320 | 3.58 |
| 32E11 | 27'-0" | 16'-2" | 18'-3" | 4'-11" | 334 | 3.69 |
| 30 E 16 | $27^{\prime}-2^{\prime \prime}$ | 19'-1" | 17'-2" | 7'-3" | 405 | 2.35 |
| 31 El 6 | 27-11" | 19'-5" | 17'-8" | $7^{\prime}-3^{\prime \prime}$ | 422 | 2.44 |
| 33E12 | 28'-1" | 17'-1" | 18'-10" | $5^{\prime}-5^{\prime \prime}$ | 369 | 3.48 |
| 34E12 | 28'-10" | 17'-5" | 19'-5" | $5^{\prime}-5^{\prime \prime}$ | 385 | 3.59 |
| 33 E 16 | 29'-5" | 19'-11" | 18'-10" | $7^{\prime}-3^{\prime \prime}$ | 455 | 2.60 |
| 34 E 16 | $30^{\prime}-2^{\prime \prime}$ | 20'-2" | 19'-5" | $7^{\prime}-3^{\prime \prime}$ | 473 | 2.68 |
| 36E12 | $30^{\prime}-4^{\prime \prime}$ | 17'-11" | 20'-7" | 5'-5" | 416 | 3.80 |
| 35E17 | $31^{\prime}-3^{\prime \prime}$ | $21^{\prime}-2^{\prime \prime}$ | 20'-0" | $7^{\prime}-9^{\prime \prime}$ | 513 | 2.59 |
| 37E13 | 31'-5" | 18'11' | 21'-2" | $5^{\prime}-10^{\prime \prime}$ | 455 | 3.60 |
| 38 E 13 | 32'-1" | $19^{\prime}-2^{\prime \prime}$ | 21'-9" | $5^{\prime}-10^{\prime \prime}$ | 472 | 3.70 |
| 36E18 | 32'-3" | 22'-2" | 20'-7" | $8^{\prime}-2^{\prime \prime}$ | 556 | 2.52 |
| 37E18 | $33^{\prime}-0^{\prime \prime}$ | 22'-5" | 21'-2" | $8^{\prime}-2^{\prime \prime}$ | 575 | 2.59 |
| 38E14 | 32'-5" | 19'-10" | 21'-9" | $6^{\prime}-4 \prime$ | 495 | 3.43 |
| 38 E 19 | $34^{\prime}-1{ }^{\prime \prime}$ | $23^{\prime}-5^{\prime \prime}$ | 21'-9" | $8^{\prime}-8^{\prime \prime}$ | 620 | 2.52 |
| $41 \mathrm{E14}$ | $34^{\prime}-8^{\prime \prime}$ | $20^{\prime}-8^{\prime \prime}$ | 23'-5" | $6^{\prime}-4 \prime$ | 549 | 3.70 |
| $41 \mathrm{E15}$ | $35^{\prime}-0^{\prime \prime}$ | $21^{\prime}-4^{\prime \prime}$ | 23'-5" | 6'-9" | 575 | 3.45 |
| $\dagger$ ¢9E20 | $35^{\prime}-2^{\prime \prime}$ | $24^{\prime}-4^{\prime \prime}$ | 22'-4" | 9'-1" | 667 | 2.45 |
| 42E16 | 36'-1" | 22'-4" | $24^{\prime}-0^{\prime \prime}$ | 7'-3" | 620 | 3.31 |
| $\dagger 44 \mathrm{E} 15$ | 37'-3" | 22'-2" | 25'-2" | 6'-9" | 632 | 3.71 |

$\dagger$ Very large or high structures sometimes call for additional special provisions for shape control during backfill. Note: Other sizes are available for special designs.


End View - Horizontal Ellipse

## SUPER-PLATE ${ }^{\circledR}$

## Aluminum Long Span Structures 9" x 2-1/2" Corrugation Specification <br> General Description

The long span aluminum structural plate structure, conforming to the dimensions shown on the plans and specifications, shall be installed at the location designated. The design and installation shall conform to AASHTO Standard Specifications for Highway Bridges, Division I, "Soil-Corrugated Metal Structure Interaction Systems", Section 12.7, "Long Span Structural Plate Structures", and Division II, Section 26, "Metal Culverts" and Division II, Section 8, "Concrete Structures".

## Materials

The aluminum structural plate shall have $9^{\prime \prime} \times 2-1 / 2^{\prime \prime}$ corrugations and shall be of the gage as shown on the plans. The plates shall be manufactured in conformance with AASHTO Specification M 219 and ASTM B 209. Bolts and nuts shall meet the provisions of ASTM A 307, Grade A and ASTM A 563, Grade A, respectively, and shall be galvanized in accordance with the requirements of ASTM A 153, Class C or B 695, Class 50. Steel anchor bolts shall conform to ASTM A 307, Grade A.

Required stiffening ribs for the crown portion shall be extruded bulb angles produced from 6061-T6 alloy providing a minimum 35 ksi yield strength.

## Long Span Special Features

Aluminum Long Span Structures will require transverse stiffening ribs as well as longitudinal stiffeners.

## Transverse Stiffeners

Transverse stiffeners will be bolted to the crown portion of the structure on $1 \mathrm{~N}\left(9.625^{\prime \prime}\right)$ maximum circumferential centers. Their size and longitudinal spacing must adequately stiffen the top portion of the crown over a minimum 55 degree arc.

## Longitudinal Structural Stiffeners (Thrust Beams)

Longitudinal stiffeners shall be located at the radius transition at the ends of the top arc. The thrust beams shall consist of reinforced concrete conforming to Division II, Section 8, Class B of the AASHTO Standard Specifications for Highway Bridges having a minimum compression strength of 2400 psi. Reinforcing steel shall conform to ASTM A 615, Grade 40, having a minimum yield strength of 40,000 psi. Black reinforcing steel shall in no instance come in contact with the Aluminum Structural Plate. Thrust beams shall be formed and poured conforming to the plan dimensions when the backfill reaches the bottom elevation of the thrust beams.

## Design

The long span structure shall be designed in accordance with the latest AASHTO design criteria and shall be required to incorporate the use of continuous longitudinal structural stiffeners (concrete thrust beams). The material supplier shall be a qualified manufacturer of steel structural plate and long span structures with a minimum of 50 successful installations. The foundation, structural backfill, and end treatment shall be as required herein and detailed on the plans.

## Structure Assembly

The structure shall be assembled in strict accordance with the manufacturer's instructions and to the design shape shown on the plans. Plates shall be assembled according to plate assembly drawings supplied by the manufacturer.

## Structural Backfill

## Material

A granular type of material shall be used around and over the structure. This select structural backfill material shall conform to one of the following classifications of soil from AASHTO Specification M-145, as modified in the following table for A-1, A-2-4 or A-2-5.

## TABLE 66. - AASHTO M-145

|  | A-1 |  | A-2(Modified) |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| GROUP CLASSIFICATION | A-1-a | A-1-b | A-2-4 | A-2-5 |


| Sieve Analysis, Percent Passing: |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| No. 10 (2.00 mm) | 50 Max. |  |  |  |
| No. 40 (0.425 mm) | 30 Max. | 50 Max. |  |  |
| No. 100 (0.150 mm) |  |  | 50 Max. | 50 Max. |
| No. 200 (0.075 mm) | 15 Max. | 25 Max. | 20 Max. | 20 Max. |
| Characteristics of Fraction Passing No. 40 (0.425 mm) |  |  |  |  |
| Liquid Limit |  |  | 40 Max. | 41 Min. |
| Plasticity Index |  |  | 10 Max. | 10 Max. |
| Usual Types of Significant | Stone Fr | gments | Silty or Clayey |  |
| Constituent Materials | Gravel | d Sand | Gravel and Sand |  |

## Additional Requirements

1. Materials must be dense graded (open graded or gap graded materials are not allowed).
2. Fine beach sands, windblown sands, and stream deposited sands, all of which exhibit fine, rounded particles and typically are classified by AASHTO M-145 as A-3 materials, are not allowed.
3. On site mixing or blending to achieve specified gradation is not allowed.

Maximum particle size shall not exceed 3 inches. For the A-2 materials, moisture content must be between - $3 \%$ and $+2 \%$ optimum as defined by AASHTO specification T-180. All soil classifications are limited to the following height of cover limits and structure shape applications:

- A-1-a material is suitable for all long span shapes, sizes and fill heights.
- A-1-b material is suitable only for use with high profile arch structures to a $12^{\prime}$ maximum fill height and for use with elliptical and low profile arch structures to a $\mathbf{2 0}^{\prime}$ maximum fill height.
- A-2-4 and A-2-5 materials are restricted to maximum heights of cover of 12'.

Other backfill materials, which provide equivalent structural properties, long-term, in the environmental conditions expected (saturation, freeze-thaw, etc.), may be used. Such materials shall be approved only after thorough investigation and testing by a soils engineer familiar with the requirements for structural backfill of long span structures.

## Backfill Envelope Limits

The backfill envelope limits are as detailed on the plans.

## Backfill Placement

Before backfilling, the erected structure shall meet the tolerance and symmetry requirements of AASHTO and the manufacturer.

Approved backfill material shall be placed in horizontal, uniform layers not exceeding $8^{\prime \prime}$ in thickness, before compaction, and shall be brought up uniformly on both sides of the structure. Each layer of backfill shall be compacted to a relative density of not less than $90 \%$, modified proctor per AASHTO Test Method specification T-180. Field density tests of compacted backfill will be made at regular intervals during backfill.

Long span structures, due to their size and shape, are sensitive to the types and weights of equipment used to place and compact the select backfill material. This is especially critical in the areas immediately adjacent to and above the structure. Therefore, equipment types will be restricted in those critical zones. Compaction equipment or methods that produce horizontal or vertical earth pressures which cause excessive distortion or damage to structures shall not be used.

Contractors should plan to have a D4 (approximately 20,000 lbs.) or similar weight tracked dozer to place and grade backfill immediately alongside and above the
structure until minimum cover level is reached. Lightweight vibratory plate or roller type compaction equipment must be used to compact the backfill in these zones. Use of heavier equipment and/or rubber tired equipment such as scrapers, graders, and front end loaders will likely be prohibited inside the select fill envelope zone until appropriate minimum cover height has been obtained.

## Shape Control Monitoring

The material supplier or the manufacturer shall provide a Shape Control Technician who is a qualified representative of a professional soils engineering firm, or other qualified organization, to ensure properly shaped structure. The Shape Control Technician shall take initial measurements of the erected structure before backfilling, observe all backfill materials and their placement, and record compaction densities. The Technician shall record all density readings and ensure they meet the requirements of the plans and specifications. However, in no case shall the relative densities be less than 90\% per AASHTO T-180. The Shape Control Technician shall monitor the structure shape during the placement of structural backfill to the minimum cover height over the structure. No structural backfill shall be placed without the Shape Control Technician on site.

## The Shape Control Technician shall:

- Monitor the structure's shape throughout the backfilling operation and report shape change rates to the contractor.
- Contact the material supplier or the manufacturer immediately if there are problems in meeting the established tolerances.
- Have full authority to stop backfill work if necessary.


## Preconstruction Conference

Prior to construction, a meeting will be held to review the construction procedures. A qualified representative of the manufacturer of the structure will be present to discuss methods and responsibility for shape monitoring and control, backfill material selection, testing and placement, and compaction methods and testing. A representative of the Engineer, Prime Contractor and any involved subcontractors must be present.

## Alternate Structures

The Contractor may furnish an alternate structure to the long span shown on the plans and these specifications but the following conditions must be met:

1. The structure must be designed using the AASHTO Long Span criteria and these plans and specifications. Steel structural plate shall conform to the requirements of AASHTO specification M167. Aluminum alloy structural plate shall conform to the requirements of AASHTO M219.
2. The corrugated metal plate thickness specified is considered the minimum acceptable for the structure(s) on this project based on structural and durability requirements. Any other structure, regardless of "special features", must be of the same thickness or greater.
3. When longitudinal reinforcements are not used, the "Special Features", such as aluminum structural ribs, shall be aluminum alloy 6061-T6. Ribs shall be placed over the same length of structure that the thrust beams would apply.
4. Alternate structures meeting the above criteria will only be considered for use if pre-approved in writing by the Engineer prior to the bid date. To qualify for pre-approval, an alternate submittal package must be submitted to the Engineer a minimum of 15 days prior to the bid date.


Aluminum Structural Plate Single Radius Arch with KeyStone Headwalls for Wetland Crossings

## BridgeCor ${ }^{\text {® }}$

## Deep Corrugation Expands Structural Plate

Structural plate has a long history of strength, durability and economy and has been a buried bridge standard for the past 80 years. Now Contech has introduced BridgeCor, a deep corrugation pattern, providing designers of bridge systems the option to use structural plate bridges with wider spans and taller rises. BridgeCor is manufactured in a $15^{\prime \prime} \mathrm{X}$ $5.5^{\prime \prime}$ corrugation pattern and Contech has improved on the manufacturing process to provide a three corrugation plate. A wider 45 inch laying length can reduce the number of plates on a project reducing the overall installed cost.

BridgeCor structures are made from sturdy, heavy gage, corrugated steel plates that are pre-formed to various shapes and sizes, then galvanized for long-term protection and performance. The plates are delivered to the job site and bolted together to form a BridgeCor structure specifically chosen for the project.

BridgeCor is available in Full Round, Single and 2-radius Arches and Box Culverts - all in a wide range of sizes. Custom shapes are also an option. The product is accepted by AASHTO and has been installed around the world.

## Superior durability

BridgeCor is similar to MULTI-PLATE and is manufactured from heavy gage steel using an industry standard of 3 ounce per square foot galvanized coating. The long history of structural plate installations have shown these designs can provide a service life of 75 years or longer.

When selecting the proper material for an application designers need to evaluate the soil side of the structure along with the corrosive and abrasive action due to the flow at the invert of the structure. The use of structural plate gives designers more structure shape options to help minimize the impact of abrasion on the invert of the structure.

## High load-carrying capacity

As a steel-soil interaction system, BridgeCor is designed to carry high combined live and dead loads. High traffic loads and deep cover applications are a structural plate specialty.

## More efficient installation process

Prefabricated plates are assembled in the field, translating into finished construction in days instead of weeks as with most cast-in-place concrete structures.

## Versatility

BridgeCor structures remove all of the shape, size and installation restrictions of precast or cast-in-place concrete.

## Descriptions of plates

BridgeCor plates are field assembled into pipe, arches, and box culverts. Corrugations of 15 -inch pitch and 5.5 -inch depth are perpendicular to the length of each plate. Each plate has a laying length of 45 inches.

Thickness. Standard specified thickness of the galvanized plates vary from 0.140 to 0.380 inches.

Widths. Standard plates come in multiples of 16 inches ( $\mathrm{S}=16$ inches or $5^{*} 3.2$ ) and are fabricated in five net covering widths, 5 S-80 inches, 6 S - 96 inches, 7 S - 112 inches, 8 S-128 inches, and 9S-144 inches, See Table 67

The "S" nomenclature translates circumference directly into nominal diameter in inches.

For example, a 54 S round structures uses six - 9 S plates ( $\mathrm{S}=16$ inches or $5 * 3.2$ )

$$
\begin{aligned}
54 \mathrm{~S} & =54 *(5 * 3.2) \\
& =270 * 3.2 \\
& =270 \mathrm{pi}
\end{aligned}
$$

Therefore, this calculates to a 270 inch ( $22^{\prime}-6^{\prime \prime}$ ) diameter round pipe. Various plate widths may be combined to obtain almost any diameter.

Lengths. BridgeCor plates are furnished in 3.75 foot nominal lengths. Actual length of the square-end structure is about three inches longer than its nominal length because a $1 \frac{1}{2}$-inch lip protrudes beyond each end of every plate for lapping purposes.

Bolt holes. BridgeCor plates are punched with 1 inch holes for 10 gage through 1 gage plates to accommodate a $3 / 4$ inch bolt. Circumferential holes are punched on 16 inch ( 1 S ) centers. All BridgeCor requires a staggered longitudinal seam. These seams have a three-hole bolt pattern in the crest and valley of the corrugations along the length of structure to help provide additional seam strength. For heavier plate structures (0.318" and $\left.0.375^{\prime \prime}\right)$, the holes are punched to $1-1 / 8$ inch diameter along the seams to accommodate a $7 / 8$ inch bolt. Bolt lengths will vary depending on the location of the bolt and the number of plates in a given location.


Guidelines

## Bolt Hole Spacing



TABLE 67. DETAILS OF UNCURVED BRIDGECOR SECTIONS

| Nominal | Net Width, <br> Inches | Overall Width, <br> Inches | Spaces <br> 16 inches | Number of <br> Circumferential <br> Bolt Holes |
| :---: | :---: | :---: | :---: | :---: |
| 5 S | 80 | 89 | 5 | 6 |
| 6 S | 96 | 105 | 6 | 7 |
| 7 S | 112 | 121 | 7 | 8 |
| 8 S | 128 | 137 | 8 | 9 |
| 9 S | 144 | 153 | 9 | 10 |

For BridgeCor, $\mathrm{S}=16$ inches.


Standard 15" x 5.5" Corrugation
Note: $5 / 16^{\prime \prime}(.318)$ and $3 / 8^{\prime \prime}(.375)$ plate shall be two corrugations ( $30^{\prime \prime}$ net length)

TABLE 68. APPROXIMATE WEIGHT OF BRIDGECOR SECTIONS

|  |  | Sheet weights, lbs. (with no fasteners) ${ }^{(1)(2)}$ |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| S | Feet | $\begin{gathered} 0.140 \\ \text { (10 Ga.) } \end{gathered}$ | $\begin{gathered} 0.170 \\ \text { (8 Ga.) } \end{gathered}$ | $\begin{gathered} 0.188 \\ (7 \mathrm{Ga} .) \end{gathered}$ | $\begin{gathered} 0.218 \\ (5 \mathrm{Ga} .) \end{gathered}$ | $\begin{gathered} 0.249 \\ (3 \mathrm{Ga} .) \end{gathered}$ | $\begin{gathered} 0.280 \\ (1 \text { Ga.) } \end{gathered}$ | $\begin{gathered} 0.318 \\ (5 / 16 \mathrm{In} .) \end{gathered}$ | $\begin{gathered} 0.375 \\ (3 / 8 \mathrm{In} .) \end{gathered}$ |
| 5 S | 3.75 | 220 | 267 | 295 | 342 | 391 | 440 | 347 | 414 |
| 6 S | 3.75 | 259 | 315 | 348 | 404 | 461 | 519 | 409 | 489 |
| 7 S | 3.75 | 299 | 363 | 401 | 465 | 531 | 598 | 471 | 563 |
| 8 S | 3.75 | 338 | 411 | 454 | 527 | 602 | 677 | 534 | 638 |
| 9 S | 3.75 | 378 | 459 | 507 | 588 | 672 | 756 | 596 | 712 |

(1) Weights are based on a zinc coating of $3 \mathrm{oz} / \mathrm{sf}$ of double-exposed surface.
(2) All weights are subject to manufacturing tolerances.
(3) Specified thickness is a nominal galvanized thickness. Reference AASHTO M 167


Unbalanced Channel Cross Section


Unbalanced Channel for BridgeCor ${ }^{\circledR}$ Arch
"Unfolded View"

## BridgeCor ${ }^{\text {® }}$ <br> Galvanized Steel Specification

Scope: This specification covers the manufacture and installation of the galvanized steel BridgeCor structure as detailed in the plans.

## I- GENERAL

### 1.0 STANDARDS AND DEFINITIONS

1.1 STANDARDS - All standards refer to latest edition unless otherwise noted.
1.1.1 ASTM A-761 "Corrugated Steel Structural Plate, Zinc Coated for Field-Bolted Pipe, Pipe-Arches and Arches" (AASHTO Designation M-167).
1.1.2 AASHTO LRFD Bridge Design Specification for Highway Bridges - Section 12.8.9.
1.1.3 AASHTO LRFD Bridge Construction Specification for Highway Bridges - Section 26.

### 1.2 DEFINITIONS

1.2.1 Owner - In these specifications the word "Owner" shall mean the site owner or the purchaser.
1.2.2 Engineer - In these specifications the word "Engineer" shall mean the Engineer of Record or Owner's designated engineering representative.
1.2.3 Manufacturer - In these specifications the word "Manufacturer" shall mean Contech Engineered Solutions, LLC 800-338-1 122.
1.2.4 Contractor - In these specifications the word "Contractor" shall mean the firm or corporation undertaking the execution of any installation work under the terms of these specifications.
1.2.5 Approved - In these specifications the word "approved" shall refer to the approval of the Engineer or his designated representative.

[^4]
### 2.0 GENERAL CONDITIONS

2.1 The Contractor shall furnish all labor, material and equipment and perform all work and services except those set out and furnished by the Owner, necessary to complete in a satisfactory manner the site preparation, excavation, filling, compaction, grading as shown on the plans and as described therein. This work shall consist of all mobilization clearing and grading, grubbing, stripping, removal of existing material unless otherwise stated, preparation of the land to be filled, filling of the land, spreading and compaction of the fill, and all subsidiary work necessary to complete the grading of the cut and fill areas to conform with the lines, grades, slopes, and specifications. This work is to be accomplished under the observation of the Owner or his designated representative.
2.2 Prior to bidding the work, the Contractor shall examine, investigate and inspect the construction site as to the nature and location of the work, and the general and local conditions at the construction site, including without limitation, the character of surface or subsurface conditions and obstacles to be encountered on and around the construction site and shall make such additional investigation as he may deem necessary for the planning and proper execution of the work.

If conditions other than those indicated are discovered by the Contractor, the Owner shall be notified immediately. The material which the Contractor believes to be a changed condition shall not be disturbed so that the owner can investigate the condition.
2.3 The construction shall be performed under the direction of the Engineer.
2.4 All aspects of the structure design and site layout including foundations, backfill, end treatments and necessary scour consideration shall be performed by the Engineer.

Any installation guidance provided herein shall be endorsed by the Engineer or superseded by the Engineer's plans and specifications.

## II - Contech BRIDGECOR [ROUND, SINGLE RADIUS ARCH, 2-radius ARCH or BOX]

### 1.0 GENERAL

1.1 Manufacturer shall fabricate the selected shape as shown on the plans. Fabrication shall conform to the requirements of ASTM A-761 and shall consist of plates, fasteners, and appurtenant items.

Plate thickness, end treatment and type of invert and foundation shall be as indicated on the plans. All manufacturing processes including corrugating, punching, curving and required galvanizing shall be performed within the United States of America.
1.2 The contractor shall verify all field dimensions and conditions prior to ordering materials.

### 2.0 DIMENSIONS

2.1 The proposed structure shall be a Contech BridgeCor with the following dimensions:

Span: $\quad X^{\prime}-Y " \quad$ Rise: $X^{\prime}-Y " \quad$ Gage: $X \quad " S "-X$
2.2 All plan dimensions on the contract drawings are measured in a true horizontal plan unless otherwise noted.

### 3.0 ASSEMBLY AND INSTALLATION

3.1 Bolts and nuts shall conform to the requirements of ASTM A-449. The Contech BridgeCor [insert shape] shall be assembled in accordance with the plate layout drawings provided by the manufacturer and per the manufacturer's recommendations.

Bolts shall be tightened using an applied torque of between 100 and 300 ft .-lbs.
3.2 The [insert structure shape] shall be installed in accordance with the plans and specifications, the manufacturer's recommendations, and AASHTO LRFD Bridge Construction Specification for Highway Bridges - Section 26.
3.3 Trench excavation shall be made in embankment material that is structurally adequate. The trench width shall be shown on the plans. Poor quality in situ embankment material must be removed and replaced with suitable backfill as directed by the Engineer.
3.4 Bedding preparation is critical to both structure performance and service life. The bed should be constructed to uniform line and grade to avoid distortions that may create undesirable stresses in the structure and/or rapid deterioration of the roadway. The bed should be free of rock formations, protruding stones, frozen lumps, roots and other foreign matter that may cause unequal settlement.
3.5 Adequate soil bearing capacity or strength shall be provided to the Engineer. Foundation details shall be provided by the Engineer.
3.6 The structure shall be assembled in accordance with the Manufacturer's instructions. All plates shall be unloaded and handled with reasonable care. Plates shall not be rolled or dragged over gravel rock and shall be prevented from striking rock or other hard objects during placement in trench or on bedding.

When assembled on a cast in place spread footing, the structure shall be assembled in the footing starting at the upstream end. When assembled on a full invert, the invert shall be placed starting at the downstream end. The structure shell shall be assembled on the invert starting at the inlet end. Circumferential seams shall be installed with the plate laps shingled downstream as viewed from the inside of the structure.

The structure shall be backfilled using clean well graded granular material that meets the requirements of AASHTO M-145 for soil classifications A-1, A-2-4, A-2-5 or A-3 according to Table 69.

Backfill must be placed symmetrically on each side of the structure in 6 to 8 inch loose lifts. Each lift shall be compacted to a minimum of 90 percent density per AASHTO T-180.
3.7 Construction loads that exceed highway load limits are not allowed to cross the structure without approval from the Engineer.
Normal highway traffic is not allowed to cross the structure until the structure has been backfilled and paved. If the road is unpaved, cover allowance to accommodate rutting shall be as directed by the Engineer.

## BridgeCor ${ }^{\circledR}$ Installation

A successful installation is dependent on these five critical components being followed:

1. Good foundation
2. Use of select structural backfill
3. $8^{\prime \prime}$ maximum thick lifts of backfill evenly placed on both sides of the structure
4. Adequate compaction of backfill
5. Adequate minimum cover over the structure

## Required elements

Satisfactory site preparation, trench excavation and bedding and backfill operations are essential to develop the strength of any flexible conduit. In order to obtain proper strength while preventing settlement, it is necessary that the soil envelope around the structure be of good granular material, properly placed, and carefully compacted.

A qualified Engineer should be engaged to design a proper foundation, adequate bedding, and backfill.

## DURING INSTALLATION AND PRIOR TO THE CONSTRUCTION OF PERMANENT EROSION CONTROL AND END TREATMENT PROTECTION, SPECIAL PRECAUTIONS MAY BE NECESSARY. THE STRUCTURE MUST BE PROTECTED FROM UNBALANCED LOADS AND FROM ANY STRUCTURAL LOADS OR HYDRAULIC FORCES THAT MAY BEND OR DISTORT THE UNSUPPORTED ENDS OF THE STRUCTURE. EROSION OR WASH OUT OF PREVIOUSLY PLACED SOIL SUPPORT MUST BE PREVENTED TO ENSURE THAT THE STRUCTURE MAINTAINS ITS LOAD CAPACITY.

## Trench excavation

If the adjacent embankment material is structurally adequate, the trench requires only a bottom clear width of the structure's span plus sufficient room for compaction equipment.

## Bedding

Proper bedding preparation is critical to both structure performance and service life. The bed should be constructed to avoid distortions that may create undesirable stresses in the structure and/or rapid deterioration of the roadway. The bed should be free of rock formations, protruding stones, and frozen matter that may cause unequal settlement.

It is recommended that the bedding be stable, well graded granular material. Placing the structure on the bedding surface is generally accomplished by one of the two following methods:

- Shaping the bedding surface to conform to the lower section of the structure
- Carefully tamping a granular or select material beneath the haunches to achieve a well-compacted condition

Using one of these two methods ensures satisfactory compaction beneath the haunches.

## Backfill

Satisfactory backfill material, proper placement and compaction are key factors in obtaining maximum strength and stability.

The backfill material should be free of rocks, frozen lumps, and foreign material that can cause hard spots or decompose to create voids. Backfill material should be well graded granular material that meets the requirements of AASHTO M 145 for soil classifications A-1, A-2, or A-3. Backfill must be placed symmetrically on each side of the structure in six-inch loose lifts. Each lift is to be compacted to a minimum of 90 percent density per AASHTO T 180.

A high percentage of silt or fine sand in the native soils suggests the need for a well graded granular backfill material to prevent soil migration.

During backfill, only small tracked vehicles (D-4 or smaller) should be near the structure as fill progresses above the crown and to the finished grade. The Engineer and Contractor are cautioned that the minimum cover may need to be increased to handle temporary construction vehicle loads (larger than D-4).

For more information, refer to ASTM A 807 and AASHTO LRFD Bridge Construction Specifications for Highway Bridges Div. II - Construction Section 26.

## Bolting

If the plates are well aligned, the torque applied with a power wrench need not be excessive. Bolts should be torque initially to a minimum 100 foot pounds and a maximum 300 foot pounds. A good plate fit is far better than high torque.

Complete detailed assembly instructions and drawings are provided with each structure.


TABLE 69. BRIDGECOR GROUP CLASSIFICATION

| TABLE 69. BRIDGECOR GROUP CLASSIFICATION |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| GROUP CLASSIFICATION | A-1-a | A-1-b | A-2-4 | A-2-5 | A-3 |
| Sieve Analysis Percent Passing |  |  |  |  |  |
| No. 10 (2.000 mm) | 50 max. | ---- | ---- | ---- | ---- |
| No. 40 (0.425 mm) | 30 max. | 50 max. | ---- | ---- | 51 max. |
| No. 100 (0.150 mm) | ---- | ---- | 50 max. | 50 max. | ---- |
| No. 200 (0.075 mm) | 15 max. | 25 max. | 20 max. | 20 max. | 10 max. |
| Atterberg Limits for Fraction Passing No. 40 (0.425 mm) |  |  |  |  |  |
| Liquid Limits | ---- | ---- | 40 max. | 41 max. | ---- |
| Plasticity Index | 6 max. | 6 max. | 10 max. | 10 max. | Non-Plastic |
| Usual Materials | Stone Fragment, Gravel and Sand |  | Silty or Clayey Gravel and Sand |  | Coarse Sand |

NOTE: Atterberg Limits are modified to provide material that are primarily granular


TABLE 70. BRIDGECOR BOX CULVERT $15^{" 1} \times 51 / 2^{" 1}$
LRFD HEIGHT OF COVER GUIDE

| Dimensions to Inside Corrugation |  |  |  | Gage Thickness (Inches) - Height of Cover Shown in Feet Maximum Height of Cover (Minimum Height of Cover) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Shape | Bottom Span (Ft.-In.) | $\begin{gathered} \text { Rise } \\ \text { (Ft.-In.) } \end{gathered}$ | Approx. Area (Sq. Ft.) | $\begin{gathered} 10 \\ (0.140) \end{gathered}$ | $\begin{gathered} 8 \\ (0.170) \end{gathered}$ | $\begin{gathered} 7 \\ (0.188) \end{gathered}$ | $\begin{gathered} 5 \\ (0.218) \end{gathered}$ | $\begin{gathered} 3 \\ (0.249) \end{gathered}$ | $\begin{gathered} 1 \\ (0.280) \end{gathered}$ | $\begin{gathered} 5 / 16 \\ (0.318) \end{gathered}$ | $\begin{gathered} 3 / 8 \\ (0.380) \end{gathered}$ | Select Fill <br> Width (ft.) | Precon (min Level) |
| 1 | 17-6 | 6-10 | 98.9 | $\begin{gathered} 11 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 13 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 14 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 16 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 17 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 19 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 21 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 25 \\ (1.5) \\ \hline \end{gathered}$ | 8.0 | 1 |
| 2 | 17-7 | 8-2 | 122.2 | $\begin{gathered} 11 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 13 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 14 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 15 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 17 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 19 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 21 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 24 \\ (1.5) \\ \hline \end{gathered}$ | 8.0 | 1 |
| 3 | 17-9 | 9-6 | 145.7 | $\begin{gathered} 11 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 13 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 14 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 15 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 17 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 19 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 21 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 24 \\ (1.5) \\ \hline \end{gathered}$ | 8.0 | 1 |
| 4 | 17-10 | 10-10 | 169.4 | $\begin{gathered} 11 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 13 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 13 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 15 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 17 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 18 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 21 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 24 \\ (1.5) \\ \hline \end{gathered}$ | 8.0 | 1 |
| 5 | 18-10 | 7-0 | 108.4 | $\begin{gathered} 10 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 11 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 12 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 14 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 15 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 17 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 19 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 22 \\ (1.5) \\ \hline \end{gathered}$ | 8.0 | 1 |
| 6 | 18-11 | 8-4 | 133.5 | $\begin{gathered} 10 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 11 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 12 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 14 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 15 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 17 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 19 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 22 \\ (1.5) \\ \hline \end{gathered}$ | 8.0 | 1 |
| 7 | 19-1 | 9-8 | 158.8 | $\begin{gathered} 10 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 11 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 12 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 14 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 15 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 17 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 18 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 22 \\ (1.5) \\ \hline \end{gathered}$ | 8.0 | 1 |
| 8 | 19-3 | 11-0 | 184.4 | $\begin{gathered} 10 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 11 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 12 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 13 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 15 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 16 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 18 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 21 \\ (1.5) \\ \hline \end{gathered}$ | 8.0 | 1 |
| 9 | 20-4 | 8-6 | 145.1 | $\begin{gathered} 9 \\ (3.0) \end{gathered}$ | $\begin{gathered} 10 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 11 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 12 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 14 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 15 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 17 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 19 \\ (1.5) \\ \hline \end{gathered}$ | 8.0 | 1 |
| 10 | 20-5 | 9-10 | 172.2 | $\begin{gathered} 9 \\ (3.5) \end{gathered}$ | $\begin{gathered} 10 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 11 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 12 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 13 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 15 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 16 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 19 \\ (2.0) \\ \hline \end{gathered}$ | 8.0 | 1 |
| 11 | 20-7 | 11-1 | 199.5 | $\begin{gathered} 8 \\ (3.5) \\ \hline \end{gathered}$ | $\begin{gathered} 10 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 11 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 12 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 13 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 15 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 16 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 19 \\ (2.0) \\ \hline \end{gathered}$ | 8.0 | 1 |
| 12 | 21-6 | 7-3 | 128.2 | $\begin{gathered} 8 \\ (3.5) \\ \hline \end{gathered}$ | $\begin{gathered} 9 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 10 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 11 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 12 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 13 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 15 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 17 \\ (2.0) \\ \hline \end{gathered}$ | 8.0 | 1 |
| 13 | 21-8 | 8-7 | 156.9 | $\begin{gathered} 8 \\ (3.5) \end{gathered}$ | $\begin{gathered} 9 \\ (3.0) \end{gathered}$ | $\begin{gathered} 10 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 11 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 12 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 13 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 15 \\ (2.0) \end{gathered}$ | $\begin{gathered} 17 \\ (2.0) \end{gathered}$ | 8.0 | 1 |
| 14 | 21-10 | 9-11 | 185.8 | $\begin{gathered} 8 \\ (3.5) \\ \hline \end{gathered}$ | $\begin{gathered} 9 \\ (3.0) \end{gathered}$ | $\begin{gathered} 9 \\ (2.5) \end{gathered}$ | $\begin{gathered} 11 \\ (2.5) \end{gathered}$ | $\begin{gathered} 12 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 13 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 15 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 17 \\ (2.0) \\ \hline \end{gathered}$ | 8.0 | 1 |
| 15 | 22-5 | 11-3 | 214.9 | $\begin{gathered} 8 \\ (3.5) \\ \hline \end{gathered}$ | $\begin{gathered} 9 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 9 \\ (2.5) \end{gathered}$ | $\begin{gathered} 10 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 12 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 13 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 14 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 17 \\ (2.0) \\ \hline \end{gathered}$ | 8.0 | 1 |
| 16 | 22-9 | 7-5 | 138.5 | $\begin{gathered} 7 \\ (3.5) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 9 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 10 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 11 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 12 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 13 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 15 \\ (2.0) \\ \hline \end{gathered}$ | 8.0 | 1 |
| 17 | 22-11 | 8-9 | 168.9 | $\begin{gathered} 7 \\ (3.5) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 9 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 10 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 11 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 12 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 13 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 15 \\ (2.0) \\ \hline \end{gathered}$ | 8.0 | 1 |
| 18 | 23-2 | 10-1 | 199.5 | $\begin{gathered} 7 \\ (3.5) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 9 \\ (2.5) \end{gathered}$ | $\begin{gathered} 11 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 12 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 13 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 15 \\ (2.0) \\ \hline \end{gathered}$ | 8.0 | 1 |
| 19 | 23-4 | 11-5 | 230.5 | $\begin{gathered} 7 \\ (3.5) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 9 \\ (2.5) \end{gathered}$ | $\begin{gathered} 10 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 11 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 13 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 15 \\ (2.0) \\ \hline \end{gathered}$ | 8.0 | 1 |
| 20 | 24-1 | 7-7 | 149.1 |  | $\begin{gathered} 7 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 9 \\ (2.5) \end{gathered}$ | $\begin{gathered} 10 \\ (2.5) \end{gathered}$ | $\begin{gathered} 11 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 12 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 14 \\ (2.0) \\ \hline \end{gathered}$ | 8.0 | 2 |
| 21 | 24-3 | 8-7 | 167.7 |  | $\begin{gathered} 7 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 9 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 9 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 10 \\ (1.5) \\ \hline \end{gathered}$ | $\begin{gathered} 12 \\ (1.5) \\ \hline \end{gathered}$ | $\begin{gathered} 14 \\ (1.5) \\ \hline \end{gathered}$ | 8.0 | 2 |
| 22 | 24-3 | 8-11 | 181.3 | $\begin{gathered} 7 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 9 \\ (3.0) \end{gathered}$ | $\begin{gathered} 9 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 10 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 11 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 12 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 14 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 16 \\ (2.0) \\ \hline \end{gathered}$ | 8.0 | 2 |
| 23 | 24-5 | 9-11 | 200.1 | $\begin{gathered} 7 \\ (3.5) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 9 \\ (2.5) \end{gathered}$ | $\begin{gathered} 10 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 11 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 12 \\ (1.5) \\ \hline \end{gathered}$ | $\begin{gathered} 14 \\ (1.5) \\ \hline \end{gathered}$ | $\begin{gathered} 16 \\ (1.5) \\ \hline \end{gathered}$ | 8.0 | 2 |
| 24 | 24-5 | 10-3 | 213.7 |  | $\begin{gathered} 7 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.5) \\ \hline \end{gathered}$ | 9 (2.5) | $\begin{gathered} 10 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 11 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 13 \\ (2.0) \\ \hline \end{gathered}$ | 8.0 | 2 |
| 25 | 24-6 | 11-3 | 232.7 | $\begin{gathered} 7 \\ (3.5) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 9 \\ (2.5) \end{gathered}$ | $\begin{gathered} 10 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 11 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 12 \\ (1.5) \\ \hline \end{gathered}$ | $\begin{gathered} 14 \\ (1.5) \\ \hline \end{gathered}$ | $\begin{gathered} 16 \\ (1.5) \\ \hline \end{gathered}$ | 8.0 | 2 |
| 26 | 24-8 | 11-7 | 246.3 |  | $\begin{gathered} 7 \\ (3.5) \\ \hline \end{gathered}$ | $\begin{gathered} 7 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 9 \\ (2.5) \end{gathered}$ | $\begin{gathered} 10 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 11 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 13 \\ (2.0) \\ \hline \end{gathered}$ | 8.0 | 2 |
| 27 | 24-8 | 12-7 | 265.4 | $\begin{gathered} 7 \\ (3.5) \end{gathered}$ | $\begin{gathered} 8 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 9 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 10 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 11 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 12 \\ (1.5) \\ \hline \end{gathered}$ | $\begin{gathered} 13 \\ (1.5) \\ \hline \end{gathered}$ | $\begin{gathered} 16 \\ (1.5) \\ \hline \end{gathered}$ | 8.0 | 2 |

Notes:

1. Not for a specific structural design. Use for budget estimating only. A CANDE analysis is required for final design and quotation.
2. The above table is based upon the minimum requirements of the AASHTO LRFD Design Specification, Section 12, and:
a. Backfill material per AASHTO M145, class A-2-5 or better.
b. Backfill 120 pcf in density and compacted to $90 \%$ modified proctor.
c. The minimum cover is per article 12.8.9.4
d. The minimum select backfill width (six to eight feet) is measured from outside the maximum span on each side of the structure.

This width only applies when the material adjacent to the select zone is determined to be competent, well consolidated material.
3. Select backfill width may increase for situations where lower strength fill exists in either the select fill zone or the adjacent embankment zone.
4. This estimate is for single barrel structures. For multiple barrels, more investigation is required.

TABLE 71. BRIDCECOR BOX CULVERT 15"X 5 5/2"
LRFD HEIGHT OF COVER GUIDE

|  |  |  |  |  |  | EIGHI | COVER | DE |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Dimensions to Inside Corrugation |  |  |  | Gage Thickness (Inches) - Height of Cover Shown in Feet Maximum Height of Cover (Minimum Height of Cover) |  |  |  |  |  |  |  |  |  |
| Shape | Bottom Span (Ft.-In.) | $\begin{gathered} \text { Rise } \\ \text { (Ft.-In.) } \end{gathered}$ | Approx. Area (Sq. Ft.) | $\begin{gathered} 10 \\ (0.140) \end{gathered}$ | $\begin{gathered} 8 \\ (0.170) \end{gathered}$ | $\begin{gathered} 7 \\ (0.188) \end{gathered}$ | $\begin{gathered} 5 \\ (0.218) \end{gathered}$ | $\begin{gathered} 3 \\ (0.249) \end{gathered}$ | $\begin{gathered} 1 \\ (0.280) \end{gathered}$ | $\begin{gathered} 5 / 16 \\ (0.318) \end{gathered}$ | $\begin{gathered} 3 / 8 \\ (0.380) \end{gathered}$ | Select Fill Width (Ft.) | Precon (Min Level) |
| 28 | 24-11 | 8-0 | 162.4 |  | $\begin{gathered} 7 \\ (3.5) \\ \hline \end{gathered}$ | $\begin{gathered} 7 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 9 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 10 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 11 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 13 \\ (2.0) \\ \hline \end{gathered}$ | 8.0 | 2 |
| 29 | 25-7 | 9-1 | 193.8 |  | $\begin{gathered} 6 \\ (3.5) \\ \hline \end{gathered}$ | $\begin{gathered} 7 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 9 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 10 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 12 \\ (2.0) \\ \hline \end{gathered}$ | 6.0 | 2 |
| 30 | 25-8 | 8-8 | 179.3 | $\begin{gathered} 7 \\ (3.5) \end{gathered}$ | $\begin{gathered} 8 \\ (3.0) \end{gathered}$ | $\begin{gathered} 8 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 9 \\ (2.5) \end{gathered}$ | $\begin{gathered} 10 \\ (2.0) \end{gathered}$ | $\begin{gathered} 11 \\ (2.0) \end{gathered}$ | $\begin{gathered} 12 \\ (1.5) \end{gathered}$ | $\begin{gathered} 14 \\ (1.5) \\ \hline \end{gathered}$ | 8.0 | 2 |
| 31 | 25-10 | 10-0 | 213.7 | $\begin{gathered} 7 \\ (3.5) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 9 \\ (2.5) \end{gathered}$ | $\begin{gathered} 10 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 11 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 12 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 14 \\ (1.5) \\ \hline \end{gathered}$ | 8.0 | 2 |
| 32 | 26-0 | 11-4 | 258.2 | $\begin{gathered} 7 \\ (3.5) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 9 \\ (2.5) \end{gathered}$ | $\begin{gathered} 10 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 11 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 12 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 14 \\ (1.5) \\ \hline \end{gathered}$ | 8.0 | 2 |
| 33 | 26-2 | 12-8 | 283.0 | $\begin{gathered} 7 \\ (3.5) \\ \hline \end{gathered}$ | $\begin{gathered} 7 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 9 \\ (2.5) \end{gathered}$ | $\begin{gathered} 10 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 11 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 12 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 14 \\ (1.5) \\ \hline \end{gathered}$ | 8.0 | 2 |
| 34 | 26-4 | 9-6 | 208.7 |  | $\begin{gathered} 6 \\ (3.5) \\ \hline \end{gathered}$ | $\begin{gathered} 6 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 7 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 9 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 10 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 11 \\ (2.0) \\ \hline \end{gathered}$ | 6.0 | 2 |
| 35 | 26-5 | 10-10 | 243.8 |  | $\begin{gathered} 6 \\ (3.5) \\ \hline \end{gathered}$ | $\begin{gathered} 6 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 7 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 9 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 10 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 11 \\ (2.0) \\ \hline \end{gathered}$ | 6.0 | 2 |
| 36 | 26-6 | 12-2 | 278.2 |  |  | $\begin{gathered} 6 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 7 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 9 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 10 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 11 \\ (2.0) \\ \hline \end{gathered}$ | 6.0 | 2 |
| 37 | 27-1 | 8-10 | 191.3 | $\begin{gathered} 6 \\ (3.5) \\ \hline \end{gathered}$ | $\begin{gathered} 7 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 7 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 9 \\ (2.0) \end{gathered}$ | $\begin{gathered} 10 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 11 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 13 \\ (1.5) \\ \hline \end{gathered}$ | 8.0 | 2 |
| 38 | 27-3 | 10-2 | 226.7 | $\begin{gathered} 6 \\ (3.5) \\ \hline \end{gathered}$ | $\begin{gathered} 7 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 7 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 9 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 10 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 11 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 13 \\ (2.0) \\ \hline \end{gathered}$ | 8.0 | 2 |
| 39 | 27-5 | 11-6 | 263.0 |  | $\begin{gathered} 7 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 7 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 9 \\ (2.0) \end{gathered}$ | $\begin{gathered} 10 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 11 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 13 \\ (2.0) \\ \hline \end{gathered}$ | 8.0 | 2 |
| 40 | 27-6 | 8-4 | 185.3 |  |  | $\begin{gathered} 6 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 7 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 7 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 9 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 10 \\ (2.0) \\ \hline \end{gathered}$ | 6.0 | 3 |
| 41 | 27-7 | 12-10 | 299.6 |  | $\begin{gathered} 8 \\ (3.0) \end{gathered}$ | $\begin{gathered} 8 \\ (3.0) \end{gathered}$ | $\begin{gathered} 9 \\ (2.5) \end{gathered}$ | $\begin{gathered} 10 \\ (2.0) \end{gathered}$ | $\begin{gathered} 10 \\ (2.0) \end{gathered}$ | $\begin{gathered} 11 \\ (2.0) \end{gathered}$ | $\begin{gathered} 13 \\ (2.0) \end{gathered}$ | 8.0 | 2 |
| 42 | 27-9 | 11-0 | 259.0 |  |  | $\begin{gathered} 6 \\ (3.5) \\ \hline \end{gathered}$ | $\begin{gathered} 6 \\ (3.0) \end{gathered}$ | $\begin{gathered} 7 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 9 \\ (2.0) \end{gathered}$ | $\begin{gathered} 10 \\ (2.0) \\ \hline \end{gathered}$ | 6.0 | 3 |
| 43 | 27-11 | 12-4 | 296.0 |  |  | $\begin{gathered} 6 \\ (3.5) \\ \hline \end{gathered}$ | $\begin{gathered} 6 \\ (3.0) \end{gathered}$ | $\begin{gathered} 7 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 10 \\ (2.0) \\ \hline \end{gathered}$ | 6.0 | 3 |
| 44 | 28-2 | 9-5 | 219.8 |  |  | $\begin{gathered} 6 \\ (3.5) \\ \hline \end{gathered}$ | $\begin{gathered} 6 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 7 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 10 \\ (2.0) \\ \hline \end{gathered}$ | 6.0 | 3 |
| 45 | 28-6 | 9-0 | 203.4 |  | $\begin{gathered} 6 \\ (3.0) \end{gathered}$ | $\begin{gathered} 7 \\ (3.0) \end{gathered}$ | $\begin{gathered} 7 \\ (2.5) \end{gathered}$ | $\begin{gathered} 8 \\ (2.0) \end{gathered}$ | $\begin{gathered} 9 \\ (2.0) \end{gathered}$ | $\begin{gathered} 10 \\ (2.0) \end{gathered}$ | $\begin{gathered} 12 \\ (2.0) \end{gathered}$ | 8.0 | 2 |
| 46 | 28-8 | 10-4 | 241.4 |  | $\begin{gathered} 6 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 7 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 7 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 9 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 10 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 11 \\ (2.0) \\ \hline \end{gathered}$ | 8.0 | 2 |
| 47 | 28-10 | 8-6 | 197.2 |  |  | $\begin{gathered} 5 \\ (3.5) \\ \hline \end{gathered}$ | $\begin{gathered} 6 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 7 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 7 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 9 \\ (2.0) \\ \hline \end{gathered}$ | 6.0 | 3 |
| 48 | 28-11 | 11-8 | 279.7 |  | $\begin{gathered} 6 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 7 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 7 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 9 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 10 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 11 \\ (2.0) \\ \hline \end{gathered}$ | 8.0 | 2 |
| 49 | 29-1 | 11-2 | 274.4 |  |  | $\begin{gathered} 5 \\ (3.5) \\ \hline \end{gathered}$ | $\begin{gathered} 6 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 6 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 7 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 9 \\ (2.0) \\ \hline \end{gathered}$ | 6.0 | 3 |
| 50 | 29-1 | 13-0 | 318.3 |  | $\begin{gathered} 6 \\ (3.5) \\ \hline \end{gathered}$ | $\begin{gathered} 6 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 7 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 9 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 10 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 11 \\ (2.0) \\ \hline \end{gathered}$ | 8.0 | 2 |
| 51 | 29-3 | 12-6 | 313.2 |  |  |  | $\begin{gathered} 6 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 6 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 7 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 9 \\ (2.0) \\ \hline \end{gathered}$ | 6.0 | 3 |
| 52 | 29-6 | 9-7 | 233.2 |  |  |  | $\begin{gathered} 6 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 6 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 7 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 9 \\ (2.0) \\ \hline \end{gathered}$ | 8.0 | 3 |
| 53 | 29-10 | 9-1 | 215.8 |  | $\begin{gathered} 6 \\ (3.5) \\ \hline \end{gathered}$ | $\begin{gathered} 6 \\ (3.0) \end{gathered}$ | $\begin{gathered} 7 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.5) \end{gathered}$ | $\begin{gathered} 8 \\ (2.0) \end{gathered}$ | $\begin{gathered} 9 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 11 \\ (2.0) \end{gathered}$ | 8.0 | 2 |

Notes:

1. Not for a specific structural design. Use for budget estimating only. A CANDE analysis is required for final design and quotation.
2. The above table is based upon the minimum requirements of the AASHTO LRFD Design Specification, Section 12, and:
a. Backfill material per AASHTO M145, class A-2-5 or better.
b. Backfill 120 pcf in density and compacted to $90 \%$ modified proctor.
c. The minimum cover is per article 12.8.9.4
d. The minimum select backfill width (six to eight feet) is measured from outside the maximum span on each side of the structure.

This width only applies when the material adjacent to the select zone is determined to be competent, well consolidated material.
3. Select backfill width may increase for situations where lower strength fill exists in either the select fill zone or the adjacent embankment zone.
4. This estimate is for single barrel structures. For multiple barrels, more investigation is required.

TABLE 72. BRIDGECOR BOX CULVERT $15^{\prime \prime} \times 5$ ¹/2"
LRFD HEIGHT OF COVER GUIDE

| LRFD HEIGHT OF COVER GUIDE |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Dimensions to Inside Corrugation |  |  |  | Gage Thickness (Inches) - Height of Cover Shown in Feet Maximum Height of Cover (Minimum Height of Cover) |  |  |  |  |  |  |  |  |  |
| Shape | Bottom Span (Ft.-In.) | $\begin{gathered} \text { Rise } \\ \text { (Ft.-In.) } \end{gathered}$ | Approx. Area (Sq. Ft.) | $\begin{gathered} 10 \\ (0.140) \end{gathered}$ | $\begin{gathered} 8 \\ (0.170) \end{gathered}$ | $\begin{gathered} 7 \\ (0.188) \end{gathered}$ | $\begin{gathered} 5 \\ (0.218) \end{gathered}$ | $\begin{gathered} 3 \\ (0.249) \end{gathered}$ | $\begin{gathered} 1 \\ (0.280) \end{gathered}$ | $\begin{gathered} 5 / 16 \\ (0.318) \end{gathered}$ | $\begin{gathered} 3 / 8 \\ (0.380) \end{gathered}$ | Select Fill Width (ft.) | Precon (Min Level) |
| 54 | 30-1 | 10-5 | 255.6 |  | $\begin{gathered} 6 \\ (3.5) \\ \hline \end{gathered}$ | $\begin{gathered} 6 \\ (3.0) \end{gathered}$ | $\begin{gathered} 7 \\ (2.5) \end{gathered}$ | $\begin{gathered} 7 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 9 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 10 \\ (2.0) \\ \hline \end{gathered}$ | 8.0 | 2 |
| 55 | 30-4 | 11-9 | 295.7 |  | $\begin{gathered} 6 \\ (3.5) \\ \hline \end{gathered}$ | $\begin{gathered} 6 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 7 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 7 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 9 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 10 \\ (2.0) \\ \hline \end{gathered}$ | 8.0 | 2 |
| 56 | 30-5 | 11-3 | 290.0 |  |  |  | 5 (3.0) | $\begin{gathered} 6 \\ (2.5) \end{gathered}$ | $\begin{gathered} 6 \\ (2.5) \end{gathered}$ | $\begin{gathered} 7 \\ (2.0) \end{gathered}$ | $\begin{gathered} 8 \\ (2.0) \\ \hline \end{gathered}$ | 8.0 | 3 |
| 57 | 30-7 | 12-7 | 330.6 |  | $\begin{gathered} 5 \\ (3.5) \\ \hline \end{gathered}$ | $\begin{gathered} 6 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 6 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 7 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 9 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 10 \\ (2.0) \\ \hline \end{gathered}$ | 8.0 | 3 |
| 58 | 30-7 | 13-1 | 336.2 |  |  |  | $\begin{gathered} 5 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 6 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 6 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 7 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.0) \\ \hline \end{gathered}$ | 8.0 | 3 |
| 59 | 30-7 | 8-5 | 206.1 |  |  |  | $\begin{gathered} 5 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 6 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 6 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 7 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.0) \\ \hline \end{gathered}$ | 8.0 | 3 |
| 60 | 30-8 | 9-7 | 232.3 |  | $\begin{gathered} 5 \\ (3.5) \\ \hline \end{gathered}$ | $\begin{gathered} 6 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 6 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 7 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 9 \\ (2.0) \end{gathered}$ | $\begin{gathered} 10 \\ (2.0) \end{gathered}$ | 8.0 | 2 |
| 61 | 30-9 | 10-11 | 272.4 |  | $\begin{gathered} 5 \\ (3.5) \\ \hline \end{gathered}$ | $\begin{gathered} 6 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 6 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 7 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 9 \\ (2.0) \end{gathered}$ | $\begin{gathered} 10 \\ (2.0) \end{gathered}$ | 8.0 | 2 |
| 62 | 30-11 | 12-2 | 313.4 |  |  | $\begin{gathered} 6 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 6 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 7 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 10 \\ (2.0) \end{gathered}$ | 8.0 | 3 |
| 63 | 31-0 | 13-6 | 354.6 |  |  | $\begin{gathered} 6 \\ (3.0) \end{gathered}$ | $\begin{gathered} 6 \\ (3.0) \end{gathered}$ | $\begin{gathered} 7 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 10 \\ (2.0) \end{gathered}$ | 8.0 | 3 |
| 64 | 31-6 | 8-9 | 221.7 |  |  |  | $\begin{gathered} 5 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 6 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 6 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 7 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.0) \\ \hline \end{gathered}$ | 8.0 | 3 |
| 65 | 31-9 | 11-5 | 305.9 |  |  |  | $\begin{gathered} 5 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 6 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 6 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 7 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.0) \\ \hline \end{gathered}$ | 8.0 | 3 |
| 66 | 32-0 | 9-8 | 245.5 |  |  | $\begin{gathered} 5 \\ (3.5) \\ \hline \end{gathered}$ | $\begin{gathered} 6 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 7 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 7 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 9 \\ (2.0) \\ \hline \end{gathered}$ | 8.0 | 3 |
| 67 | 32-2 | 11-0 | 288.2 |  |  | $\begin{gathered} 5 \\ (3.5) \end{gathered}$ | $\begin{gathered} 6 \\ (3.0) \end{gathered}$ | $\begin{gathered} 6 \\ (2.5) \end{gathered}$ | $\begin{gathered} 7 \\ (2.5) \end{gathered}$ | $\begin{gathered} 8 \\ (2.0) \end{gathered}$ | $\begin{gathered} 9 \\ (2.0) \end{gathered}$ | 8.0 | 3 |
| 68 | 32-4 | 12-4 | 331.1 |  |  | $\begin{gathered} 5 \\ (3.5) \\ \hline \end{gathered}$ | $\begin{gathered} 6 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 6 \\ (3.0) \end{gathered}$ | $\begin{gathered} 7 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 9 \\ (2.0) \end{gathered}$ | 8.0 | 3 |
| 69 | 32-6 | 13-8 | 374.3 |  |  | $\begin{gathered} 5 \\ (3.5) \\ \hline \end{gathered}$ | $\begin{gathered} 6 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 6 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 7 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 9 \\ (2.0) \\ \hline \end{gathered}$ | 8.0 | 3 |
| 70 | 33-5 | 9-10 | 258.8 |  |  |  | $\begin{gathered} 6 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 6 \\ (3.0) \end{gathered}$ | $\begin{gathered} 7 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 7 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.0) \\ \hline \end{gathered}$ | 8.0 | 3 |
| 71 | 33-7 | 11-2 | 303.4 |  |  |  | $\begin{gathered} 5 \\ (3.0) \end{gathered}$ | $\begin{gathered} 6 \\ (3.0) \end{gathered}$ | $\begin{gathered} 7 \\ (2.5) \end{gathered}$ | $\begin{gathered} 7 \\ (2.5) \end{gathered}$ | $\begin{gathered} 8 \\ (2.0) \end{gathered}$ | 8.0 | 3 |
| 72 | 33-9 | 12-6 | 348.2 |  |  |  | $\begin{gathered} 5 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 6 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 6 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 7 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.0) \\ \hline \end{gathered}$ | 8.0 | 3 |
| 73 | 34-0 | 13-10 | 393.2 |  |  |  | $\begin{gathered} 5 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 6 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 6 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 7 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.0) \\ \hline \end{gathered}$ | 8.0 | 3 |
| 74 | 34-9 | 10-0 | 272.5 |  |  |  | $\begin{gathered} 5 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 6 \\ (3.0) \end{gathered}$ | $\begin{gathered} 6 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 7 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.0) \\ \hline \end{gathered}$ | 8.0 | 3 |
| 75 | 34-11 | 11-3 | 317.9 |  |  |  | $\begin{gathered} 5 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 6 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 6 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 7 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.0) \\ \hline \end{gathered}$ | 8.0 | 3 |
| 76 | 35-2 | 12-7 | 364.4 |  |  |  | $\begin{gathered} 5 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 6 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 6 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 7 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.0) \\ \hline \end{gathered}$ | 8.0 | 3 |
| 77 | 35-4 | 13-11 | 411.3 |  |  |  | $\begin{gathered} 5 \\ (3.0) \end{gathered}$ | $\begin{gathered} 6 \\ (3.0) \\ \hline \end{gathered}$ | $\begin{gathered} 6 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 7 \\ (2.5) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (2.0) \\ \hline \end{gathered}$ | 8.0 | 3 |
| CUSTOM | UP TO 45' | VARIES |  |  |  |  | VAR |  |  |  |  | INQUIRE | INQUIRE |

Notes:

1. Not for a specific structural design. Use for budget estimating only. A CANDE analysis is required for final design and quotation.
2. The above table is based upon the minimum requirements of the AASHTO LRFD Design Specification, Section 12, and:
a. Backfill material per AASHTO M145, class A-2-5 or better.
b. Backfill 120 pcf in density and compacted to $90 \%$ modified proctor.
c. The minimum cover is per article 12.8.9.4
d. The minimum select backfill width (six to eight feet) is measured from outside the maximum span on each side of the structure.

This width only applies when the material adjacent to the select zone is determined to be competent, well consolidated material.
3. Select backfill width may increase for situations where lower strength fill exists in either the select fill zone or the adjacent embankment zone.
4. This estimate is for single barrel structures. For multiple barrels, more investigation is required.

TABLE 73. BRIDGECOR BOX CULVERT $15^{\prime \prime} \times 51 / 2^{\prime \prime}$

## WEIGHT TABLES

|  |  |  |  |  |  |  | GHT TAB |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Dimensions to Inside Corrugation |  |  |  | Gage Thickness (Inches) <br> Weight Shown as per Foot of Structure |  |  |  |  |  |  |  | Plate Make-Up |  |  |  |  |  |
| Structure Number | Total S | Bottom Span (Ft.-ln.) | $\begin{gathered} \text { Rise } \\ \text { (Ft.-In.) } \end{gathered}$ | $\begin{gathered} 10 \\ (0.140) \end{gathered}$ | $\begin{gathered} 8 \\ (0.170) \end{gathered}$ | $\begin{gathered} 7 \\ (0.188) \end{gathered}$ | $\begin{gathered} 5 \\ (0.218) \end{gathered}$ | $\begin{gathered} 3 \\ (0.249) \end{gathered}$ | $\begin{gathered} 1 \\ (0.280) \end{gathered}$ | $\begin{gathered} 5 / 16 \\ (0.318) \end{gathered}$ | $\begin{gathered} 3 / 8 \\ (0.380) \end{gathered}$ | 9 S | 8 S | 7 S | 6 S | 5 S | Total Plates |
| 1 | 19 | 17-6 | 6-10 | 226 | 273 | 301 | 348 | 396 | 445 | 530 | 631 |  |  | 1 | 2 |  | 3 |
| 2 | 21 | 17-7 | 8-2 | 247 | 299 | 330 | 381 | 434 | 487 | 581 | 691 |  | 1 | 1 | 1 |  | 3 |
| 3 | 23 | 17-9 | 9.6 | 269 | 325 | 358 | 414 | 472 | 530 | 631 | 751 |  | 2 | 1 |  |  | 3 |
| 4 | 25 | 17-10 | 10-10 | 290 | 350 | 387 | 447 | 510 | 572 | 681 | 811 | 1 | 2 |  |  |  | 3 |
| 5 | 20 | 18-10 | 7-0 | 237 | 286 | 315 | 365 | 415 | 466 | 555 | 661 |  | 1 | 1 |  | 1 | 3 |
| 6 | 22 | 18-11 | 8-4 | 258 | 312 | 344 | 398 | 453 | 508 | 606 | 721 |  | 1 | 2 |  |  | 3 |
| 7 | 24 | 19-1 | 9-8 | 279 | 337 | 373 | 431 | 491 | 551 | 656 | 781 | 1 | 1 | 1 |  |  | 3 |
| 8 | 26 | 19-3 | 11-0 | 301 | 363 | 401 | 464 | 529 | 593 | 707 | 842 | 2 | 1 |  |  |  | 3 |
| 9 | 23 | 20-4 | 8-6 | 269 | 325 | 358 | 414 | 472 | 530 | 631 | 751 |  | 2 | 1 |  |  | 3 |
| 10 | 25 | 20-5 | 9-10 | 290 | 350 | 387 | 447 | 510 | 572 | 681 | 811 | 1 | 2 |  |  |  | 3 |
| 11 | 27 | 20-7 | 11-1 | 319 | 386 | 427 | 493 | 561 | 629 | 751 | 893 |  | 2 |  | 1 | 1 | 4 |
| 12 | 22 | 21-6 | 7-3 | 258 | 312 | 344 | 398 | 453 | 508 | 606 | 721 |  | 1 | 2 |  |  | 3 |
| 13 | 24 | 21-8 | 8-7 | 279 | 337 | 373 | 431 | 491 | 551 | 656 | 781 | 1 | 1 | 1 |  |  | 3 |
| 14 | 26 | 21-10 | $9-11$ | 301 | 363 | 401 | 464 | 529 | 593 | 707 | 842 | 2 | 1 |  |  |  | 3 |
| 15 | 28 | 22-5 | 11-3 | 331 | 399 | 440 | 509 | 580 | 650 | 776 | 923 | 1 | 1 |  | 1 | 1 | 4 |
| 16 | 23 | 22-9 | 7-5 | 269 | 325 | 358 | 414 | 472 | 530 | 631 | 751 |  | 2 | 1 |  |  | 3 |
| 17 | 25 | 22-11 | 8-9 | 290 | 350 | 387 | 447 | 510 | 572 | 681 | 811 | 1 | 2 |  |  |  | 3 |
| 18 | 27 | 23-2 | 10-1 | 319 | 386 | 427 | 493 | 561 | 629 | 751 | 893 |  | 1 | 1 | 2 |  | 4 |
| 19 | 29 | 23-4 | 11-5 | 341 | 412 | 455 | 526 | 599 | 671 | 801 | 953 | 1 | 1 |  | 2 |  | 4 |
| 20 | 24 | 24-1 | 7-7 |  | 337 | 373 | 431 | 491 | 551 | 656 | 781 | 1 | 1 | 1 |  |  | 3 |
| 21 | 26 | 24-3 | 8-7 |  | 299 | 330 | 381 | 434 | 487 | 581 | 691 | 1 | 2 |  |  |  | 3 |
| 22 | 25 | 24-3 | 8-11 | 290 | 350 | 387 | 447 | 510 | 572 | 681 | 811 | 2 | 1 |  |  |  | 3 |
| 23 | 27 | 24-5 | 9-11 | 319 | 380 | 427 | 493 | 561 | 629 | 751 | 893 |  |  | 3 | 1 |  | 4 |
| 24 | 28 | 24-5 | 10-3 |  | 399 | 440 | 509 | 580 | 650 | 776 | 923 | 1 | 1 |  | 1 | 1 | 4 |
| 25 | 29 | 24-6 | 11-3 | 341 | 412 | 455 | 526 | 599 | 671 | 801 | 953 |  | 1 | 3 |  |  | 4 |
| 26 | 30 | 24-8 | 11-10 |  | 425 | 469 | 542 | 618 | 693 | 827 | 983 | 2 | 1 |  |  |  | 3 |
| 27 | 31 | 24-8 | 12-7 | 363 | 438 | 483 | 559 | 636 | 714 | 852 | 1013 | 1 | 1 | 2 |  |  | 4 |
| 28 | 25 | 24-11 | 8-0 |  | 350 | 387 | 447 | 510 | 572 | 681 | 811 | 1 | 1 | 2 |  |  | 4 |
| 29 | 27 | 25-7 | 9-1 |  | 386 | 427 | 493 | 561 | 629 | 751 | 893 |  |  | 3 | 1 |  | 4 |
| 30 | 26 | 25-8 | 8-8 | 301 | 363 | 401 | 464 | 529 | 593 | 707 | 842 | 2 | 1 |  |  |  | 3 |
| 31 | 28 | 25-10 | 10-0 | 331 | 399 | 440 | 509 | 580 | 650 | 776 | 923 |  | 2 | 1 |  |  | 3 |
| 32 | 30 | 26-0 | 11-4 | 352 | 418 | 462 | 533 | 608 | 682 | 779 | 928 |  | 2 | 2 |  |  | 4 |
| 33 | 32 | 26-2 | 12-8 | 374 | 451 | 498 | 575 | 655 | 735 | 877 | 1044 | 1 | 2 | 1 |  |  | 4 |
| 34 | 28 | 26-4 | 9-6 |  | 399 | 440 | 509 | 580 | 650 | 776 | 923 |  | 2 | 1 | 1 |  | 4 |
| 35 | 30 | 26-5 | 10-10 |  | 425 | 469 | 542 | 618 | 693 | 827 | 983 |  | 2 | 2 |  |  | 4 |

## Notes:

1. Weights include $3 / 4^{\prime \prime}$ diameter fasteners for assembly. Inquire for cases utilizing $7 / 8^{\prime \prime}$ diameter fasteners.
2. Weight include a galvanized coating which is 3 ounces per square foot, total both sides.
3. Alternate plate make-ups may be supplied due to material availability, which may effect the structure weight.
4. Plates are $45^{\prime \prime}$ in net length except for $5 / 16^{\prime \prime}$ and $3 / 8^{\prime \prime}$ gages, which are $30^{\prime \prime}$ net width.
5. If unbalanced channels are supplied, add 20 pounds per foot to the structure length.

TABLE 74. BRIDGECOR BOX CULVERT 15" ${ }^{\text {5 }}$ ½"

## WEIGHT TABLES

|  |  |  |  |  |  |  | GHT TA |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Dimensions to Inside Corrugation |  |  |  | Gage Thickness (Inches) <br> Weight Shown as per Foot of Structure |  |  |  |  |  |  |  | Plate Make-Up |  |  |  |  |  |
| Structure <br> Number | Total S | Bottom Span (Ft.-ln.) | $\begin{gathered} \text { Rise } \\ \text { (Ft.-In.) } \end{gathered}$ | $\begin{gathered} 10 \\ (0.140) \end{gathered}$ | $\begin{gathered} 8 \\ (0.170) \end{gathered}$ | $\begin{gathered} 7 \\ (0.188) \end{gathered}$ | $\begin{gathered} 5 \\ (0.218) \end{gathered}$ | $\begin{gathered} 3 \\ (0.249) \end{gathered}$ | $\begin{gathered} 1 \\ (0.280) \end{gathered}$ | $\begin{gathered} 5 / 16 \\ (0.318) \end{gathered}$ | $\begin{gathered} 3 / 8 \\ (0.380) \end{gathered}$ | 9 S | 8 S | 7 S | 6 S | 5 S | Total Plates |
| 36 | 32 | 26-6 | 12-2 |  |  | 498 | 575 | 655 | 735 | 877 | 1044 | 1 | 2 | 1 |  |  | 4 |
| 37 | 27 | 27-1 | 8-10 | 319 | 386 | 427 | 493 | 561 | 629 | 751 | 893 |  |  | 3 | 1 |  | 4 |
| 38 | 29 | 27-3 | 10-2 | 341 | 412 | 455 | 526 | 599 | 671 | 801 | 953 |  | 1 | 3 |  |  | 4 |
| 39 | 31 | 27-5 | 11-6 |  | 438 | 483 | 559 | 636 | 714 | 852 | 1013 |  |  | 3 | 1 |  | 4 |
| 40 | 27 | 27-6 | 8-4 |  |  | 427 | 493 | 561 | 629 | 751 | 893 |  |  | 3 | 1 |  | 4 |
| 41 | 33 | 27-7 | 12-10 |  | 463 | 512 | 592 | 674 | 756 | 902 | 1074 | 1 | 3 |  |  |  | 4 |
| 42 | 31 | 27-9 | 11-0 |  |  | 483 | 559 | 636 | 714 | 852 | 1013 |  | 3 | 1 |  |  | 4 |
| 43 | 33 | 27-11 | 12-4 |  |  | 512 | 592 | 674 | 756 | 902 | 1074 | 1 | 3 |  |  |  | 4 |
| 44 | 29 | 28-2 | 9-5 |  |  | 455 | 526 | 599 | 671 | 801 | 953 |  | 1 | 3 |  |  | 4 |
| 45 | 28 | 28-6 | 9-0 |  | 463 | 512 | 592 | 674 | 756 | 902 | 1074 |  | 2 | 1 |  | 1 | 4 |
| 46 | 28 | 28-8 | 10-4 |  | 399 | 440 | 509 | 580 | 650 | 776 | 923 |  | 2 | 2 |  |  | 4 |
| 47 | 28 | 28-10 | 8-6 |  |  | 440 | 509 | 580 | 650 | 776 | 923 |  | 2 | 1 |  | 1 | 4 |
| 48 | 34 | 29-1 | 13-0 |  | 476 | 526 | 608 | 693 | 778 | 927 | 1104 | 1 | 2 | 1 |  |  | 4 |
| 49 | 32 | 29-1 | 11-2 |  |  | 498 | 575 | 655 | 735 | 877 | 1044 | 1 | 2 | 1 |  |  | 4 |
| 50 | 34 | 29-1 | 13-0 |  | 476 | 526 | 608 | 693 | 778 | 927 | 1104 | 2 | 2 |  |  |  | 4 |
| 51 | 34 | 29-3 | 12-6 |  |  |  | 608 | 693 | 778 | 927 | 1104 | 2 | 2 |  |  |  | 4 |
| 52 | 30 | 29-3 | 9-7 |  |  |  | 542 | 618 | 693 | 827 | 983 |  | 2 | 2 |  |  | 4 |
| 53 | 29 | 29-10 | 9-1 |  | 412 | 455 | 526 | 599 | 671 | 801 | 953 |  | 1 | 3 |  |  | 4 |
| 54 | 31 | 30-1 | 10-5 |  | 438 | 483 | 559 | 636 | 714 | 852 | 1013 |  | 3 | 1 |  |  | 4 |
| 55 | 33 | 30-7 | 11-9 |  | 463 | 512 | 592 | 674 | 756 | 902 | 1074 | 1 | 3 |  |  |  | 4 |
| 56 | 33 | 30-5 | 11-3 |  |  |  | 592 | 674 | 756 | 902 | 1074 | 1 | 3 |  |  |  | 4 |
| 57 | 35 | 30-7 | 12-7 |  | 489 | 541 | 625 | 712 | 799 | 953 | 1135 | 3 | 1 |  |  |  | 4 |
| 58 | 35 | 30-7 | 13-1 |  |  |  |  | 712 | 799 | 953 | 1135 | 3 | 1 |  |  |  | 4 |
| 59 | 29 | 30-7 | 8-5 |  |  |  |  | 599 | 671 | 801 | 953 |  | 1 | 3 |  |  | 4 |
| 60 | 30 | 30-8 | 9-7 |  | 425 | 469 | 542 | 618 | 693 | 827 | 983 |  | 2 | 2 |  |  | 4 |
| 61 | 32 | 30-9 | 10-11 |  | 451 | 498 | 575 | 655 | 735 | 877 | 1044 | 1 | 2 | 1 |  |  | 4 |
| 62 | 34 | 30-11 | 12-2 |  |  | 526 | 608 | 693 | 778 | 927 | 1104 | 2 | 2 |  |  |  | 4 |
| 63 | 36 | 31-0 | 13-6 |  |  | 566 | 654 | 744 | 835 | 997 | 1186 | 2 | 1 |  |  |  | 3 |
| 64 | 30 | 31-6 | 8-9 |  |  |  | 542 | 618 | 693 | 827 | 983 |  | 2 | 2 |  |  | 4 |
| 65 | 34 | 31--9 | 11-5 |  |  |  | 608 | 693 | 778 | 927 | 1104 | 2 | 2 |  |  |  | 4 |
| 66 | 31 | 32-0 | 9-8 |  |  | 483 | 559 | 636 | 714 | 852 | 1013 |  | 3 | 1 |  |  | 4 |
| 67 | 33 | 32-2 | 11-0 |  |  | 512 | 592 | 674 | 756 | 902 | 1074 | 1 | 3 |  |  |  | 4 |
| 68 | 35 | 32-4 | 12-4 |  |  | 541 | 625 | 712 | 799 | 953 | 1135 | 3 | 1 |  |  |  | 4 |
| 69 | 37 | 32-6 | 13-8 |  |  | 580 | 670 | 763 | 856 | 1022 | 1216 | 2 | 1 |  | 1 | 1 | 4 |
| 70 | 32 | 33-5 | 9-10 |  |  |  | 575 | 655 | 735 | 877 | 1044 | 1 | 2 | 1 |  |  | 4 |
| 71 | 34 | 33-7 | 11-2 |  |  |  | 608 | 693 | 778 | 927 | 1104 | 2 | 2 |  |  |  | 4 |
| 72 | 36 | 33-9 | 12-6 |  |  |  | 654 | 744 | 835 | 997 | 1186 |  | 1 | 4 |  |  | 5 |
| 73 | 38 | 34-0 | 13-10 |  |  |  | 687 | 782 | 877 | 1047 | 1246 | 1 | 1 | 3 |  |  | 4 |
| 74 | 33 | 34-9 | 10-0 |  |  |  | 592 | 674 | 756 | 902 | 1074 | 1 | 3 |  |  |  | 4 |
| 75 | 35 | 34-11 | 11-3 |  |  |  | 625 | 712 | 799 | 953 | 1135 | 3 | 1 |  |  |  | 4 |
| 76 | 37 | 35-2 | 12-7 |  |  |  | 670 | 763 | 856 | 1022 | 1216 |  | 3 | 1 | 1 |  | 5 |
| 77 | 39 | 35-4 | 13-11 |  |  |  | 703 | 801 | 898 | 1197 | 1276 | 1 | 3 |  | 1 |  | 5 |
| VARIES | UP TO 45' | VARIES |  | INQUIRE |  |  |  |  |  |  |  |  |  |  |  |  |  |

Notes:

1. Weights include $3 / 4^{\prime \prime}$ diameter fasteners for assembly. Inquire for cases utilizing $7 / 8^{\prime \prime}$ diameter fasteners.
2. Weight include a galvanized coating which is 3 ounces per square foot, total both sides.
3. Alternate plate make-ups may be supplied due to material availability, which may effect the structure weight.
4. Plates are $45^{\prime \prime}$ in net length except for $5 / 16^{\prime \prime}$ and $3 / 8^{\prime \prime}$ gages, which are $30^{\prime \prime}$ net width.
5. If Unbalanced Channels are supplied, add 20 pounds per foot to the structure length.

TABLE 75. BRIDGECOR ROUND PIPE 15" $\times 5 /{ }^{\prime \prime}$ "

## LRED HEIGHT OF COVER GUIDE

| Dimensions to Inside Corrugation |  |  |  | Gage Thickness (Inches) Maximum Cover Height Shown in Feet |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Diameter (Ft.-In.) | Approx. Area (Sq. Ft) | Min. Cover (Ft.) | Total S | $\begin{gathered} 10 \\ (0.140) \end{gathered}$ | $\begin{gathered} 8 \\ (0.170) \end{gathered}$ | $\begin{gathered} 7 \\ (0.188) \end{gathered}$ | $\begin{gathered} 5 \\ (0.218) \end{gathered}$ | $\begin{gathered} 3 \\ (0.249) \end{gathered}$ | $\begin{gathered} 1 \\ (0.280) \end{gathered}$ | $\begin{gathered} 5 / 16 \\ (0.318) \end{gathered}$ | $\begin{gathered} 3 / 8 \\ (0.380) \end{gathered}$ | Select <br> Backfill Width <br> (ft) | Precon (Min. Level) |
| 19-11 | 311.4 | 2.5 | 48 | 23 | 28 | 31 | 36 | 41 | 46 | 52 | 63 | 8.0 | 1 |
| 20-9 | 338.5 | 2.5 | 50 | 22 | 26 | 29 | 34 | 39 | 44 | 51 | 61 | 8.0 | 1 |
| 21-7 | 366.8 | 2.5 | 52 | 20 | 25 | 28 | 33 | 38 | 43 | 49 | 59 | 8.0 | 1 |
| 22-6 | 396.3 | 2.5 | 54 | 19 | 24 | 27 | 32 | 36 | 41 | 47 | 57 | 8.0 | 1 |
| 23-4 | 426.8 | 2.5 | 56 | 18 | 23 | 26 | 30 | 35 | 40 | 46 | 55 | 8.0 | 1 |
| 24-2 | 458.5 | 2.5 | 58 | 17 | 22 | 25 | 29 | 34 | 38 | 44 | 54 | 8.0 | 1 |
| 25-0 | 490.9 | 2.5 | 60 | 16 | 21 | 23 | 28 | 32 | 37 | 43 | 52 | 8.0 | 1 |
| 25-10 | 524.9 | 2.5 | 62 | 15 | 20 | 22 | 27 | 31 | 36 | 41 | 50 | 8.0 | 1 |
| 26-8 | 560 | 2.5 | 64 | 14 | 19 | 21 | 26 | 30 | 34 | 40 | 49 | 8.0 | 1 |
| 27-7 | 596.2 | 2.5 | 66 | 13 | 18 | 20 | 24 | 29 | 33 | 38 | 47 | 8.0 | 2 |
| 28-5 | 633.5 | 2.5 | 68 | 13 | 17 | 19 | 23 | 28 | 32 | 37 | 45 | 8.0 | 2 |
| 29-3 | 672.0 | 2.5 | 70 | 12 | 16 | 18 | 22 | 27 | 31 | 36 | 44 | 8.0 | 2 |
| 30-1 | 711.6 | 3.0 | 72 | 11 | 15 | 18 | 21 | 26 | 30 | 34 | 42 | 8.0 | 2 |
| 30-11 | 752.3 | 3.0 | 74 | 11 | 14 | 17 | 21 | 24 | 28 | 33 | 41 | 8.0 | 2 |
| 31-10 | 794.2 | 3.0 | 76 | 10 | 14 | 16 | 20 | 24 | 27 | 32 | 40 | 8.0 | 2 |
| 32-8 | 837.3 | 3.0 | 78 |  | 13 | 15 | 19 | 23 | 26 | 31 | 38 | 8.0 | 2 |
| 33-6 | 880.9 | 3.0 | 80 |  | 12 | 14 | 18 | 22 | 25 | 30 | 37 | 8.0 | 2 |
| 34-4 | 926.2 | 3.0 | 82 |  | 12 | 14 | 17 | 21 | 24 | 29 | 36 | 8.0 | 2 |
| 35-2 | 972.6 | 3.0 | 84 |  | 11 | 13 | 17 | 20 | 23 | 28 | 35 | 8.0 | 2 |
| 36-0 | 1020.1 | 3.0 | 86 |  |  | 13 | 16 | 19 | 22 | 27 | 33 | 8.0 | 2 |
| 36-11 | 1069.0 | 3.0 | 88 |  |  | 12 | 15 | 18 | 22 | 26 | 32 | 8.0 | 2 |
| 37-9 | 1118.6 | 3.0 | 90 |  |  |  | 15 | 18 | 21 | 25 | 31 | 8.0 | 2 |
| 38-7 | 1169.6 | 3.0 | 92 |  |  |  | 14 | 17 | 20 | 24 | 30 | 8.0 | 2 |
| 39-5 | 1221.7 | 3.0 | 94 |  |  |  | 14 | 16 | 19 | 23 | 29 | 8.0 | 2 |
| 40-3 | 1274.9 | 3.0 | 96 |  |  |  | 13 | 16 | 19 | 22 | 28 | 8.0 | 3 |
| 41-2 | 1328.6 | 3.0 | 98 |  |  |  |  | 15 | 18 | 21 | 27 | 8.0 | 3 |
| 42-0 | 1384.1 | 3.0 | 100 |  |  |  |  | 15 | 17 | 21 | 26 | 8.0 | 3 |
| 42-10 | 1440.7 | 3.0 | 102 |  |  |  |  | 14 | 17 | 20 | 26 | 8.0 | 3 |
| 43-8 | 1498.5 | 3.0 | 104 |  |  |  |  |  | 16 | 19 | 25 | 8.0 | 3 |
| 44-6 | 1557.4 | 3.0 | 106 |  |  |  |  |  | 16 | 19 | 24 | 8.0 | 3 |
| 45-5 | 1617.4 | 3.0 | 108 |  |  |  |  |  | 15 | 18 | 23 | 8.0 | 3 |
| 46-3 | 1678.6 | 4.0 | 110 |  |  |  |  |  | 15 | 18 | 23 | 8.0 | 3 |
| 47-1 | 1740.9 | 4.0 | 112 |  |  |  |  |  |  | 17 | 22 | 8.0 | 4 |
| 47-11 | 1803.5 | 4.0 | 114 |  |  |  |  |  |  | 17 | 21 | 8.0 | 4 |
| 48-9 | 1868.1 | 4.0 | 116 |  |  |  |  |  |  | 16 | 21 | 8.0 | 4 |
| 49-7 | 1933.8 | 5.0 | 118 |  |  |  |  |  |  | 16 | 20 | 8.0 | 4 |
| 50-6 | 2000.6 | 5.0 | 120 |  |  |  |  |  |  |  | 20 | 8.0 | 4 |

Notes:

1. Not for a specific structural design. Use for budget estimating only. A CANDE analysis is required for final design and quotation.
2. The above table is based upon the minimum requirements of the AASHTO LRFD Design Specification, Section 12, and:
a. Backfill material per AASHTO M145, class A-2-5 or better.
b. Backfill 120 pcf in density and compacted to $90 \%$ modified proctor.
c. The minimum cover is per article 12.8.9.4
d. The minimum select backfill width (eight feet) is measured from outside the maximum span on each side of the structure. This width only applies when the material adjacent to the select zone is determined to be
competent, well consolidated material
3. Select backfill width may increase for situations where lower strength fill exists in either the select fill zone or the adjacent embankment zone.
4. This estimate is for single barrel structures. For multiple barrels, more investigation is required.

TABLE 76. BRIDGECOR ROUND PIPE 15" $\times 51 / 21$
WEIGHT TABLES

| Inside Diameter |  | Gage Thickness (Inches) - Weight Shown as per Foot of Structure |  |  |  |  |  |  |  | Plate Make-Up |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Diameter (Ft.-In.) | Total S | $\begin{gathered} 10 \\ (0.140) \end{gathered}$ | $\begin{gathered} 8 \\ (0.170) \end{gathered}$ | $\begin{gathered} 7 \\ (0.188) \end{gathered}$ | $\begin{gathered} 5 \\ (0.218) \end{gathered}$ | $\begin{gathered} 3 \\ (0.249) \\ \hline \end{gathered}$ | $\begin{gathered} 1 \\ (0.280) \end{gathered}$ | $\begin{gathered} 5 / 16 \\ (0.318) \\ \hline \end{gathered}$ | $\begin{gathered} 3 / 8 \\ (0.380) \\ \hline \end{gathered}$ | 9 S | 8 S | 7 S | 6S | 5 S | Total Plates |
| 19-11 | 48 | 565 | 680 | 750 | 867 | 987 | 1107 | 1325 | 1574 |  | 6 |  |  |  | 6 |
| 20-9 | 50 | 586 | 706 | 779 | 900 | 1025 | 1149 | 1375 | 1635 | 2 | 4 |  |  |  | 6 |
| 21-7 | 52 | 607 | 731 | 808 | 933 | 1063 | 1191 | 1426 | 1696 | 4 | 2 |  |  |  | 6 |
| 22-6 | 54 | 629 | 757 | 837 | 966 | 1101 | 1234 | 1476 | 1757 | 6 |  |  |  |  | 6 |
| 23-4 | 56 | 659 | 793 | 875 | 1012 | 1152 | 1292 | 1546 | 1837 |  | 7 |  |  |  | 7 |
| 24-2 | 58 | 680 | 819 | 904 | 1045 | 1190 | 1334 | 1596 | 1898 | 2 | 5 |  |  |  | 7 |
| 25-0 | 60 | 702 | 845 | 933 | 1078 | 1227 | 1376 | 1646 | 1958 | 4 | 3 |  |  |  | 7 |
| 25-10 | 62 | 723 | 870 | 962 | 1111 | 1265 | 1418 | 1697 | 2019 | 6 | 1 |  |  |  | 7 |
| 26-8 | 64 | 753 | 907 | 1001 | 1156 | 1316 | 1476 | 1766 | 2099 |  | 8 |  |  |  | 8 |
| 27-7 | 66 | 774 | 932 | 1029 | 1189 | 1354 | 1518 | 1817 | 2160 | 2 | 6 |  |  |  | 8 |
| 28-5 | 68 | 796 | 958 | 1058 | 1222 | 1392 | 1561 | 1867 | 2221 | 4 | 4 |  |  |  | 8 |
| 29-3 | 70 | 817 | 983 | 1087 | 1255 | 1430 | 1603 | 1918 | 2282 | 6 | 2 |  |  |  | 8 |
| 30-1 | 72 | 838 | 1009 | 1116 | 1289 | 1468 | 1645 | 1968 | 2342 | 8 |  |  |  |  | 8 |
| 30-11 | 74 | 869 | 1046 | 1154 | 1334 | 1519 | 1703 | 2038 | 2422 | 2 | 7 |  |  |  | 9 |
| 31-10 | 76 | 890 | 1071 | 1183 | 1367 | 1557 | 1745 | 2088 | 2483 | 4 | 5 |  |  |  | 9 |
| 32-8 | 78 |  | 1097 | 1212 | 1400 | 1594 | 1787 | 2138 | 2544 | 6 | 3 |  |  |  | 9 |
| 33-6 | 80 |  | 1122 | 1241 | 1433 | 1632 | 1829 | 2189 | 2605 | 8 | 1 |  |  |  | 9 |
| 34-4 | 82 |  | 1159 | 1279 | 1478 | 1683 | 1887 | 2258 | 2685 | 2 | 8 |  |  |  | 10 |
| 35-2 | 84 |  | 1185 | 1308 | 1511 | 1721 | 1930 | 2309 | 2746 | 4 | 6 |  |  |  | 10 |
| 36-0 | 86 |  |  | 1337 | 1545 | 1759 | 1972 | 2359 | 2806 | 6 | 4 |  |  |  | 10 |
| 36-11 | 88 |  |  | 1366 | 1578 | 1797 | 2014 | 2410 | 2867 | 8 | 2 |  |  |  | 10 |
| 37-9 | 90 |  |  |  | 1611 | 1835 | 2056 | 2460 | 2928 | 10 |  |  |  |  | 10 |
| 38-7 | 92 |  |  |  | 1656 | 1886 | 2114 | 2530 | 3008 | 4 | 7 |  |  |  | 11 |
| 39-5 | 94 |  |  |  | 1689 | 1923 | 2156 | 2580 | 3069 | 6 | 5 |  |  |  | 11 |
| 40-3 | 96 |  |  |  | 1722 | 1961 | 2198 | 2630 | 3130 | 8 | 3 |  |  |  | 11 |
| 41-2 | 98 |  |  |  |  | 1999 | 2241 | 2681 | 3190 | 10 | 1 |  |  |  | 11 |
| 42-0 | 100 |  |  |  |  | 2050 | 2299 | 2750 | 3270 | 4 | 8 |  |  |  | 12 |
| 42-10 | 102 |  |  |  |  | 2088 | 2341 | 2801 | 3331 | 6 | 6 |  |  |  | 12 |
| 43-8 | 104 |  |  |  |  |  | 2383 | 2851 | 3392 | 8 | 4 |  |  |  | 12 |
| 44-6 | 106 |  |  |  |  |  | 2425 | 2902 | 3453 | 10 | 2 |  |  |  | 12 |
| 45-5 | 108 |  |  |  |  |  | 2467 | 2952 | 3514 | 12 |  |  |  |  | 12 |
| 46-3 | 110 |  |  |  |  |  | 2525 | 3022 | 3594 | 6 | 7 |  |  |  | 13 |
| 47-1 | 112 |  |  |  |  |  |  | 3072 | 3654 | 8 | 5 |  |  |  | 13 |
| 47-11 | 114 |  |  |  |  |  |  | 3122 | 3715 | 10 | 3 |  |  |  | 13 |
| 48-9 | 116 |  |  |  |  |  |  | 3173 | 3776 | 12 | 1 |  |  |  | 13 |
| 49-7 | 118 |  |  |  |  |  |  | 3242 | 3856 | 6 | 8 |  |  |  | 14 |
| 50-6 | 120 |  |  |  |  |  |  |  | 3917 | 8 | 6 |  |  |  | 14 |

Notes:

1. Weights include $3 / 4^{\prime \prime}$ diameter fasteners for assembly. Inquire for applications requiring 7/8" diameter fasteners.
2. Weights include a 3 oz . per square foot galvanized coating on both sides.
3. An alternate plate make-up may be supplied due to material availability. This may affect the overall structure weight.
4. 10 ga. through 1 ga. plate net lay length is $45^{\prime \prime} .5 / 16^{\prime \prime}$ and $3 / 8^{\prime \prime}$ plate net lay length is 30 ".

TABLE 77. BRIDGECOR SINGLE RADIUS ARCH $15^{\prime \prime} \mathrm{X} 5 /{ }^{\prime \prime}$
LRFD HEIGHT OF COVER GUIDE

| LRFD HEIGHT OF COVER GUIDE |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Dimensions to Inside Corrugation |  |  |  |  | Gage Thickness (Inches) Maximum Height of Cover Shown in Feet |  |  |  |  |  |  |  |  |  |
| Bottom Span (Ft.-ln.) | $\begin{gathered} \text { Rise } \\ \text { (Ft.-In.) } \end{gathered}$ | Approx. Area (Sq. Ft.) | Min Cover (Ft.) | Total S | $\begin{gathered} 10 \\ (0.140) \end{gathered}$ | $\begin{gathered} 8 \\ (0.170) \end{gathered}$ | $\begin{gathered} 7 \\ (0.188) \end{gathered}$ | $\begin{gathered} 5 \\ (0.218) \end{gathered}$ | $\begin{gathered} 3 \\ (0.249) \end{gathered}$ | $\begin{gathered} 1 \\ (0.280) \end{gathered}$ | $\begin{gathered} 5 / 16 \\ (0.318) \end{gathered}$ | $\begin{gathered} 3 / 8 \\ (0.380) \end{gathered}$ | Select Fill Width (ft.) | Precon (min Level) |
| 19-7 | 9-9 | 150.0 | 2.0 | 23 | 18 | 22 | 24 | 29 | 33 | 37 | 43 | 52 | 8.0 | 1 |
| 19-10 | 5-0 | 66.3 | 2.0 | 17 | 18 | 22 | 24 | 29 | 33 | 37 | 43 | 52 | 8.0 | 1 |
| 20-5 | 10-2 | 163.5 | 2.0 | 24 | 17 | 21 | 23 | 28 | 32 | 36 | 42 | 50 | 8.0 | 1 |
| 21-3 | 10-7 | 177.2 | 2.0 | 25 | 16 | 20 | 23 | 27 | 31 | 35 | 40 | 49 | 8.0 | 1 |
| 22-1 | 11-0 | 191.5 | 2.0 | 26 | 15 | 19 | 22 | 26 | 30 | 34 | 39 | 47 | 8.0 | 1 |
| 22-10 | 11-6 | 206.6 | 2.0 | 27 | 15 | 19 | 21 | 25 | 29 | 33 | 38 | 46 | 8.0 | 1 |
| 23-10 | 11-11 | 222.2 | 2.0 | 28 | 14 | 18 | 20 | 24 | 28 | 32 | 36 | 44 | 8.0 | 1 |
| 24-8 | 12-4 | 238.3 | 2.0 | 29 | 13 | 17 | 19 | 23 | 27 | 30 | 35 | 43 | 8.0 | 1 |
| 24-8 | 6-0 | 102.7 | 3.0 | 21 | 13 | 17 | 19 | 23 | 27 | 30 | 35 | 43 | 8.0 | 1 |
| 25-6 | 12-9 | 255.0 | 2.0 | 30 | 13 | 16 | 19 | 22 | 26 | 29 | 34 | 41 | 8.0 | 1 |
| 26-4 | 13-2 | 272.3 | 2.0 | 31 | 12 | 16 | 18 | 21 | 25 | 28 | 33 | 40 | 8.0 | 1 |
| 27-2 | 13-7 | 290.1 | 2.0 | 32 | 12 | 15 | 17 | 20 | 24 | 27 | 32 | 38 | 8.0 | 2 |
| 28-0 | 14-0 | 308.5 | 2.0 | 33 | 11 | 14 | 16 | 20 | 23 | 26 | 30 | 37 | 8.0 | 2 |
| 28-10 | 7-5 | 149.1 | 2.0 | 25 | 10 | 13 | 15 | 18 | 21 | 24 | 28 | 35 | 8.0 | 2 |
| 28-10 | 14-5 | 327.5 | 2.0 | 34 | 11 | 14 | 16 | 19 | 22 | 25 | 29 | 36 | 8.0 | 2 |
| 29-8 | 14-10 | 347.0 | 2.0 | 35 | 10 | 13 | 15 | 18 | 21 | 24 | 28 | 35 | 8.0 | 2 |
| 30-6 | 15-3 | 367.1 | 2.0 | 36 | 10 | 13 | 14 | 17 | 20 | 24 | 27 | 34 | 8.0 | 2 |
| 31-6 | 15-9 | 387.8 | 2.0 | 37 | 9 | 12 | 14 | 17 | 20 | 23 | 26 | 32 | 8.0 | 2 |
| 32-4 | 16-1 | 409.1 | 2.0 | 38 | 9 | 12 | 13 | 16 | 19 | 22 | 25 | 31 | 8.0 | 2 |
| 33-2 | 16-7 | 430.9 | 2.0 | 39 | 8 | 11 | 13 | 15 | 18 | 21 | 25 | 30 | 8.0 | 2 |
| 34-0 | 17-0 | 453.2 | 2.0 | 40 | 8 | 10 | 12 | 15 | 18 | 20 | 24 | 29 | 8.0 | 2 |
| 34-1 | 9-2 | 219.4 | 2.0 | 30 | 8 | 10 | 12 | 15 | 18 | 20 | 24 | 29 | 8.0 | 2 |
| 35-8 | 17-10 | 499.6 | 2.0 | 42 | 7 | 9 | 11 | 14 | 16 | 19 | 22 | 27 | 8.0 | 2 |
| 37-0 | 18-9 | 548.2 | 2.0 | 44 | 6 | 9 | 10 | 12 | 15 | 17 | 20 | 25 | 8.0 | 2 |
| 38-11 | 10-2 | 277.5 | 2.0 | 34 | 6 | 8 | 9 | 11 | 14 | 16 | 19 | 24 | 8.0 | 2 |
| 39-0 | 19-6 | 599.3 | 2.0 | 46 | 6 | 8 | 9 | 11 | 14 | 16 | 19 | 24 | 8.0 | 2 |
| 40-8 | 20-4 | 652.5 | 2.0 | 48 | 5 | 7 | 8 | 11 | 13 | 15 | 18 | 22 | 8.0 | 3 |
| 42-6 | 21-3 | 708.0 | 2.0 | 50 | 4 | 6 | 8 | 10 | 12 | 14 | 17 | 21 | 8.0 | 3 |
| 44-2 | 22-1 | 765.7 | 2.0 | 52 | 4 | 6 | 7 | 9 | 11 | 13 | 16 | 20 | 8.0 | 3 |
| 45-10 | 22-11 | 825.7 | 2.0 | 54 | 4 | 5 | 6 | 8 | 10 | 12 | 15 | 19 | 8.0 | 3 |
| 46-0 | 11-9 | 379.5 | 2.0 | 40 | 4 | 5 | 6 | 8 | 10 | 12 | 15 | 19 | 8.0 | 3 |
| 49-2 | 24-7 | 952.5 | 2.5 | 58 |  | 4 | 5 | 7 | 9 | 11 | 13 | 17 | 8.0 | 3 |
| 51-0 | 25-6 | 1019.4 | 2.5 | 60 |  | 4 | 5 | 7 | 9 | 10 | 13 | 16 | 8.0 | 3 |
| 52-8 | 26-4 | 1088.4 | 3.0 | 62 |  |  | 5 | 7 | 8 | 10 | 12 | 16 | 8.0 | 3 |
| 54-4 | 27-2 | 1159.7 | 3.0 | 64 |  |  |  | 6 | 8 | 10 | 12 | 16 | 8.0 | 3 |

Notes:

1. Not for a specific structural design. Use for budget estimating only. A CANDE analysis is required for final design and quotation.
2. The above table is based upon the minimum requirements of the AASHTO LRFD Design Specification, Section 12, and:
a. Backfill material per AASHTO M145, class A-2-5 or better.
b. Backfill 120 pcf in density and compacted to $90 \%$ modified proctor.
c. The minimum cover is per article 12.8.9.4
d. The minimum select backfill width (eight feet) is measured from outside the maximum span on each side of the structure.

This width only applies when the material adjacent to the slect zone is determined to be competent, well consolidated material
3. Select backfill width may increase for situations where lower strength fill exists in either the select fill zone or the adjacent embankment zone.
4. This estimate is for single barrel structures. For multiple barrels, more investigation is required.

| TABLE 78. BRIDGECOR SINGLE RADIUS ARCH $15{ }^{\prime \prime} \times 1 ½$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| WEIGHT TABLES |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Dimensions to Inside Corrugation |  |  | Gage Thickness (Inches) <br> Weight Shown as per Foot of Structure |  |  |  |  |  |  |  | Plate Make-Up |  |  |  |  |  |
| Bottom Span (Ft.-In.) | Rise (Ft.-In.) | Total S | $\begin{gathered} 10 \\ (0.140) \end{gathered}$ | $\begin{gathered} 8 \\ (0.170) \end{gathered}$ | $\begin{gathered} 7 \\ (0.188) \end{gathered}$ | $\begin{array}{\|l} 5 \\ (0.218) \end{array}$ | $\begin{gathered} 3 \\ (0.249) \end{gathered}$ | $\begin{gathered} 1 \\ (0.280) \end{gathered}$ | $\begin{gathered} 5 / 16 \\ (0.318) \end{gathered}$ | $\begin{gathered} 3 / 8 \\ (0.380) \end{gathered}$ | 9 S | 8 S | 7 S | 6 S | 5 S | Total Plates |
| 19-7 | 9-9 | 23 | 269 | 325 | 358 | 414 | 472 | 530 | 631 | 751 |  | 2 | 1 |  |  | 3 |
| 19-10 | 5-0 | 17 | 196 | 237 | 262 | 303 | 345 | 387 | 461 | 549 | 1 | 1 |  |  |  | 2 |
| 20-5 | 10-2 | 24 | 279 | 337 | 373 | 431 | 491 | 551 | 656 | 781 | 1 | 1 | 1 |  |  | 3 |
| 21-3 | 10-7 | 25 | 290 | 350 | 387 | 447 | 510 | 572 | 681 | 811 | 1 | 2 |  |  |  | 3 |
| 22-1 | 11-0 | 26 | 301 | 363 | 401 | 464 | 529 | 593 | 707 | 842 | 2 | 1 |  |  |  | 3 |
| 22-10 | 11-6 | 27 | 319 | 386 | 427 | 493 | 561 | 629 | 751 | 893 |  |  | 3 | 1 |  | 4 |
| 23-10 | 11-11 | 28 | 331 | 399 | 440 | 509 | 580 | 650 | 776 | 923 |  | 2 | 1 |  | 1 | 4 |
| 24-8 | 12-4 | 29 | 341 | 412 | 455 | 526 | 599 | 671 | 801 | 953 |  | 1 | 3 |  |  | 4 |
| 24-8 | 6-0 | 21 | 247 | 330 | 299 | 381 | 434 | 487 | 581 | 691 |  | 1 | 1 | 1 |  | 3 |
| 25-6 | 12-9 | 30 | 352 | 469 | 425 | 542 | 618 | 693 | 827 | 983 |  | 2 | 2 |  |  | 4 |
| 26-4 | 13-2 | 31 | 363 | 483 | 438 | 559 | 636 | 714 | 852 | 1013 |  | 3 | 1 |  |  | 4 |
| 27-2 | 13-7 | 32 | 374 | 498 | 451 | 575 | 655 | 735 | 877 | 1044 | 1 | 2 | 1 |  |  | 4 |
| 28-0 | 14-0 | 33 | 385 | 463 | 512 | 592 | 674 | 756 | 902 | 1074 | 1 | 3 |  |  |  | 4 |
| 28-10 | 14-5 | 34 | 395 | 476 | 526 | 608 | 693 | 778 | 927 | 1104 | 2 | 2 |  |  |  | 4 |
| 29-8 | 14-10 | 35 | 406 | 489 | 541 | 625 | 712 | 799 | 953 | 1135 | 3 | 1 |  |  |  | 4 |
| 28-10 | 7-5 | 25 | 290 | 350 | 387 | 447 | 510 | 572 | 681 | 811 | 1 | 2 |  |  |  | 3 |
| 30-6 | 15-3 | 36 | 424 | 513 | 566 | 654 | 744 | 835 | 997 | 1186 |  | 1 | 4 |  |  | 5 |
| 31-6 | 15-9 | 37 | 435 | 525 | 580 | 670 | 763 | 856 | 1022 | 1216 |  | 3 | 1 | 1 |  | 5 |
| 32-4 | 16-1 | 38 | 446 | 538 | 594 | 687 | 782 | 877 | 1047 | 1246 |  | 3 | 2 |  |  | 5 |
| 33-2 | 16-7 | 39 | 457 | 551 | 608 | 703 | 801 | 899 | 1073 | 1276 |  | 4 | 1 |  |  | 5 |
| 34-0 | 17-0 | 40 | 468 | 564 | 623 | 720 | 820 | 920 | 1098 | 1306 | 1 | 3 | 1 |  |  | 5 |
| 34-1 | 9-2 | 30 | 352 | 425 | 469 | 542 | 618 | 693 | 827 | 983 |  | 2 | 2 |  |  | 4 |
| 35-8 | 17-10 | 42 | 489 | 590 | 651 | 753 | 858 | 962 | 1148 | 1367 | 2 | 3 |  |  |  | 5 |
| 37-0 | 18-9 | 44 | 511 | 615 | 680 | 786 | 896 | 680 | 1199 | 1427 | 4 | 1 |  |  |  | 5 |
| 39-0 | 19-6 | 46 | 540 | 652 | 719 | 831 | 947 | 1062 | 1268 | 1508 |  | 4 | 2 |  |  | 6 |
| 38-11 | 10-2 | 34 | 395 | 476 | 526 | 608 | 693 | 778 | 927 | 1104 | 2 | 2 |  |  |  | 4 |
| 40-8 | 20-4 | 48 | 562 | 677 | 748 | 864 | 984 | 1104 | 1319 | 1569 | 2 | 2 | 2 |  |  | 6 |
| 42-6 | 21-3 | 50 | 583 | 703 | 776 | 898 | 1022 | 1147 | 1369 | 1629 | 2 | 4 |  |  |  | 6 |
| 44-2 | 22-1 | 52 | 605 | 729 | 805 | 931 | 1060 | 1189 | 1419 | 1690 | 4 | 2 |  |  |  | 6 |
| 45-10 | 22-11 | 54 | 634 | 765 | 844 | 976 | 1111 | 1246 | 1489 | 1771 |  | 5 | 2 |  |  | 7 |
| 46-0 | 11-9 | 40 | 468 | 564 | 623 | 720 | 820 | 920 | 1098 | 1306 | 1 | 3 | 1 |  |  | 5 |
| 49-2 | 24-7 | 58 |  | 816 | 902 | 1042 | 1187 | 1331 | 1590 | 1891 | 2 | 5 |  |  |  | 7 |
| 51-0 | 25-6 | 60 |  | 842 | 930 | 1075 | 1225 | 1373 | 1640 | 1952 | 4 | 3 |  |  |  | 7 |
| 52-8 | 26-4 | 62 |  |  | 959 | 1108 | 1263 | 1415 | 1691 | 2013 | 6 | 1 |  |  |  | 7 |
| 54-4 | 27-2 | 64 |  |  |  | 1154 | 1314 | 1473 | 1760 | 2093 | 1 | 6 | 1 |  |  | 8 |

## Notes

1. Weights include $3 / 4^{\prime \prime}$ diameter fasteners for assembly. Inquire for applications requiring 7/8" diameter fasteners.
2. Weights include a 3 oz . per square foot galvanized coating on both sides.
3. An alternate plate make-up may be supplied due to material availability. This may affect the overall structure weight.
4. 10 ga. through 1 ga. plate net lay length is $45^{\prime \prime} .5 / 16^{\prime \prime}$ and $3 / 8^{\prime \prime}$ plate net lay length is 30 ".
5. If unbalanced channels are required, add 20 lbs ./ foot times the total structure length.

## LRED HEGHT OF COVER GUIDE

| Dimensions to Inside Corrugation |  |  |  |  | Gage Thickness (Inches) - Height of Cover Shown in Feet Maximum Height of Cover (Minimum Height of Cover) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Shape | Maximum Span (Ft.-In.) | $\begin{gathered} \text { Rise } \\ \text { (Ft.-ln.) } \end{gathered}$ | Approx. Area (Sq. Ft.) | Total S | $\begin{gathered} 10 \\ (0.140) \end{gathered}$ | $\begin{gathered} 8 \\ (0.170) \end{gathered}$ | $\begin{gathered} 7 \\ (0.188) \end{gathered}$ | $\begin{gathered} 5 \\ (0.218) \end{gathered}$ | $\begin{gathered} 3 \\ (0.249) \end{gathered}$ | $\begin{gathered} 1 \\ (0.280) \end{gathered}$ | $\begin{gathered} 5 / 16 \\ (0.318) \end{gathered}$ | $\begin{gathered} 3 / 8 \\ (0.380) \end{gathered}$ | Select Fill <br> Width (ft.) | Precon (min Level) |
| 11 A 5 | 18-5 | 8-4 | 123.9 | 21 | $\begin{gathered} 21 \\ (2.0) \end{gathered}$ | $\begin{gathered} 26 \\ (2.0) \end{gathered}$ | $\begin{gathered} 29 \\ (1.5) \end{gathered}$ | $\begin{gathered} 34 \\ (1.5) \end{gathered}$ | $\begin{gathered} 39 \\ (1.5) \end{gathered}$ | $\begin{gathered} 45 \\ (1.5) \end{gathered}$ | $\begin{gathered} 51 \\ (1.5) \end{gathered}$ | $\begin{gathered} 61 \\ (1.5) \end{gathered}$ | 8.0 | 2 |
| 13A6 | 22-0 | 10-0 | 172.9 | 25 | $\begin{gathered} 18 \\ (2.5) \end{gathered}$ | $\begin{gathered} 22 \\ (2.0) \end{gathered}$ | $\begin{gathered} 25 \\ (2.0) \end{gathered}$ | $\begin{gathered} 29 \\ (1.5) \end{gathered}$ | $\begin{gathered} 34 \\ (1.5) \end{gathered}$ | $\begin{gathered} 39 \\ (1.5) \\ \hline \end{gathered}$ | $\begin{gathered} 44 \\ (1.5) \end{gathered}$ | $\begin{gathered} 53 \\ (1.5) \\ \hline \end{gathered}$ | 8.0 | 2 |
| 15A5 | 23-5 | 9-3 | 172.2 | 25 | $\begin{gathered} 15 \\ (2.5) \end{gathered}$ | $\begin{gathered} 19 \\ (2.0) \end{gathered}$ | $\begin{gathered} 22 \\ (2.0) \end{gathered}$ | $\begin{gathered} 26 \\ (1.5) \end{gathered}$ | $\begin{gathered} 31 \\ (1.5) \\ \hline \end{gathered}$ | $\begin{gathered} 35 \\ (1.5) \end{gathered}$ | $\begin{gathered} 41 \\ (1.5) \end{gathered}$ | $\begin{gathered} 49 \\ (1.5) \end{gathered}$ | 8.0 | 2 |
| 15A7 | 25-5 | 11-7 | 228.3 | 29 | $\begin{gathered} 14 \\ (2.5) \end{gathered}$ | $\begin{gathered} 18 \\ (2.0) \end{gathered}$ | $\begin{gathered} 21 \\ (2.0) \end{gathered}$ | $\begin{gathered} 25 \\ (2.0) \end{gathered}$ | $\begin{gathered} 29 \\ (2.0) \end{gathered}$ | $\begin{gathered} 33 \\ (2.0) \end{gathered}$ | $\begin{gathered} 38 \\ (2.0) \end{gathered}$ | $\begin{gathered} 46 \\ (2.0) \end{gathered}$ | 8.0 | 2 |
| 17A6 | 26-11 | 10-10 | 232.7 | 29 | $\begin{gathered} 13 \\ (2.5) \end{gathered}$ | $\begin{gathered} 17 \\ (2.5) \end{gathered}$ | $\begin{gathered} 19 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 23 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 26 \\ (2.0) \end{gathered}$ | $\begin{gathered} 30 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 35 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 43 \\ (2.0) \\ \hline \end{gathered}$ | 8.0 | 2 |
| 18A5 | 27-2 | 9-10 | 212.2 | 28 | $\begin{gathered} 11 \\ (3.0) \end{gathered}$ | $\begin{gathered} 12 \\ (2.5) \end{gathered}$ | $\begin{gathered} 13 \\ (2.5) \end{gathered}$ | $\begin{gathered} 14 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 15 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 17 \\ (2.0) \end{gathered}$ | $\begin{gathered} 18 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 21 \\ (2.0) \end{gathered}$ | 8.0 | 2 |
| 17A8 | 28-11 | 13-2 | 306.2 | 33 | $\begin{gathered} 12 \\ (2.5) \end{gathered}$ | $\begin{gathered} 16 \\ (2.0) \end{gathered}$ | $\begin{gathered} 18 \\ (2.0) \end{gathered}$ | $\begin{gathered} 21 \\ (2.0) \end{gathered}$ | $\begin{gathered} 25 \\ (2.0) \end{gathered}$ | $\begin{gathered} 28 \\ (2.0) \end{gathered}$ | $\begin{gathered} 33 \\ (2.0) \end{gathered}$ | $\begin{gathered} 40 \\ (2.0) \end{gathered}$ | 8.0 | 3 |
| 20A7 | 31-8 | 12-8 | 319.5 | 34 | $\begin{gathered} 10 \\ (2.5) \end{gathered}$ | $\begin{gathered} 13 \\ (2.5) \end{gathered}$ | $\begin{gathered} 15 \\ (2.0) \end{gathered}$ | $\begin{gathered} 18 \\ (2.0) \end{gathered}$ | $\begin{gathered} 21 \\ (2.0) \end{gathered}$ | $\begin{gathered} 25 \\ (2.0) \end{gathered}$ | $\begin{gathered} 29 \\ (2.0) \end{gathered}$ | $\begin{gathered} 35 \\ (2.0) \\ \hline \end{gathered}$ | 8.0 | 3 |
| 21A6 | 31-11 | 11-8 | 295.4 | 33 | $\begin{gathered} 10 \\ (3.0) \end{gathered}$ | $\begin{gathered} 11 \\ (2.5) \end{gathered}$ | $\begin{gathered} 12 \\ (2.5) \end{gathered}$ | $\begin{gathered} 13 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 14 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 16 \\ (2.0) \end{gathered}$ | $\begin{gathered} 17 \\ (2.0) \end{gathered}$ | $\begin{gathered} 19 \\ (2.0) \end{gathered}$ | 8.0 | 3 |
| 22A5 | 32-2 | 10-8 | 270.6 | 32 |  | $\begin{gathered} 10 \\ (2.5) \end{gathered}$ | $\begin{gathered} 10 \\ (2.5) \end{gathered}$ | $\begin{gathered} 11 \\ (2.0) \end{gathered}$ | $\begin{gathered} 12 \\ (2.0) \end{gathered}$ | $\begin{gathered} 13 \\ (2.0) \end{gathered}$ | $\begin{gathered} 14 \\ (2.0) \end{gathered}$ | $\begin{gathered} 15 \\ (2.0) \end{gathered}$ | 8.0 | 3 |
| 19A9 | 32-5 | 14-9 | 384.9 | 37 | $\begin{gathered} 10 \\ (2.5) \end{gathered}$ | $\begin{gathered} 13 \\ (2.0) \end{gathered}$ | $\begin{gathered} 15 \\ (2.0) \end{gathered}$ | $\begin{gathered} 18 \\ (2.0) \end{gathered}$ | $\begin{gathered} 21 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 24 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 28 \\ (2.0) \end{gathered}$ | $\begin{gathered} 35 \\ (2.0) \\ \hline \end{gathered}$ | 8.0 | 3 |
| 25A5 | 35-10 | 11-4 | 318.2 | 35 |  |  | $\begin{gathered} 9 \\ (2.5) \end{gathered}$ | $\begin{gathered} 9 \\ (2.5) \end{gathered}$ | $\begin{gathered} 10 \\ (2.5) \end{gathered}$ | $\begin{gathered} 10 \\ (2.0) \end{gathered}$ | $\begin{gathered} 11 \\ (2.0) \end{gathered}$ | $\begin{gathered} 12 \\ (2.0) \end{gathered}$ | 8.0 | 3 |
| 21A10 | 35-11 | 16-5 | 472.7 | 41 | $\begin{gathered} 8 \\ (2.5) \end{gathered}$ | $\begin{gathered} 11 \\ (2.0) \end{gathered}$ | $\begin{gathered} 13 \\ (2.0) \end{gathered}$ | $\begin{gathered} 15 \\ (2.0) \end{gathered}$ | $\begin{gathered} 18 \\ (2.0) \end{gathered}$ | $\begin{gathered} 21 \\ (2.0) \end{gathered}$ | $\begin{gathered} 24 \\ (2.0) \end{gathered}$ | $\begin{gathered} 30 \\ (2.0) \end{gathered}$ | 8.0 | 3 |
| 23A8 | 36-5 | 14-5 | 420.0 | 39 | $\begin{gathered} 8 \\ (3.0) \end{gathered}$ | $\begin{gathered} 11 \\ (2.5) \end{gathered}$ | $\begin{gathered} 12 \\ (2.0) \end{gathered}$ | $\begin{gathered} 15 \\ (2.0) \end{gathered}$ | $\begin{gathered} 17 \\ (2.0) \end{gathered}$ | $\begin{gathered} 20 \\ (2.0) \end{gathered}$ | $\begin{gathered} 23 \\ (2.0) \end{gathered}$ | $\begin{gathered} 29 \\ (2.0) \end{gathered}$ | 8.0 | 3 |
| 25A7 | 37-10 | 13-8 | 411.5 | 39 |  | $\begin{gathered} 10 \\ (2.5) \end{gathered}$ | $\begin{gathered} 11 \\ (2.5) \end{gathered}$ | $\begin{gathered} 12 \\ (2.0) \end{gathered}$ | $\begin{gathered} 13 \\ (2.0) \end{gathered}$ | $\begin{gathered} 14 \\ (2.0) \end{gathered}$ | $\begin{gathered} 15 \\ (2.0) \end{gathered}$ | $\begin{gathered} 18 \\ (2.0) \end{gathered}$ | 8.0 | 3 |
| 26A6 | 38-1 | 12-9 | 382.0 | 38 |  | $\begin{gathered} 9 \\ (2.5) \end{gathered}$ | $\begin{gathered} 10 \\ (2.5) \end{gathered}$ | $\begin{gathered} 11 \\ (2.5) \end{gathered}$ | $\begin{gathered} 11 \\ (2.5) \end{gathered}$ | $\begin{gathered} 12 \\ (2.5) \end{gathered}$ | $\begin{gathered} 13 \\ (2.5) \end{gathered}$ | $\begin{gathered} 14 \\ (2.0) \end{gathered}$ | 8.0 | 3 |
| 23A11 | 39-5 | 18-0 | 569.4 | 45 |  | $\begin{gathered} 9 \\ (2.0) \end{gathered}$ | $\begin{gathered} 11 \\ (2.0) \end{gathered}$ | $\begin{gathered} 13 \\ (2.0) \end{gathered}$ | $\begin{gathered} 16 \\ (2.0) \end{gathered}$ | $\begin{gathered} 18 \\ (2.0) \end{gathered}$ | $\begin{gathered} 21 \\ (2.0) \end{gathered}$ | $\begin{gathered} 26 \\ (2.0) \end{gathered}$ | 8.0 | 3 |
| 25A9 | 39-11 | 16-1 | 511.8 | 43 |  | $\begin{gathered} 9 \\ (2.5) \end{gathered}$ | $\begin{gathered} 10 \\ (2.0) \end{gathered}$ | $\begin{gathered} 13 \\ (2.0) \end{gathered}$ | $\begin{gathered} 15 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 17 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 20 \\ (2.0) \end{gathered}$ | $\begin{gathered} 25 \\ (2.0) \end{gathered}$ | 8.0 | 3 |
| 29A5 | 40-10 | 12-2 | 386.7 | 39 |  |  |  |  | $\begin{gathered} 9 \\ (2.5) \end{gathered}$ | $\begin{gathered} 9 \\ (2.5) \end{gathered}$ | $\begin{gathered} 10 \\ (2.5) \end{gathered}$ | $\begin{gathered} 11 \\ (2.0) \end{gathered}$ | 8.0 | 4 |
| 28A8 | 42-7 | 15-6 | 524.7 | 44 |  |  | $\begin{gathered} 10 \\ (2.5) \end{gathered}$ | $\begin{gathered} 11 \\ (2.0) \end{gathered}$ | $\begin{gathered} 12 \\ (2.0) \end{gathered}$ | $\begin{gathered} 13 \\ (2.0) \end{gathered}$ | $\begin{gathered} 14 \\ (2.0) \end{gathered}$ | $\begin{gathered} 16 \\ (2.0) \end{gathered}$ | 8.0 | 4 |
| 25A12 | 42-11 | 19-7 | 675.2 | 49 |  | $\begin{gathered} 8 \\ (2.0) \end{gathered}$ | $\begin{gathered} 10 \\ (2.0) \end{gathered}$ | $\begin{gathered} 12 \\ (2.0) \end{gathered}$ | $\begin{gathered} 14 \\ (2.0) \end{gathered}$ | $\begin{gathered} 16 \\ (2.0) \end{gathered}$ | $\begin{gathered} 19 \\ (2.0) \end{gathered}$ | $\begin{gathered} 23 \\ (2.0) \end{gathered}$ | 8.0 | 4 |
| 30A6 | 43-1 | 13-7 | 457.7 | 42 |  |  |  | $\begin{gathered} 9 \\ (2.5) \end{gathered}$ | $\begin{gathered} 9 \\ (2.5) \end{gathered}$ | $\begin{gathered} 10 \\ (2.5) \end{gathered}$ | $\begin{gathered} 11 \\ (2.5) \end{gathered}$ | $\begin{gathered} 12 \\ (2.0) \end{gathered}$ | 8.0 | 4 |
| 30A7 | 44-1 | 14-9 | 512.6 | 44 |  |  | $\begin{gathered} 9 \\ (2.5) \end{gathered}$ | $\begin{gathered} 10 \\ (2.5) \end{gathered}$ | $\begin{gathered} 11 \\ (2.5) \end{gathered}$ | $\begin{gathered} 11 \\ (2.5) \end{gathered}$ | $\begin{gathered} 12 \\ (2.5) \end{gathered}$ | $\begin{gathered} 14 \\ (2.0) \\ \hline \end{gathered}$ | 8.0 | 4 |
| 28A10 | 44-7 | 17-10 | 637.2 | 48 |  | $\begin{gathered} 8 \\ (2.5) \end{gathered}$ | $\begin{gathered} 9 \\ (2.0) \end{gathered}$ | $\begin{gathered} 11 \\ (2.0) \end{gathered}$ | $\begin{gathered} 13 \\ (2.0) \end{gathered}$ | $\begin{gathered} 15 \\ (2.0) \end{gathered}$ | $\begin{gathered} 17 \\ (2.0) \end{gathered}$ | $\begin{gathered} 21 \\ (2.0) \end{gathered}$ | 8.0 | 4 |
| 27A13 | 46-5 | 21-2 | 790.1 | 53 |  |  | $\begin{gathered} 8 \\ (2.0) \end{gathered}$ | $\begin{gathered} 10 \\ (2.0) \end{gathered}$ | $\begin{gathered} 13 \\ (2.0) \end{gathered}$ | $\begin{gathered} 15 \\ (2.0) \end{gathered}$ | $\begin{gathered} 17 \\ (2.0) \end{gathered}$ | $\begin{gathered} 21 \\ (2.0) \end{gathered}$ | 8.0 | 4 |
| 31A9 | 47-4 | 17-4 | 651.6 | 49 |  |  |  | $\begin{gathered} 10 \\ (2.0) \end{gathered}$ | $\begin{gathered} 11 \\ (2.0) \end{gathered}$ | $\begin{gathered} 12 \\ (2.0) \end{gathered}$ | $\begin{gathered} 13 \\ (2.0) \end{gathered}$ | $\begin{gathered} 15 \\ (2.0) \end{gathered}$ | 8.0 | 4 |
| 34A6 | 48-0 | 14-5 | 539.2 | 46 |  |  |  |  | $\begin{gathered} 8 \\ (2.5) \end{gathered}$ | $\begin{gathered} 9 \\ (2.5) \end{gathered}$ | $\begin{gathered} 9 \\ (2.5) \end{gathered}$ | $\begin{gathered} 10 \\ (2.0) \end{gathered}$ | 8.0 | 4 |
| 30A11 | 48-1 | 19-6 | 749.1 | 52 |  |  | $\begin{gathered} 8 \\ (2.0) \end{gathered}$ | $\begin{gathered} 10 \\ (2.0) \end{gathered}$ | $\begin{gathered} 12 \\ (2.0) \end{gathered}$ | $\begin{gathered} 13 \\ (2.0) \end{gathered}$ | $\begin{gathered} 15 \\ (2.0) \end{gathered}$ | $\begin{gathered} 19 \\ (2.0) \end{gathered}$ | 8.0 | 4 |
| 32A9 | 48-7 | 17-7 | 676.2 | 50 |  |  |  | $\begin{gathered} 10 \\ (2.0) \end{gathered}$ | $\begin{gathered} 11 \\ (2.0) \end{gathered}$ | $\begin{gathered} 12 \\ (2.0) \end{gathered}$ | $\begin{gathered} 13 \\ (2.0) \end{gathered}$ | $\begin{gathered} 14 \\ (2.0) \end{gathered}$ | 8.0 | 4 |
| 29A14 | 49-11 | 22-10 | 913.8 | 57 |  |  |  | $\begin{gathered} 9 \\ (2.0) \end{gathered}$ | $\begin{gathered} 12 \\ (2.0) \end{gathered}$ | $\begin{gathered} 14 \\ (2.0) \end{gathered}$ | $\begin{gathered} 16 \\ (2.0) \end{gathered}$ | $\begin{gathered} 20 \\ (2.0) \end{gathered}$ | 8.0 | 4 |
| 34A8 | 50-0 | 16-10 | 662.3 | 50 |  |  |  | $\begin{gathered} 9 \\ (2.5) \end{gathered}$ | $\begin{gathered} 10 \\ (2.5) \end{gathered}$ | $\begin{gathered} 11 \\ (2.5) \end{gathered}$ | $\begin{gathered} 12 \\ (2.5) \end{gathered}$ | $\begin{gathered} 13 \\ (2.0) \end{gathered}$ | 8.0 | 4 |
| 35A7 | 50-3 | 15-10 | 622.7 | 49 |  |  |  | $\begin{gathered} 9 \\ (2.5) \end{gathered}$ | $\begin{gathered} 9 \\ (2.5) \end{gathered}$ | $\begin{gathered} 9 \\ (2.5) \end{gathered}$ | $\begin{gathered} 10 \\ (2.5) \end{gathered}$ | $\begin{gathered} 11 \\ (2.0) \\ \hline \end{gathered}$ | 8.0 | 4 |
| 32A11 | 50-7 | 19-11 | 803.8 | 54 |  |  |  | $\begin{gathered} 9 \\ (2.0) \end{gathered}$ | $\begin{gathered} 11 \\ (2.0) \end{gathered}$ | $\begin{gathered} 12 \\ (2.0) \end{gathered}$ | $\begin{gathered} 14 \\ (2.0) \\ \hline \end{gathered}$ | $\begin{gathered} 17 \\ (2.0) \end{gathered}$ | 8.0 | 4 |
| 35A7 | 50-3 | 15-10 | 622.7 | 49 |  |  |  | $\begin{gathered} 9 \\ (2.5) \end{gathered}$ | $\begin{gathered} 9 \\ (2.5) \end{gathered}$ | $\begin{gathered} 9 \\ (2.5) \end{gathered}$ | $\begin{gathered} 10 \\ (2.5) \end{gathered}$ | $\begin{gathered} 11 \\ (2.0) \end{gathered}$ | 8.0 | 4 |
| 32A11 | 50-7 | 19-11 | 803.8 | 54 |  |  |  | $\begin{gathered} 9 \\ (2.0) \end{gathered}$ | $\begin{gathered} 11 \\ (2.0) \end{gathered}$ | $\begin{gathered} 12 \\ (2.0) \end{gathered}$ | $\begin{gathered} 14 \\ (2.0) \end{gathered}$ | $\begin{gathered} 17 \\ (2.0) \end{gathered}$ | 8.0 | 4 |
| VARIES | UP TO 65' |  |  | VARIES |  |  |  |  |  | UIRE |  |  |  |  |

Notes:

1. Not for a specific structural design. Use for budget estimating only. A CANDE analysis is required for final design and quotation.
2. The above table is based upon the minimum requirements of the AASHTO LRFD Design Specification, Section 12, and:
a. Backfill material per AASHTO M145, class A-2-5 or better.
b. Backfill 120 pcf in density and compacted to $90 \%$ modified proctor.
c. The minimum cover is per article 12.8.9.4
d. The minimum select backfill width (eight feet) is measured from outside the maximum span on each side of the structure.

This width only applies when the material adjacent to the select zone is determined to be competent, well consolidated material
3. Select backfill width may increase for situations where lower strength fill exists in either the select fill zone or the adjacent embankment zone.
4. This estimate is for single barrel structures. For multiple barrels, more investigation is required.

| TABLE 80. BRIDGECOR 2-RADIUS ARCH $15{ }^{\prime \prime} \times$ ¢ 1 ¹" |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| WEIGHT TABLES |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Dimensions to Inside Corrugation |  |  |  | Gage Thickness (Inches) <br> Weight Shown as per Foot of Structure |  |  |  |  |  |  |  | Plate Make-Up |  |  |  |  |  |
| Shape | Maximum Span (Ft.-In.) | $\begin{gathered} \text { Rise } \\ \text { (Ft.-In.) } \end{gathered}$ | Total S | $\begin{gathered} 10 \\ (0.140) \end{gathered}$ | $\begin{gathered} 8 \\ (0.170) \end{gathered}$ | $\begin{gathered} 7 \\ (0.188) \end{gathered}$ | $\begin{gathered} 5 \\ (0.218) \end{gathered}$ | $\begin{gathered} 3 \\ (0.249) \end{gathered}$ | $\begin{gathered} 1 \\ (0.280) \end{gathered}$ | $\begin{gathered} 5 / 16 \\ (0.318) \end{gathered}$ | $\begin{gathered} 3 / 8 \\ (0.380) \end{gathered}$ | 9 S | 8 S | 7 S | 6 S | 5 S | Total Plates |
| 11A5 | 18-5 | 8-4 | 21 | 247 | 299 | 330 | 381 | 434 | 487 | 581 | 691 |  | 1 | 1 | 1 |  | 3 |
| 13A6 | 22-0 | 10-0 | 25 | 290 | 350 | 387 | 447 | 510 | 572 | 681 | 811 | 1 | 2 |  |  |  | 3 |
| 15A5 | 23-5 | 9-3 | 25 | 290 | 350 | 387 | 447 | 510 | 572 | 681 | 811 | 1 | 2 |  |  |  | 3 |
| 15A7 | 25-5 | 11-7 | 29 | 341 | 412 | 455 | 526 | 599 | 672 | 801 | 954 | 1 | 1 |  | 2 |  | 4 |
| 17A6 | 26-11 | 10-10 | 29 | 341 | 412 | 455 | 526 | 599 | 671 | 801 | 953 |  | 1 | 3 |  |  | 4 |
| 18A5 | 27-2 | 9-10 | 28 | 330 | 399 | 441 | 509 | 580 | 650 | 776 | 923 |  | 1 | 2 | 1 |  | 4 |
| 17 A 8 | 28-11 | 13-2 | 33 | 392 | 474 | 523 | 604 | 687 | 771 | 921 | 1096 |  |  | 3 | 2 |  | 5 |
| 20A7 | 31-8 | 12-8 | 34 | 395 | 476 | 526 | 608 | 693 | 778 | 927 | 1104 | 2 | 2 |  |  |  | 4 |
| 21A6 | 31-11 | 11-8 | 33 | 385 | 463 | 512 | 592 | 674 | 756 | 902 | 1074 | 1 | 3 |  |  |  | 4 |
| 22A5 | 32-2 | 10-8 | 32 |  | 451 | 498 | 575 | 655 | 735 | 877 | 1044 | 1 | 2 | 1 |  |  | 4 |
| 19A9 | 32-5 | 14-9 | 37 | 435 | 525 | 580 | 670 | 763 | 856 | 1022 | 1216 |  | 3 | 1 | 1 |  | 5 |
| 25A5 | 35-10 | 11-4 | 35 |  |  | 541 | 625 | 712 | 799 | 953 | 1135 | 3 | 1 |  |  |  | 4 |
| 21A10 | 35-11 | 16-5 | 41 | 478 | 577 | 637 | 736 | 839 | 941 | 1123 | 1337 | 2 | 2 | 1 |  |  | 5 |
| 23A8 | 36-5 | 14-5 | 39 | 457 | 561 | 620 | 716 | 814 | 913 | 1092 | 1298 |  |  | 3 | 3 |  | 6 |
| 25A7 | 37-10 | 13-8 | 39 |  | 551 | 608 | 703 | 801 | 898 | 1072 | 1276 | 2 | 2 |  |  | 1 | 5 |
| 26A6 | 38-1 | 12-9 | 38 |  | 538 | 594 | 687 | 782 | 877 | 1047 | 1246 |  | 3 | 2 |  |  | 5 |
| 23A11 | 39-5 | 18-0 | 45 |  | 639 | 705 | 815 | 928 | 1040 | 1243 | 1478 |  | 3 | 3 |  |  | 6 |
| 25A9 | 39-11 | 16-1 | 43 |  | 613 | 676 | 782 | 890 | 998 | 1192 | 1418 |  | 3 | 2 |  | 1 | 6 |
| 29A5 | 40-10 | 12-2 | 39 |  |  |  |  | 801 | 899 | 1073 | 1276 |  | 4 | 1 |  |  | 5 |
| 28A8 | 42-7 | 15-6 | 44 |  |  | 680 | 811 | 922 | 1034 | 1237 | 1470 |  |  | 3 | 3 | 1 | 7 |
| 25A12 | 42-11 | 19-7 | 49 |  | 690 | 762 | 811 | 1003 | 1126 | 1344 | 1599 | 1 | 5 |  |  |  | 6 |
| 30A6 | 43-1 | 13-7 | 42 |  |  |  | 753 | 858 | 962 | 1148 | 1367 | 2 | 3 |  |  |  | 5 |
| 30A7 | 44-1 | 14-9 | 44 |  |  | 680 | 786 | 896 | 1004 | 1199 | 1427 | 4 | 1 |  |  |  | 5 |
| 28A10 | 44-7 | 17-10 | 48 |  | 677 | 748 | 864 | 984 | 1104 | 1319 | 1569 | 2 | 2 | 2 |  |  | 6 |
| 27A13 | 46-5 | 21-2 | 53 |  |  | 820 | 947 | 1079 | 1210 | 1445 | 1720 | 5 | 1 |  |  |  | 6 |
| 31A9 | 47-4 | 17-4 | 49 |  |  |  | 881 | 1016 | 1140 | 1363 | 1621 |  | 3 | 1 | 3 |  | 7 |
| 34A6 | 48-0 | 14-5 | 46 |  |  |  |  | 947 | 1062 | 1268 | 1508 |  | 4 | 2 |  |  | 6 |
| 30A11 | 48-1 | 19-6 | 52 |  |  | 805 | 931 | 1060 | 1189 | 1419 | 1690 | 4 | 2 |  |  |  | 6 |
| 32A9 | 48-7 | 17-7 | 50 |  |  |  | 910 | 1035 | 1162 | 1388 | 1651 |  | 3 | 2 | 2 |  | 7 |
| 29A14 | 49-11 | 22-10 | 57 |  |  |  | 1026 | 1168 | 1310 | 1565 | 1861 | 1 | 6 |  |  |  | 7 |
| 34A8 | 50-0 | 16-10 | 50 |  |  |  | 910 | 1048 | 1176 | 1407 | 1673 |  |  | 2 | 6 |  | 8 |
| 35A7 | 50-3 | 15-10 | 49 |  |  |  | 881 | 1003 | 1126 | 1344 | 1599 | 1 | 5 |  |  |  | 6 |
| 32A11 | 50-7 | 19-11 | 54 |  |  |  | 976 | 1111 | 1246 | 1489 | 1771 |  | 5 | 2 |  |  | 7 |
| VARIES | UP TO 65' |  | VARIES |  |  |  |  |  | INQ | UIRE |  |  |  |  |  |  |  |

Notes:

1. Weights include $3 / 4^{\prime \prime}$ diameter fasteners for assembly. Inquire for applications requiring $7 / 8^{\prime \prime}$ diameter fasteners.
2. Weights include a 3 oz . per square foot galvanized coating on both sides.
3. An alternate plate make-up may be supplied due to material availability. This may affect the overall structure weight.
4. 10 ga. through 1 ga. plate net lay length is $45^{\prime \prime} .5 / 16^{\prime \prime}$ and $3 / 8^{\prime \prime}$ plate net lay length is 30 ".
5. If unbalanced channels are required, add 20 lbs ./ foot of the total structure length.

For more information, call Contech Engineered Solutions:

## 800-338-1 122

## www.ContechES.com

9025 Centre Pointe Drive, Suite 400
West Chester, Ohio 45069
(800) 338-1 122

Fax: (513) 645-7993

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[^0]:    * Larger steel sizes are available up through 65 -foot spans with our BridgeCor ${ }^{\circledR}$ product line. Call your local Contech representative for more information.
    ** The design process for these bridge structures is not covered by this document. Call your local Contech representative for more information.

[^1]:    Notes:

    1. Dimensions are to inside crests of corrugations and are subject to manufacturing tolerances.
    2. These plate arrangements will be furnished unless noted otherwise on assembly drawings.
    3. Galvanized, with bolts and nuts.
    4. Specified thickness is a nominal galvanized thickness.
[^2]:    (1) Dimensions are to inside crests of corrugations and are subject to manufacturing tolerances. See Table 23 for structure Pi
    ${ }^{(2)}$ These plate arrangements will be furnished unless noted otherwise on assembly drawings.
    ${ }^{(3)}$ Galvanized, with bolts and nuts.

[^3]:    ${ }^{(1)}$ Smaller (junior) underpasses are also available.

[^4]:    1.2.6 As Directed - In these specifications the words "as directed" shall refer to the directions to the Contractor from the Owner or his designated representative.

